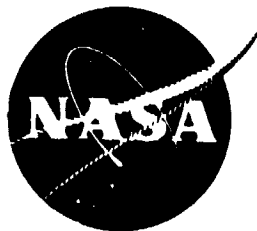


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NASA CR-135140

QUIET CLEAN SHORT-HAUL EXPERIMENTAL ENGINE (QCSEE)

Whirl Test of Cam/Harmonic Pitch Change Actuation System

by

Aircraft Systems Department, Propulsion Project Group

Hamilton Standard
Division of United Technologies Corporation

Under Subcontract to General Electric Company
(P.O. 200-4XX-14G38570)

(NASA-CR-135140) QUIET CLEAN SHORT-HAUL
EXPERIMENTAL ENGINE (QCSEE) WHIRL TEST OF
CAM/HARMONIC PITCH CHANGE ACTUATION SYSTEM
Contractor Report, 10 Nov. 1975 - 16 Feb.
1976 (Hamilton Standard, Windsor Locks,

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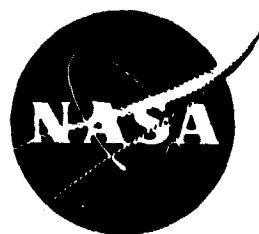
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Prepared For

National Aeronautics and Space Administration

NASA Lewis Research Center
Contract NAS3-18021





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16. Abstract <p>A variable pitch fan actuation system, which incorporates a remote nacelle mounted blade angle regulator, was tested. The regulator drives a rotating fan mounted mechanical actuator through a flexible shaft and differential gear train. The actuator incorporates a high-ratio harmonic drive attached to a multi-track spherical cam which changes blade pitch through individual cam follower arms attached to each blade trunnion.</p> <p>Testing of the actuator on a whirl rig, is reported. The tests were conducted to verify that the unit satisfied the design requirements and was structurally adequate for use in an engine test.</p>					
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TABLE OF CONTENTS

<u>Section</u>	<u>Description</u>	<u>Page</u>
1.0	SUMMARY	1
2.0	INTRODUCTION	3
3.0	SYSTEM DESCRIPTION	5
4.0	RIG DESCRIPTION	11
5.0	TEST PROCEDURE	19
6.0	TEST RESULTS	23
7.0	CONCLUSION	55
8.0	APPENDICES	57
A	Operating Procedure	59
B	Test Plans	71
C	Sanborn Records	91
D	Log Sheets	121
E	Test Chronology	209
F	References	217

LIST OF FIGURES

<u>Figure</u>	<u>Title</u>	<u>Page</u>
1	QCSEE Variable Pitch Actuator System	6
2	Beta Regulator Schematic	7
3	Whirl Rig Arrangement	12
4	Curve - Net Twisting Moment	13
5	Assembly - Front Input Hardware	14
6	Photograph - Actuator on Whirl Rig	17
7	Photograph - 763494-1 Output Shaft	24
8	Output Shaft Comparison	25
9	Photograph - 763402-1 Flexible Shaft	28
10	Curve - Lubrication Flow vs Pressure	30
11	Curve - Lubrication Flow vs Pressure	31
12	Curve - Output Voltage vs Blade Angle, LVDT #1	34
13	Curve - Output Voltage vs Blade Angle, LVDT #2	35
14	Curve - Overtravel & Shaft Torque vs Valve Time Constant	38
15	Test Setup - Static Blade Angle Positioning Accuracy	43
16	Curve - Set vs Resultant Blade Angle	46
17	Frequency Response - Servo Valve Current vs LVDT Current, $\beta = -3^\circ$, 0 rpm, No Snubber	49
18	Frequency Response - Servo Valve Current vs Blade Angle, $\beta = -3^\circ$, 0 rpm, No Snubber	50

LIST OF FIGURES (Continued)

<u>Figure</u>	<u>Title</u>	<u>Page</u>
19	Frequency Response - Servo Valve Current vs LVDT Current, $\beta = -3^\circ$, 3066 rpm, No Snubber	51
20	Frequency Response - Servo Valve Current vs LVDT Current, $\beta = -100^\circ$, 2920 rpm, No Snubber	52
21	Frequency Response - Servo Valve Current vs LVDT Current, $\beta = -3^\circ$, 0 rpm, Snubber	53
22	Frequency Response, Servo Valve Current vs Blade Angle, $\beta = -3^\circ$, 0 rpm, Snubber	54

LIST OF TABLES

<u>Table</u>	<u>Description</u>	<u>Page</u>
I	Instrumentation List	16
II	Flight Cycle Setup	21
III	Test Data - LVDT Calibration	32
IV	Test Data - Travel Limit Switch	37
V	Test Data - Blade Angle Positioning Accuracy (Rotating)	39
VI	Test Data - Blade Angle Positioning Accuracy (Rotating)	40
VII	Test Data - Blade Angle Positioning Accuracy (Rotating)	41
VIII	Test Data - Blade Angle Positioning Accuracy (Static)	44
IX	Test Data - Performance	47

1.0

SUMMARY

The Hamilton Standard blade pitch change actuation system for the Quiet Clean Short Haul Experimental Engine (QCSEE) was tested on a whirl rig, at Hamilton Standard, between November 10, 1975 and February 16, 1976.

The objectives of the test were to verify that the unit satisfied the design requirements and was structurally adequate for use in an engine test.

The testing included evaluation of the travel limit switch, blade angle position accuracy, performance, frequency response, and endurance.

During tests of the travel limit switch it was found that the no-back output shaft was under-designed. Analysis of the shaft revealed that it could not be adequately strengthened within the space available. In order to reduce the load on the no-back, a snubber was installed in the actuator. When run with the snubber, no further distress was noted on the output shaft.

The testing showed that:

- Blade overtravel after actuation of the travel limit switch at maximum pitch change rate and zero fan speed was within the calculated value of 6.5-7.0 degrees.
- Blade angle can be positioned within 0.25 degrees when moving from open to close at zero fan speed and within 1.5 degrees at high fan speeds.
- There is approximately 1 degree of hysteresis in the system when reversing the direction of blade angle change at zero fan speed.
- The minimum attainable blade angle change was 0.17 degrees toward open and 0.26 degrees toward close.
- The maximum pitch change rate attained during a blade angle change was 135 degrees/second.
- Frequency response without the snubber indicated reasonable correlation with predictions at frequencies up to 1 Hertz where the magnitude ratio was lower and the phase shift was higher than at frequencies above 1 Hertz.

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- Frequency response with the snubber again indicated reasonable correlation with predictions at frequencies up to 1 Hertz with excitation magnitudes of ± 8 ma, however with ± 4 ma excitation the magnitude ratio was down and there was considerable phase shift.
- The actuation system successfully completed 500 simulated mission endurance cycles at pitch change rates up to 75 degrees/second and 50 cycles at pitch change rates up to 135 degrees/second.

2.0

INTRODUCTION

During the proposal effort for the Quiet Clean Shorthaul Experimental Engine (QCSEE), a design study of ten prospective fan pitch change systems was conducted. The results of this study were reported in HSPC 74A14 QCSEE Variable Pitch Fan System Proposal. On the basis of this effort, four systems were selected for further study.

The detail study of the four systems was conducted under General Electric Purchase Order 200-4XX-14G31376. The results of the study were presented in SP 08A74 QCSEE Variable Pitch Fan Pitch Change System. The study showed that a system incorporating a remotely mounted Beta Regulator, driving a harmonic drive/cam actuator through a flexible drive shaft, was the most attractive. This type of system was designed, manufactured, and tested under NASA Contract NAS 3-18021. The results of the design effort were reported in NASA CR-134852 which also includes a summary of the preliminary design studies done on the other systems.

A second actuator was also developed by the General Electric Company. Details of the design of the General Electric actuator are presented in NASA CR-134873 "QCSEE Ball Spline Pitch Change Mechanism Design Report".

This report describes the whirl rig testing conducted on the system. The object of the test was to determine the operating characteristics of the actuator, verify that it satisfies the design requirements, and assure its structural adequacy for use in an engine test.

3.0

SYSTEM DESCRIPTION

The variable pitch actuator system is shown in Figure 1. An electrical input command signal from the engine digital control to the electro-hydraulic servo valve (EHV) directs high pressure oil to motors in the beta regulator. This provides rotary mechanical input to the actuator differential gear train through a flexible drive shaft. Rotary motion is then transmitted through a no-back, harmonic drive, rotating cam, and cam follower arms to the blade trunnions. Since there is a fixed mechanical relationship between hydraulic motor rotation and blade angle, two linear variable differential transformers (LVDT) driven by motor output provide redundant blade angle feedback signals to the digital control to close the control loop and null the input signal when the blades reach the commanded position.

The overall gear ratio from the blades to the drive shaft is 1005:1 with most of the ratio (201:1) provided by a harmonic drive. This permits the low-torque power transmission elements between the beta regulator and the harmonic drive to be designed for low weight and improved blade angle accuracy.

The mechanical pitch change power and blade angle feedback functions are provided by the beta regulator module which is remotely mounted in a readily accessible area of the engine cowling. A simplified schematic of the beta regulator is shown in Figure 2. A blade angle change command from the engine control to the EHV mounted in the accessory section, causes movement of the servo valve to direct supply oil to either the open or close pitch ports of the hydraulic motor. The motor output drives the flexible shaft to change blade angle and drives two LVDT's through a worm gear and screw to provide an electrically redundant blade position feedback. Electrical limit switches are provided to cut off the command signal to the EHV if a blade angle is commanded beyond the maximum operating range. Pressure relief valves across the motor ports limit motor pressure to 3000 psi during rapid accelerations of the actuator system.

The rotary output of the beta regulator is transmitted to the actuator differential gear train through a flexible drive shaft passing through the engine reduction gearing. The shaft core is encased in a flexible teflon lined casing supported in a rigid conduit mounted on the engine reduction gear support. Continuous engine lubrication oil flow is directed through the casing from the beta regulator to lubricate the core and the actuator components.

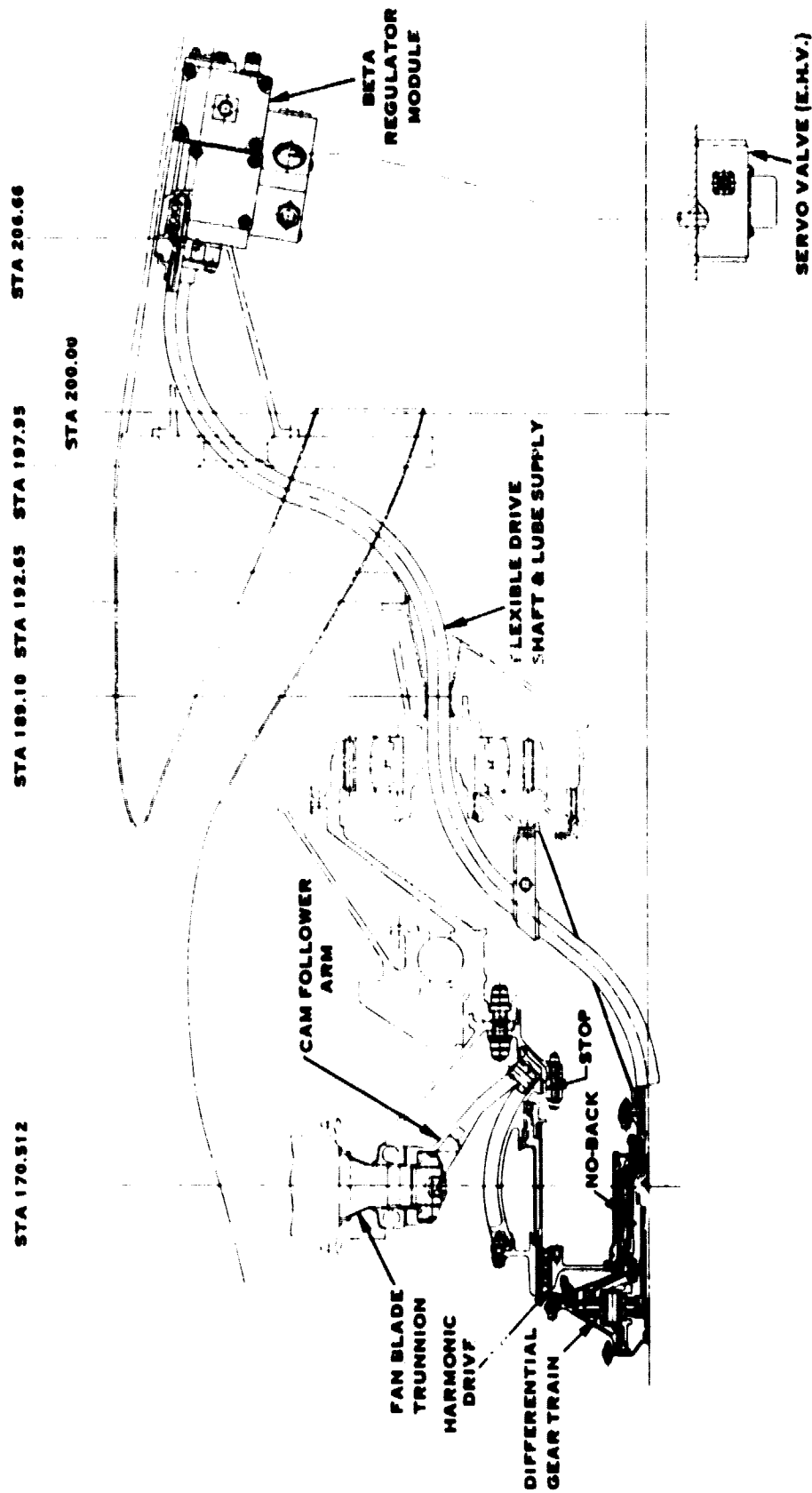


FIGURE 1. QCSEE VARIABLE PITCH ACTUATOR SYSTEM

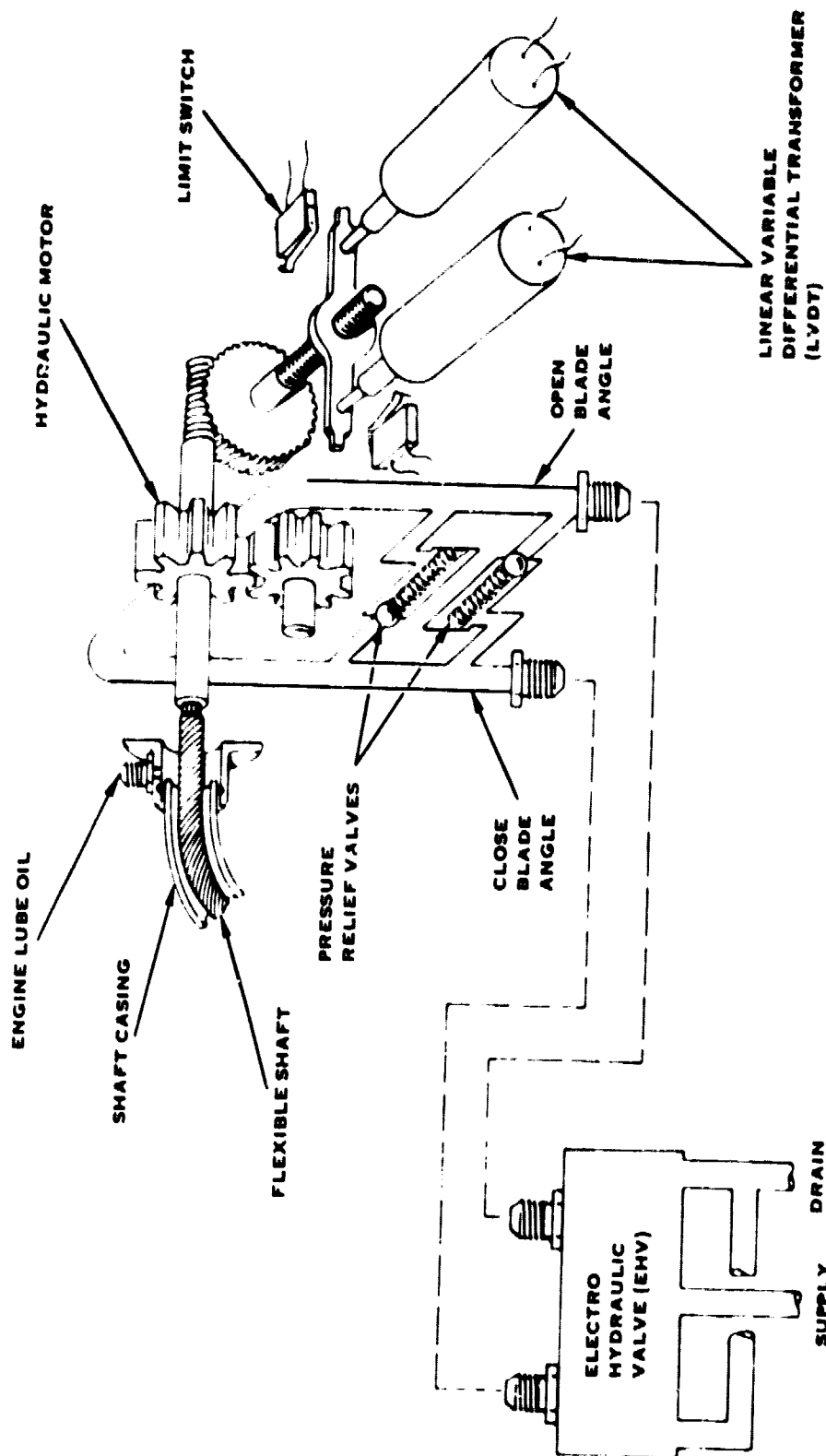


FIGURE 2. BETA REGULATOR SCHEMATIC

3.0 (Continued)

A planetary differential gear train is utilized to cross the rotating boundary of the fan. The differential gearing is a conventional 5:1 ratio phase difference type with a grounded sun gear, an input sun gear driven by the flexible shaft, three pairs of planet gears on a bearing supported cage, a reference speed ring gear fixed to the fan disk and an output ring gear driving the no-back input. With no pitch change input, the output ring gear rotates at fan speed. Rotation of the input sun gear during pitch change causes the output ring gear to either advance or recede with respect to the fan speed. This change in output is the input to the no-back. The gears and bearings are lubricated by oil directed outward centrifugally from the sun gear shafts.

A bi-directional spring clutch or "no-back" is provided between the differential gearing and the harmonic drive to maintain the set blade angle position in the absence of a pitch change command. This device consists of a self-energizing steel spring which is in contact with the inner surface of a fixed housing, the input and output shafts and the necessary couplings and bearings. When holding a fixed blade angle, the blade loads are transmitted to ground (housing) through the spring. When the input acts against opposing blade loads (raising the load), the spring slides in the housing and does not react to any blade loads. When the input acts against aiding blade loads (lowering the load), the input releases the spring at the commanded pitch rate and the blade load energy is dissipated in frictional heat between the spring and housing. Due to the short duty cycle and the thermal mass of the parts, the total heat rise is low in the no-back. Lubrication oil flows continually through the no-back and is supplied centrifugally from the sun gear shafts.

No-back housing torque is reacted by a disk-type torque limiter brake. The no-back is a high-gain locking device capable of locking more than a million in-lbs of torque at high friction coefficients, and the torque limiter limits maximum no-back torque to ground to acceptable structural limits during rapid pitch change decelerations. The brake disks are lubricated by oil supplied centrifugally from the differential gearing.

The harmonic drive provides the primary gear reduction for the mechanical actuator and increases the input torque to the level required to change pitch. Four basic elements are incorporated in this high-ratio (201:1) mechanical transmission rated at 50,000 in-lbs output. They are: a three-lobed harmonic-shaped wave generator input plug which provides the harmonic the harmonic lobe shape to the flexible spline, a triplex split inner race ball bearing set for high radial stiffness, a flexible spline (flex spline) to convert from

3.0 (Continued)

the harmonic lobe shape to a grounded circular shape with minimum frictional losses and a stiff circular output spline which drives the blade pitch cam.

The thin-race ball bearings are pressed on the three-lobed wave generator plug and assume the three-lobe harmonic shape. Spline teeth on the outside diameter of the flex spline mesh with spline teeth on the inside diameter of the circular spline at the three lobe locations. Circular splines on the other end of the flex spline ground it to the fan disk. Due to a 3-tooth difference in number of teeth between the circular spline and flex spline ($603-600=3$), one revolution of the wave generator input rotates the circular spline output $3/603$ or $1/201$ of a revolution.

Lubrication oil for the harmonic bearings and splines is supplied centrifugally from the differential gearing and no-back.

The cam and follower arms convert output rotation of the harmonic drive to fan blade angle change. Titanium follower arms, splined and clamped to the blade trunnions, engage individual cam slots in the spherical cam surface through cam rollers to synchronize the blades and sum the blade torques. The radial axis defined by the roller and cam track centerlines always intersects the fan axis of rotation at the same point similar to the apex point of a bevel gear mesh.

Cam support is provided by a preloaded duplex bearing set mounted on a support ring attached to the fan disk mounting flange for accurate balance control. Lubrication oil from the harmonic drive lubes the bearing set and is returned centrifugally to the engine scavenge area. A single dynamic oil seal with centrifugal venting precludes a dynamic pressure head.

Fixed mechanical stop lugs between the cam and cam support ring restrict the blades to 7° overtravel at each end of the maximum operating range.

4.0

RIG DESCRIPTION

Figure 3 is a drawing showing the arrangement of the whirl rig and the actuator.

The whirl rig used for the test was a modification of an existing rig. The rig utilizes a 186.4 kilowatts (250 horsepower) electric motor to drive the fan through an eddy current clutch and a speed increasing gearbox. The connecting shaft between the gearbox and the actuator has a flange which dimensionally duplicates the actuator/disk mounting surface in the engine. The flange also provides a path for the removal of the lubrication fluid.

A disk together with trunnions, stub blades (counterweights), and other retention hardware was provided for the test by General Electric. The stub blades are designed to apply the same centrifugal load to the blade retention and the actuator as the actual blade, and to approximate the twisting moment of the actual blade. Figure 4 is a curve of twisting moment versus blade angle for the actual and the stub blade. Stub blades were used for the test as they do not produce thrust and therefore can be driven by a relatively small motor.

Initial attempts to run the rig revealed the need to provide a shroud to enclose the stub blades and their retention to reduce the windage losses and consequently the power required to drive the assembly and the noise level in the vicinity of the test rig.

In the engine, the Beta Regulator is mounted behind the actuator and the flex shaft is routed through the engine gearbox to the actuator. To duplicate this arrangement on the whirl rig would require a hollow connecting shaft between the speed increaser gear box and the actuator, a hollow shaft through the gear box, and a quill shaft between the flex cable and the pitch change input at the actuator. This approach was investigated and discarded as it added another spring rate to the pitch change input system (the quill shaft), as well as being expensive and time consuming to obtain a hollow shaft gearbox.

Instead, a set of test hardware which provided a front input to the actuator for the flex cable was designed and manufactured. This hardware does not affect the spring rate of the input system. Figure 5 is an assembly drawing of the front input hardware.

In an engine installation, the lubricating and pitch change fluids are supplied by an engine driven pump. For the whirl test, a Viking pump rated at 18.9 liters/min (5 gpm) at 68.9 newtons/cm² (100 psi) was used to supply the

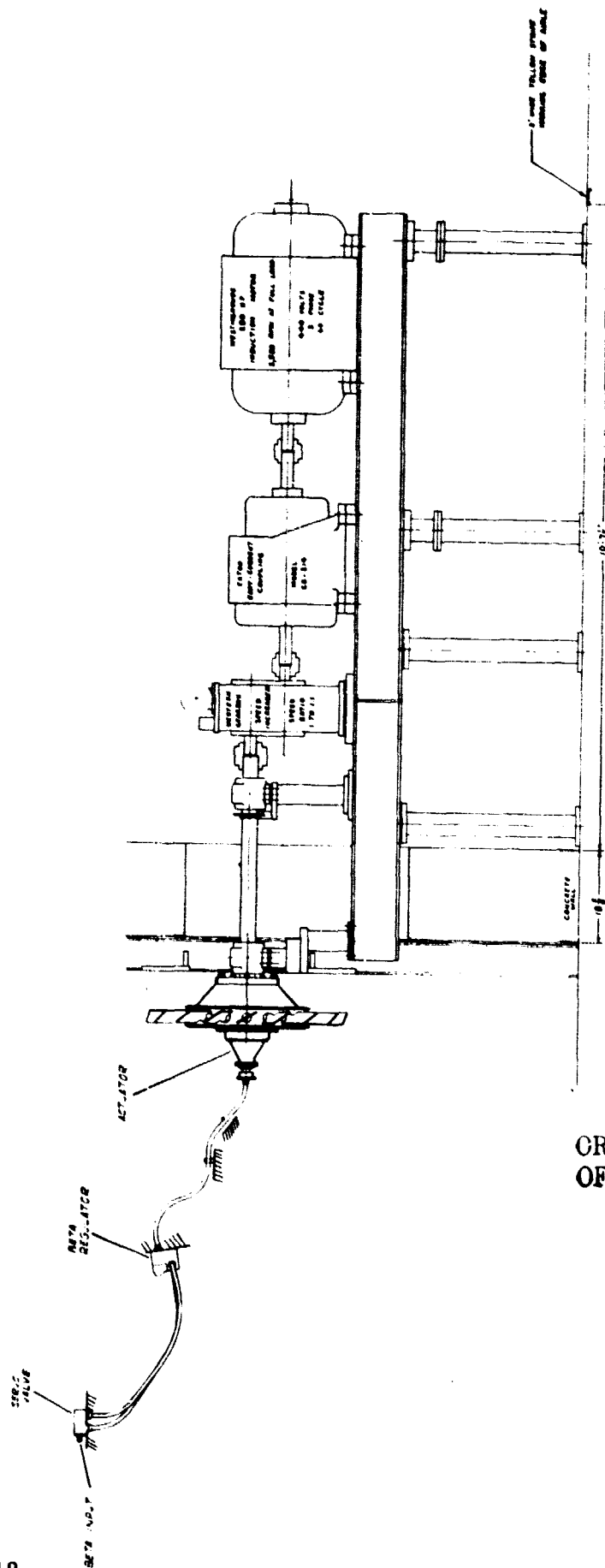


FIGURE 3. WHIRL RIG ARRANGEMENT

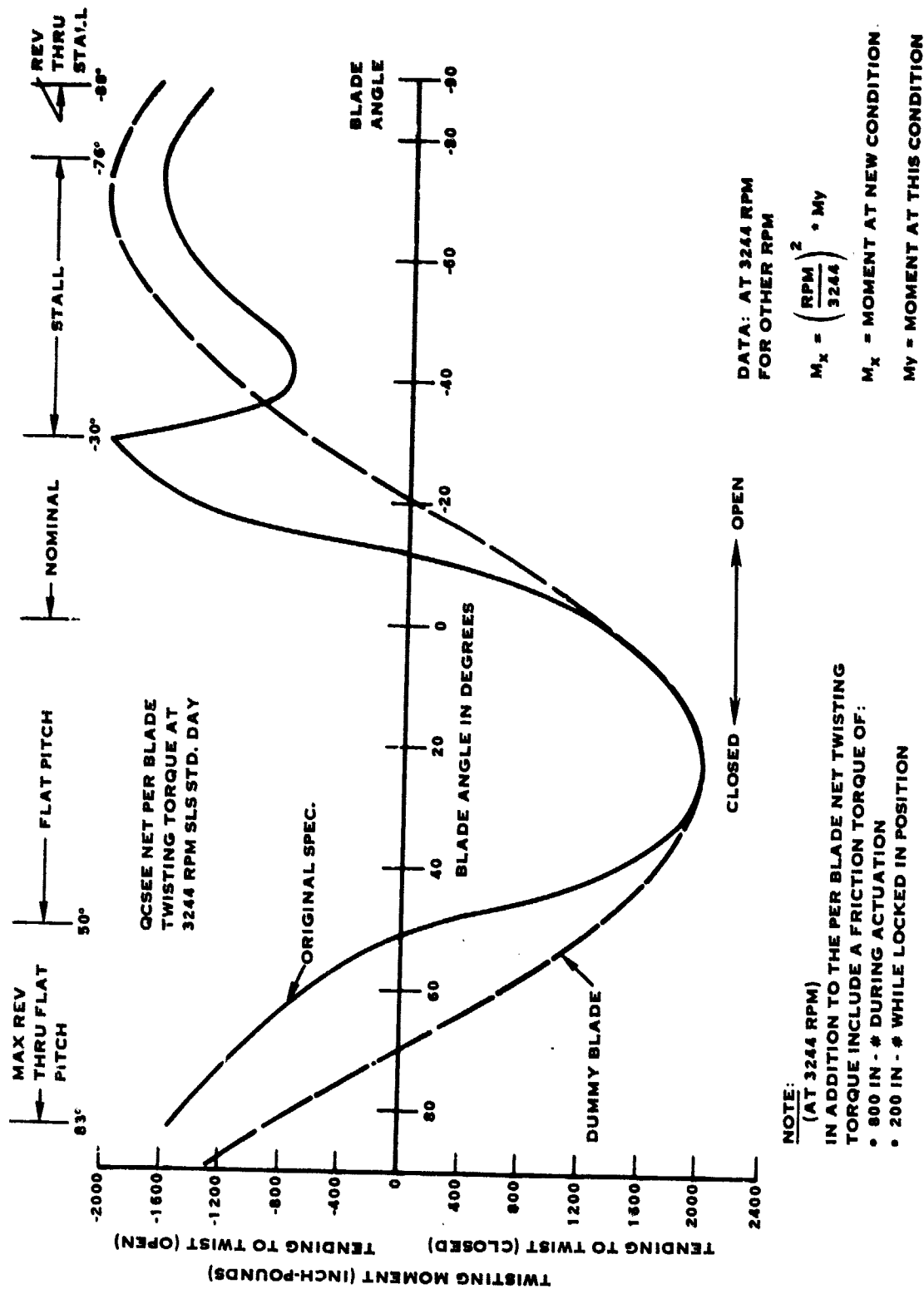


FIGURE 4. MAX NET TWISTING MOMENT

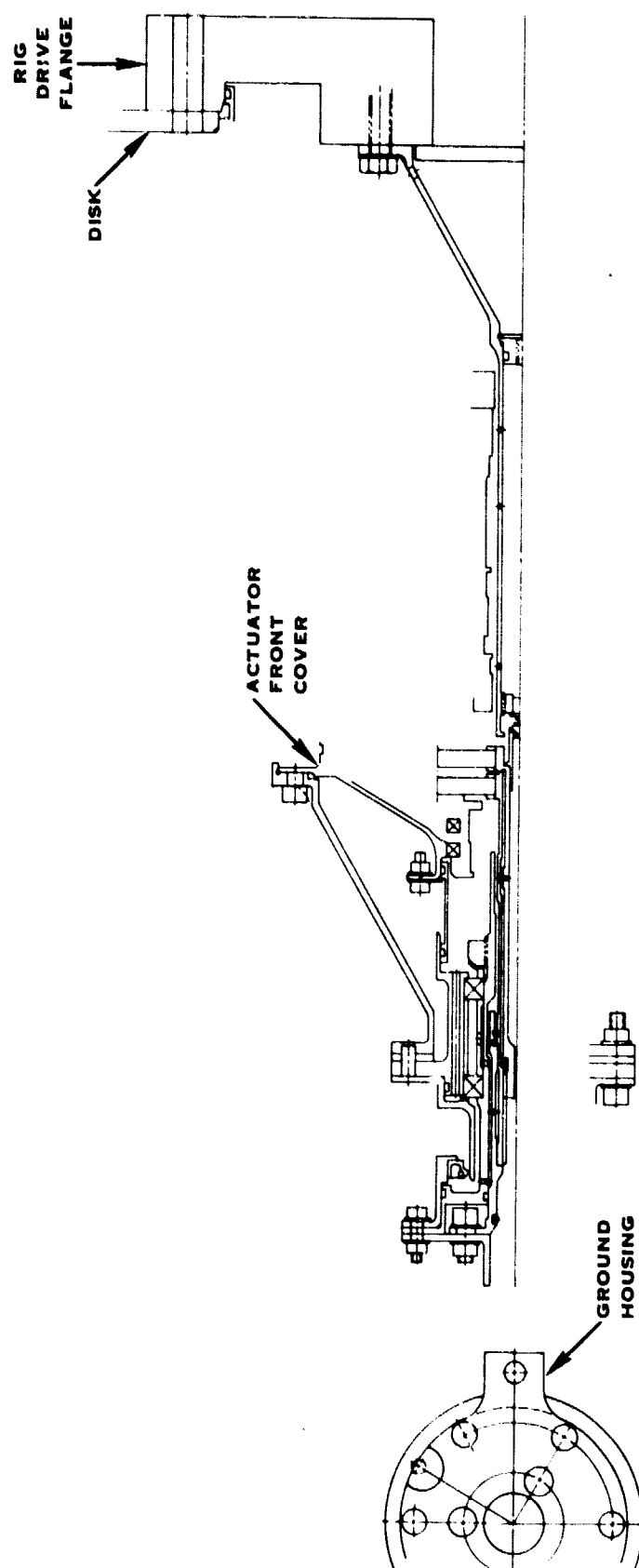


FIGURE 5. ASSEMBLY, FRONT INPUT HARDWARE

lubricating fluid. Initially, it was planned to use one Denison pump rated at 132.5 liters/min (35 gpm) at 3447.4 newtons/cm² (5000 psi) to supply change fluid for the majority of the testing, and to use a Denison pump rated at 94.6 liters/min in parallel with it for testing requiring high flow (maximum pitch change rates). Operating the two pumps proved to be quite difficult, so the second pump was replaced by an accumulator.

The instrumentation provided for the test is listed in Table I. The flex shaft speed was measured by machining a six tooth wheel on the feedback shaft in the beta regulator, and installing a magnetic pickup in the beta regulator housing.

The flex shaft torque was measured by strain gaging and calibrating the ground sun gear in the actuator.

Actual blade angle was measured using photo diode sensors to measure the relative position of the actuator cam and the disk. The output of the sensors was read by a phase meter.

Figure 6 is a photograph of the whirl rig installation.

A closed loop variable gain control system, modified from an existing unit, was used to operate the actuator.

The rig was operated in accordance with Operating Procedure 222PT-37. A copy of this procedure is included in Appendix A.

TABLE I
INSTRUMENTATION LIST

Measurement	Range	Accuracy
EHV Supply Pressure	0 - 4000 psig	± 40 psi
EHV Current Signal	± 100 ma	± 2.25% of reading
Flow to EHV	0 - 45 gpm	± 2.83% of full scale
ΔP Across-Motor	0 - 3500 psig	± 2.25% of full scale
Temperatures	0 - 300°F	± 2°F
Blade Angle Command	+20 to -120°	± 2% of full scale
LVDT Feedback Voltage	± 5 V dc	± 2% of full scale
Flex Shaft Speed	0 - 24,000 rpm	± 2.83% of full scale
Flex Shaft Torque	0 - 200 in lb	± 2.83% of full scale
Lube Oil Flow	0 - 1 qt/min	± 2% of reading
Lube Oil Pressure	0 - 100 psig	± 1 psi
Fan Speed	0 - 3700 rpm	± 2% of full scale
Vibration - Horizontal	0 - 30 mils	± 5% of reading
Vibration - Vertical	0 - 30 mils	± 5% of reading
Fan Blade Angle	+20 to -120°	± 0.2°

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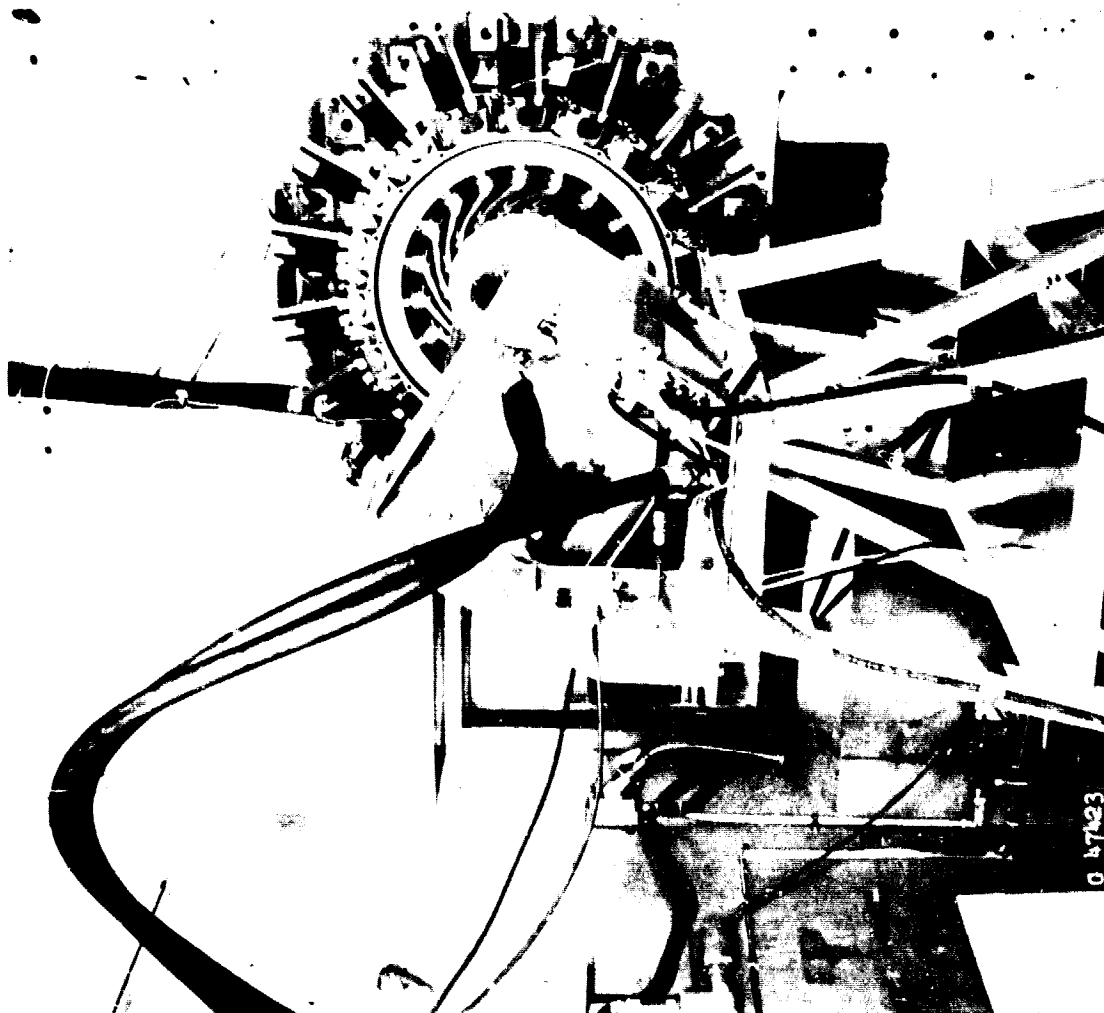
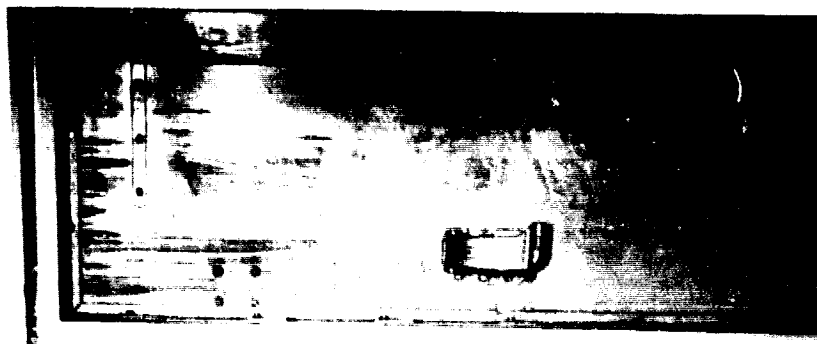


FIGURE 6. ACTUATOR IN WHIRL RIG

5.0

TEST PROCEDURE

The test was conducted essentially in accordance with Plan of Test 222PT-31 Rev. A. A copy of this plan is included in Appendix B. Variations from the Plan of Test are described below at the appropriate point in the test procedure description.

The test points in the plan are defined in terms of fan blade angle to be compatible with the specification. However, the stub blades supplied by General Electric were offset 25° relative to the blade angle in order to properly locate the peak twisting moment loads on the actuation system and a portion of the test data was recorded in terms of counterweight angles. The data is marked blade angle or counterweight angle, as appropriate, and the relationship between the two is that blade angle plus 25° equals counterweight angle. For the test, the counterweights were reindexed 2 spline teeth (18.5 degrees) from the design condition. This was done at the direction of General Electric to obtain more reverse blade angle.

The lubrication flow check was conducted with the flex shaft disconnected from the actuator. The flow from the shaft was measured at varying inlet pressures. Inlet pressure was measured at the pump.

The test was later repeated measuring the pressure at the inlet to the regulator and measuring the flow at the inlet to the flex shaft.

The LVDT null and calibration test was accomplished by changing blade angle with the manual pitch change input and measuring the counterweight angle. The blades were moved from "close" to "open" only.

The travel limit switch tests were accomplished by setting the controller to give a step command of approximately 30-40 degrees of blade angle which would actuate the travel limit switch. The pitch change rate was varied by regulating servo valve supply pressure and flow. The amount of overtravel was determined by physical measurement of the angle at which the counterweights stopped, compared with the angle at which the switch actuated. The testing was conducted at 0 fan rpm.

During early testing it was found that operation at the maximum pitch change rate overstressed the no-back output shaft. In order to continue testing, the maximum pitch change rate was limited to 75 degrees/second.

Initial running revealed a rig resonance at approximately 2500 fan rpm. To avoid this resonance, all testing specified at 2500 rpm was conducted at 2700 rpm.

5.0

(Continued)

The position accuracy test was conducted by setting blade angle with the controller and measuring actual blade angle. Because of the instrumentation accuracies in this test (controller setting, actual blade angle readout) an alternate static positioning accuracy test was also run. In this test, the blade angle feedback (LVDT's) were positioned with the manual input and the actual blade angle change was measured by a dial indicator and converted to angle change.

The test to determine the pressure and flow required to start and sustain actuator motion was conducted by commanding the desired change with no pressure to the servo valve, and then increasing the pressure to the valve until the blade angle change was complete.

The test to determine the minimum blade angle change around 0° was conducted by slowly changing the controller input until a change in LVDT feedback voltage was observed. The actual counterweight position was measured to determine that the blades had moved.

Frequency response testing was conducted with a two channel transfer function analyzer with automatic gain and sweep control and direct plot output. For the static testing, blade angle was measured by a proximity pickup set up on one of the stub blades.

The endurance test was conducted in accordance with Table II. The forward thrust test points were set manually, the modulating thrust points were run using an oscillator input to the controller, and the reverse/unreverse transients were step inputs to the controller. Initial cycles were conducted at approximately six per hour to preclude overheating the no-back. Since experience showed no evidence of heating on the no-back spring, the remaining cycles were conducted at a rate of ten to twelve per hour.

Following testing in accordance with Plan of Test 222PT-31 Rev. A, the actuator was modified by the addition of a snubber. Testing in accordance with Plan of Test 222PT-38 was then accomplished. A copy of this plan is included in Appendix B.

TABLE II
QCSEE ACTUATOR

Speed (rpm)	Blade Angle	DC Command Pot Setting	Feedback Gain	Step Command Set	Cond.
2700 (#3)	12°	309	325	9.81	ON
2700	-3°	205	↑ <		

*Plug in Function Gen. - Amp - Min
Freq - Range 0.1
Dial 1.9

Don't Forget to go to 2700 Prior to Unreverse.

≈ 10 min/cycle

5.0 (Continued)

These tests were conducted in the same manner as the tests of Plan of Test 222PT-31 Rev. A with the exception of the frequency response test. This test was conducted with a single channel transfer function analyzer. This unit did not have automatic gain and sweep control, or direct plot capability. The following test points were run rather than those listed in the plan of test.

Frequency (cps)	Servo Valve Current (ma)
0.5	$\pm 4 \pm 8$
1.0	$\pm 4 \pm 8$
2.0	$\pm 4 \pm 8 \pm 12$
3.0	$\pm 4 \pm 8 \pm 16$

6.0

TEST RESULTSStructural

During the test the following structural problems were noted with the hardware.

During the initial tests of the travel limit switches, after six actuations at pitch change rates up to 82 degrees/second, it was found that the no-back output shaft had fractured at the webs between the three windows. Figure 7 is a photograph of the shaft. The fracture of the shaft was attributed to the shaft being under-designed in this area for the expected load of 271.1 newton meters (2400 inch pounds). The shaft was repaired by electron beam welding, and "beefed" up in the area where it had fractured. In addition a new shaft was fabricated incorporating additional strengthening. The welded shaft (763494-1/222X575) was approximately twice as strong and the new shaft (763494-1 Chg. B) was four times as strong as the design which fractured. Figure 8 is a comparison of the three configurations.

Testing was resumed with the welded output shaft. Performance tests, including some running at high pitch change rates, and a total of 46 flight cycles were completed. The unit was disassembled for a routine inspection, and the welded output shaft was found to be fractured in two of the three webs.

Analysis of this incident revealed that the original design of the shaft did not take into account the torque generated by inertia of the no-back drum and brake hardware which must be accelerated up to speed when the actuator starts slowing down.

At pitch change rates of 135 degrees per second, this inertia raises the load on the shaft to 536.6 newton meters (4750 inch pounds). Further analysis revealed that even with the inertia reduced as much as feasible in the existing design, the output shaft could not be strengthened sufficiently within the space available. Consequently, testing with the new shaft was limited to a pitch change rate of 75 degrees per second.

After completion of 500 flight cycles, the new shaft (763494-1 Chg. B) was found to be cracked in the web area. Investigation of this incident including a static torque test of the system, revealed that the spring rate of the system was 5648.7 newton meters per radian (50,000 inch pounds per radian) rather than the calculated 2824.4 newton meters per radian (25000 inch pounds per radian). The higher spring rate raises the expected 271.1 newton meter load on the shaft at 75°/second pitch change rate, to 451.9 newton meters (4000 inch pounds).

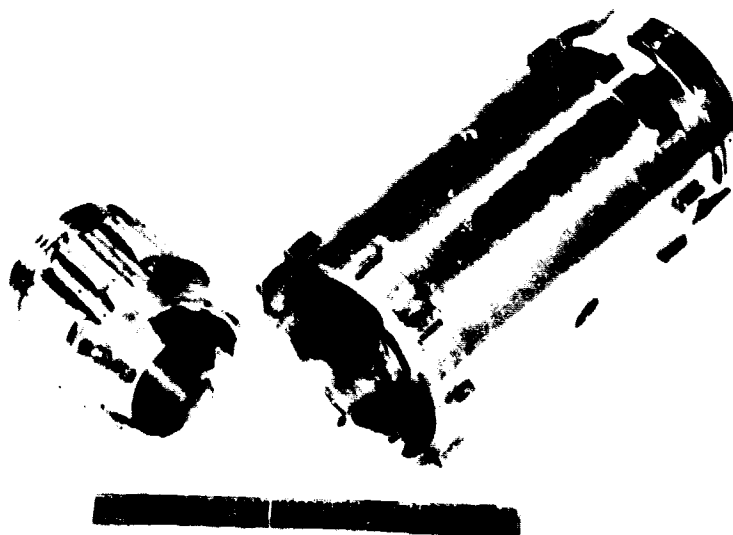


FIGURE 7. 763494-1 OUTPUT SHAFT

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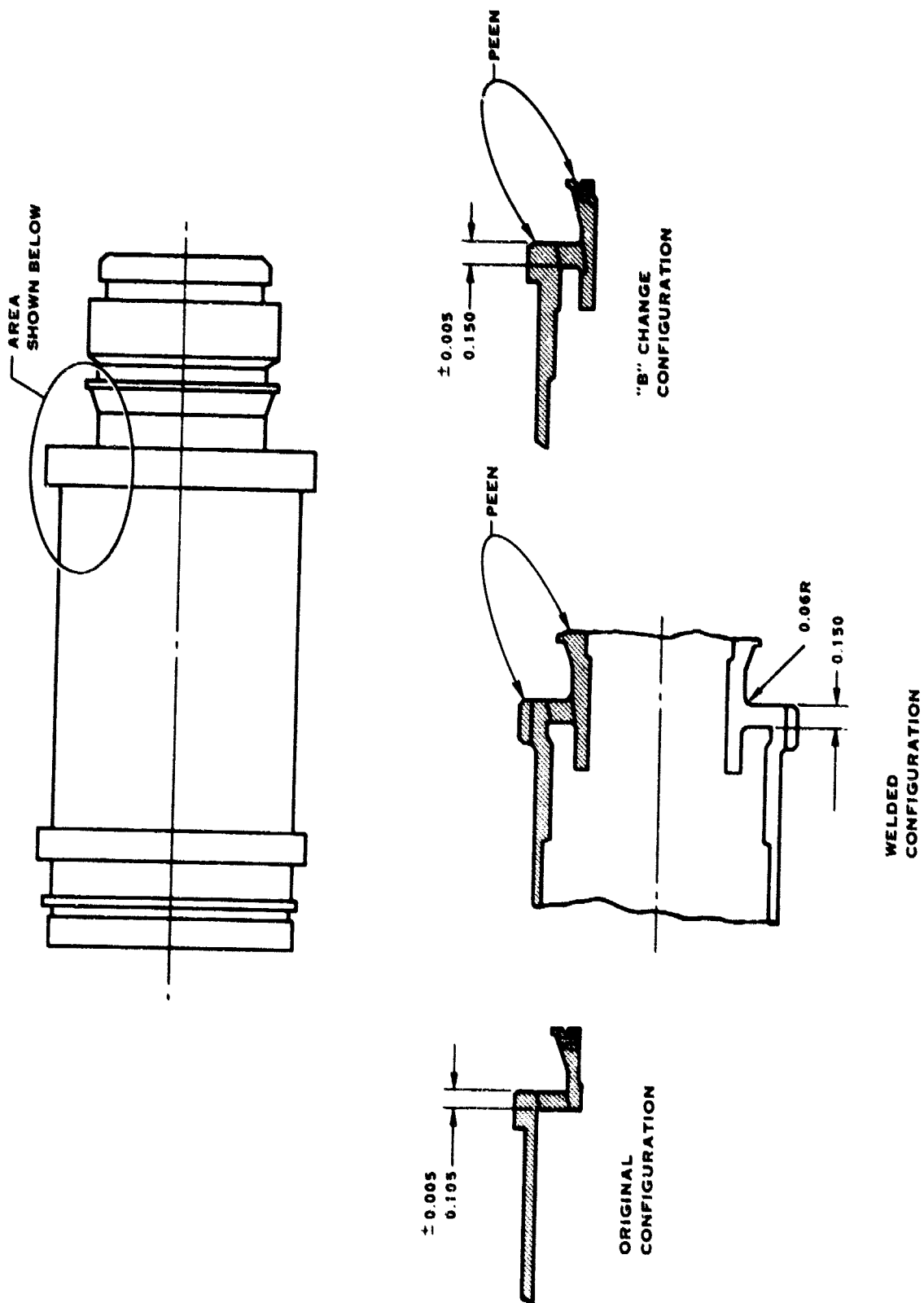


FIGURE 8. OUTPUT SHAFT COMPARISON

6.0 (Continued)

The difference between the calculated and actual system spring rates is the result of the coefficient of friction assumed between the no-back spring and the no-back drum. In the calculations, a lower than actual coefficient was used. This results in more engaged spring coils to absorb a given torque resulting in a greater spring deflection, and therefore a lower no-back spring rate.

To restore the actuators maximum pitch change rate capability, a snubber was designed and fabricated to reduce the spring rate of the system to 677.8 newton meters per radian (6000 inch pounds per radian), which reduced the output shaft load to 271.1 newton meters at the maximum pitch change rate of 135°/second.

Incorporation of the snubber results in the following life predictions for the output shaft and the snubber:

Maximum Flex Shaft Speed (rpm)	17,500	21,000
Snubber Fatigue Life (cycles)		
at room temperature	> 1,000	750
at 93.3°C (200°F)	1,000	500
Output Shaft Fatigue Life (cycles)		
at room temperature	5×10^4	1.5×10^4
at 93.3°C (200°F)	2.1×10^5	1×10^5

At the same time that the snubber was installed in the actuator, the no-back spring was replaced with a new part. This was done as a precautionary measure as the original spring had been subjected to higher than design loads during operation without a snubber.

Prior to, and following the testing of Plan of Test 222PT-38, the spring rate of the snubber was measured. The initial measurement revealed the actual spring rate to agree closely with the calculated rate (684.4 newton meters per radian [6067 inch pounds per radian] vs. 698.2 newton meters per radian [6180 inch pounds per radian]). The after testing check revealed no change in spring rate or other deterioration of the snubber.

6.0 (Continued)

During the initial spring rate check of the snubber, its deflection versus load was calibrated. A means of indicating relative motion during actuator operation was added to the snubber, and the deflection checked at various pitch change rates up to maximum. These measurements indicated that the snubber limited the load on the output shaft to the design value of 293.7 newton meters (2600 in lbs).

It was observed during the test that the wear pattern on the cam tracks was high in the track on one side, and low on the other. Inspection of the cam revealed that the sides of the tracks were not parallel to a radius through the center of the track. Subsequent running over the full range of speeds and loads has shown that this small abnormality in the pattern does not represent a significant problem and no corrective action was taken.

As a result of an assembly error, the rear support housing was fractured in the 'O' seal groove area that mates to the engine. This fracture extended about 3 inches circumferentially at the aft edge of the seal groove. The housing was repaired by removing the damaged area, electron beam welding a new ring onto the back of the housing, and remachining.

During the lubrication flow check it was found that oil leaked through the outer casing of the flex shaft at the junction with the end fittings. This was found to be a result of a drawing error which did not call for the teflon lining in the casing to be swaged between the casing and the end fittings. The second flex cable leaked slightly at the junction of one end fitting and the casing. This was attributed to a poor joint at the swage of the casing to the end fitting. For rig running, the conduit was sealed at the actuator and the drain hole plugged to contain the leakage.

At the completion of testing, the flex shaft core was deformed, apparently as a result of having been over-torqued. The distortion of the core during the over-torque also deformed the casing. Reference Figure 9. The over-torque was attributed to a shutdown during the travel limit switch tests from a pitch change rate of 130 degrees per second with a controller time constant of 10 milliseconds. The controller was modified to a time constant of 25 milliseconds, (system designed for 20-30) and subsequent shaft torques were measured to be within acceptable limits.

During the inspection following the completion of testing per 222PT-31 Rev. A, pitting and scoring were noted on the bevel gears and their pinion. The data received with the bevel gear set from the manufacturer had shown the final grind pattern to be marginal.

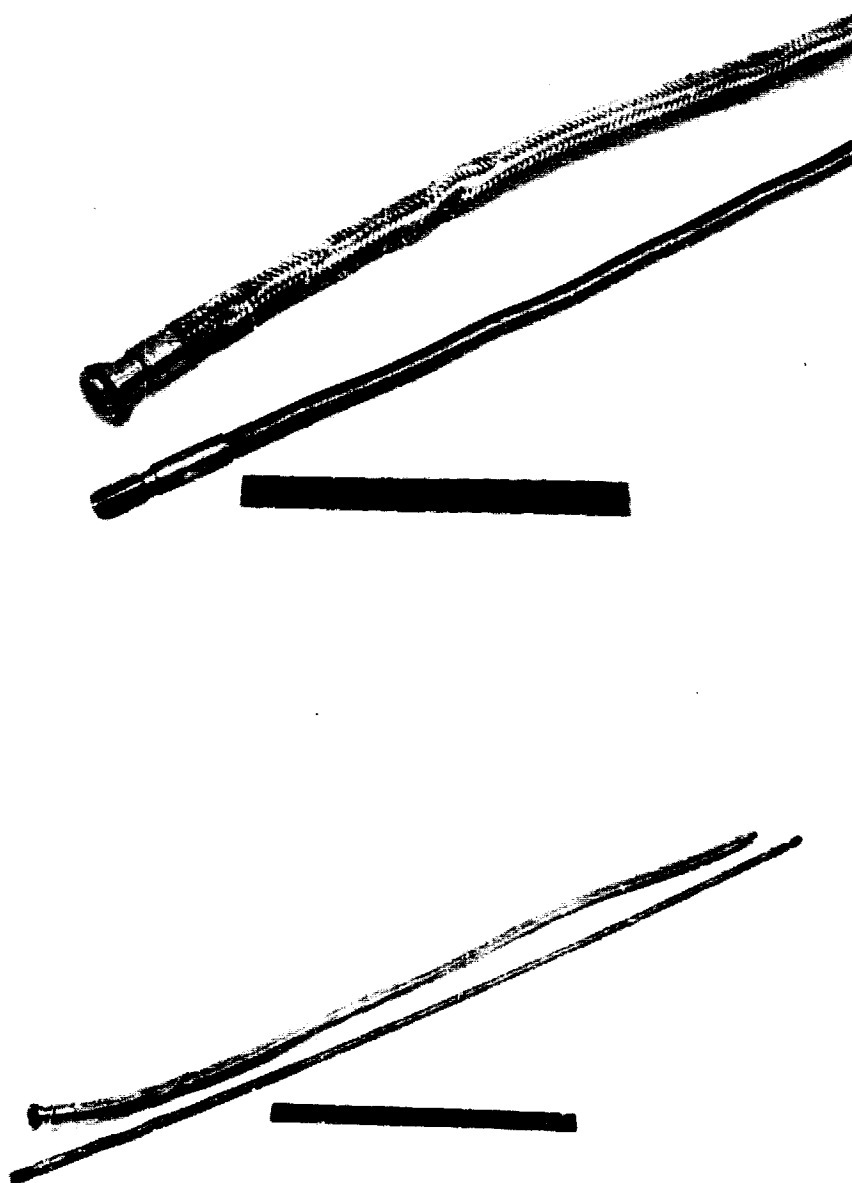


FIGURE 9. 763402-1 FLEXIBLE SHAFT

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6.0 (Continued)

During the course of the test, the gear pattern had been examined several times and always appeared to be high on the tooth. Consequently, the shimming of the pinion and gears was changed several times to bring them closer into mesh. As the parts are brought closer into mesh the backlash is reduced. The lubrication system for the beta regulator was designed to provide a mist to lubricate the gear mesh. As the backlash was reduced, this method of lubrication apparently became marginal. The gear set was replaced, and the regulator reworked to provide an oil jet which sprays directly into the gear mesh. The mesh was shimmed to insure sufficient backlash rather than attempting to center the pattern on the tooth.

During the disassembly of one of the hydraulic motors for inspection, the bearing housing was damaged by a faulty disassembly procedure. This motor was replaced by a new motor. Following the completion of the flight cycles conducted with the snubber, an attempt was made to conduct the frequency response test. With an input to the servo valve of ± 4 ma, no response was obtained from the actuator. The hydraulic motors were disassembled for inspection, and the new motor was found to exhibit heavy wear on the housing bore at the drive gear face. Dimensional inspection revealed no reason for this wear. Another motor was installed in the regulator, and the actuator then responded to current inputs to the servo valve of ± 4 ma.

All other hardware in the actuator and the regulator was in good condition following the tests. The hardware was subjected to magnaflux, zygo, and visual inspection following the completion of testing per Plan of Test 222PT-31 Rev. A, and visual inspection following testing per Plan of Test 222PT-38.

Performance

The lubrication flow check revealed that it took 63.8 newtons per square centimeter (92.5 pounds per square inch) at the lubrication pump to obtain a flow of 0.80 liters per minute (0.85 quarts per minute) out of the flex shaft. Figure 10 is a plot of the data taken during this test. A second check was made to determine the pressure required at the inlet to the regulator to obtain the required flow. This test showed that it took 42 newtons per square centimeter (61 pounds per square inch) to achieve the desired flow. The design value was 48 newtons per square centimeter (70 pounds per square inch). Figure 11 is a plot of the data taken during this test.

The results of the LVDT calibration tests showed the output voltages from the two LVDT's to be in close agreement. Table III is a summary of the data taken during the test where the blades were moved from "close" to "open", and Figures 12 and 13 are plots of output voltage versus blade angle.

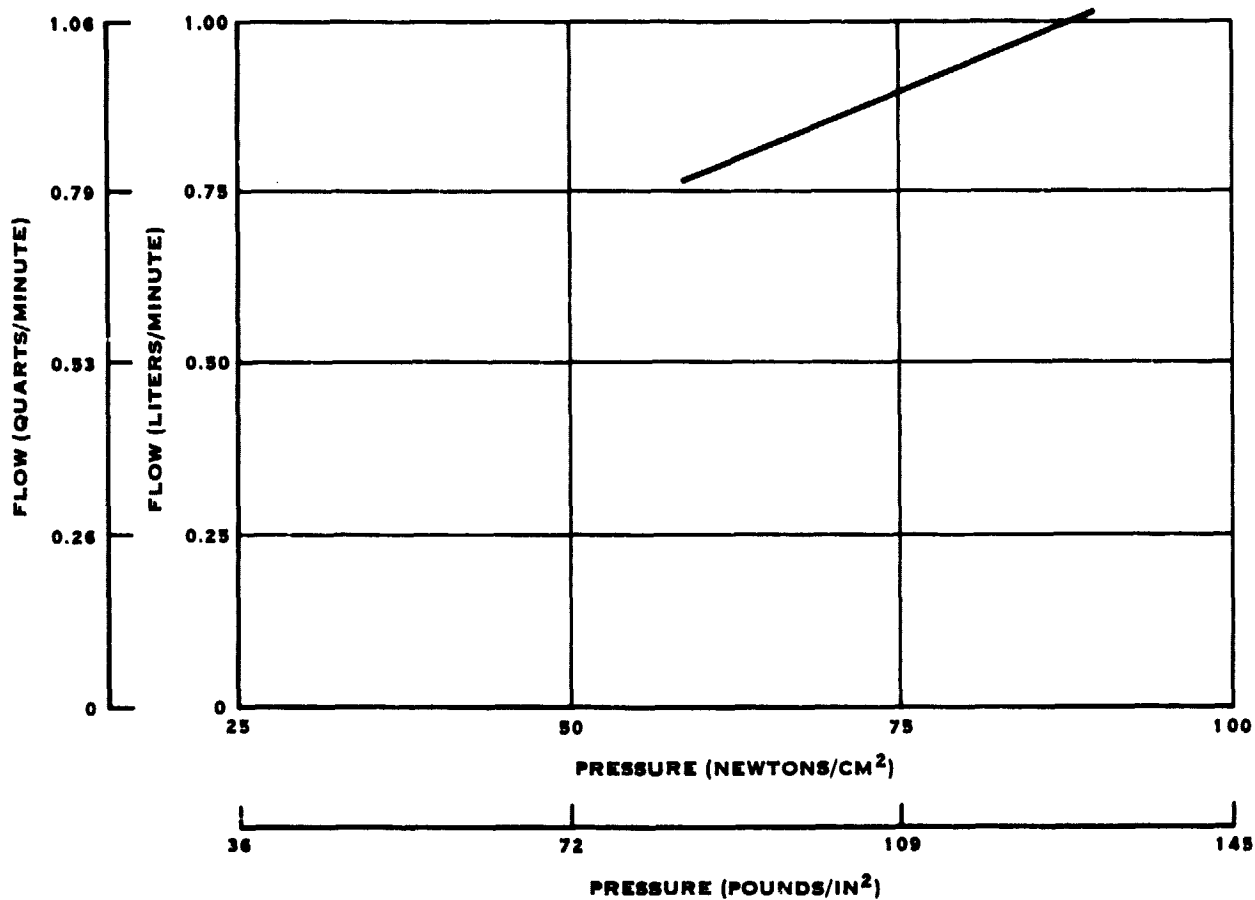


FIGURE 10. LUBRICATION FLOW CHECK FLOW VS. PRESSURE AT PUMP 11-10-75

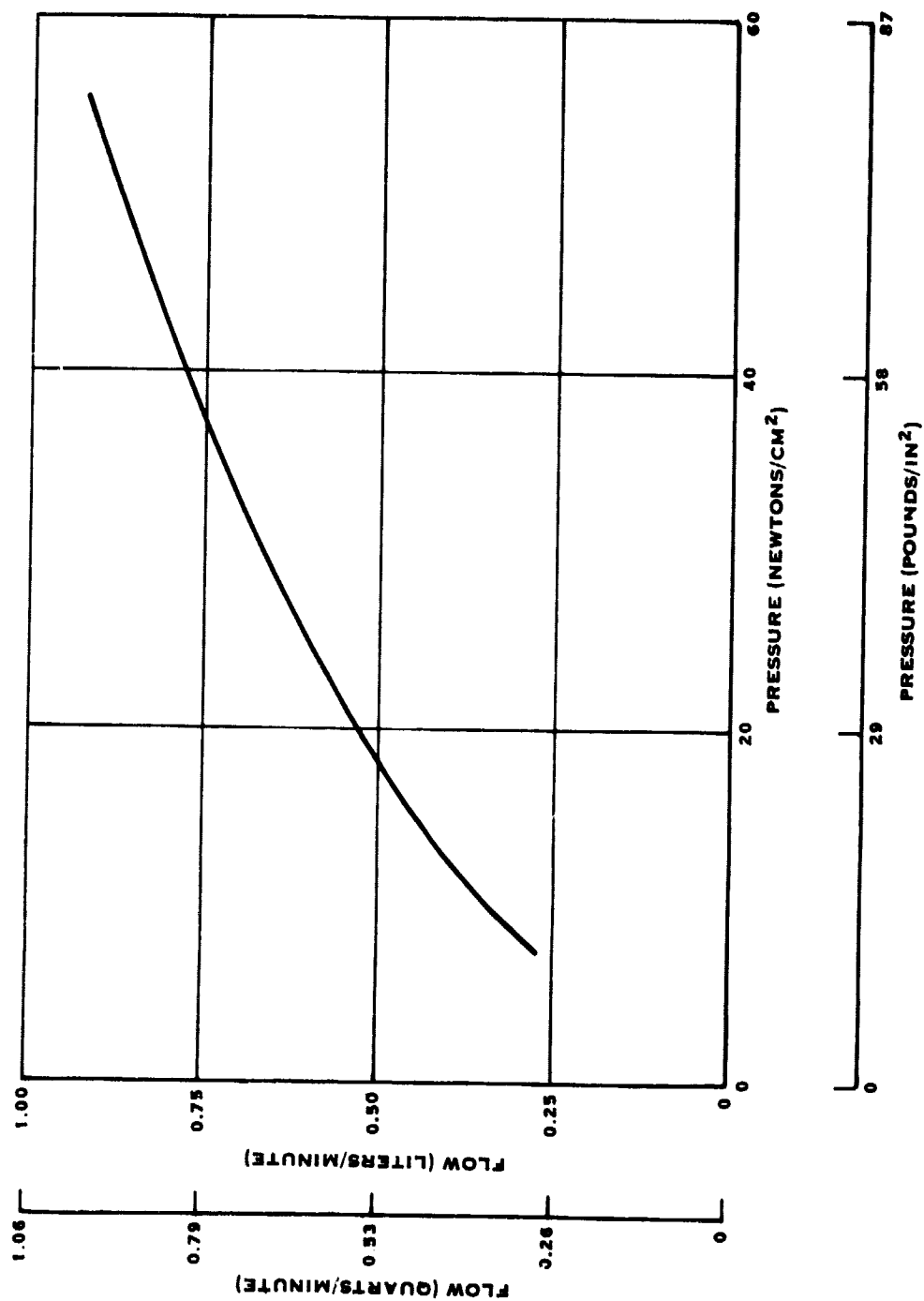


FIGURE 11. LUBRICATION FLOW CHECK - FLOW VS. PRESSURE AT REGULATOR 1-14-76

TABLE III
LVDT CALIBRATION

DATA FROM 11-10-75

Counterweight Angle	Blade Angle	Excitation Voltage	Output Voltage Total		Output Voltage Volts/Volt	
			LVDT1	LVDT2	LVDT1	LVDT2
*42.2	17.2	5.666	2.373	2.371	0.419	0.418
35.0	10.0	5.665	2.107	2.105	0.372	0.372
30.0	5.0	5.667	1.907	1.905	0.337	0.336
25.0	0	5.664	1.715	1.711	0.303	0.302
20.0	- 5.0	5.666	1.513	1.509	0.267	0.266
15.0	-10.0	5.667	1.307	1.305	0.231	0.230
10.0	-15.0	5.665	1.094	1.091	0.193	0.193
5.0	-20.0	5.666	0.893	0.890	0.158	0.157
0	-25.0	5.665	0.706	0.704	0.125	0.124
- 5.0	-30.0	5.665	0.518	0.517	0.091	0.091
-10.0	-35.0	5.666	0.345	0.342	0.061	0.060
-15.0	-40.0	5.665	0.184	0.183	0.032	0.032
-20.0	-45.0	5.664	0.034	0.033	0.006	0.006
-25.0	-50.0	5.665	-0.121	-0.121	-0.021	-0.021
-30.0	-55.0	5.665	-0.265	-0.265	-0.047	-0.047
-35.0	-60.0	5.665	-0.425	-0.425	-0.075	-0.075
-40.0	-65.0	5.665	-0.575	-0.574	-0.102	-0.101
-45.0	-70.0	5.665	-0.725	-0.725	-0.128	-0.128
-50.0	-75.0	5.665	-0.875	-0.873	-0.154	-0.154
-55.0	-80.0	5.665	-1.027	-1.027	-0.181	-0.181
-60.0	-85.0	5.665	-1.190	-1.187	-0.210	-0.210
-65.0	-90.0	5.665	-1.353	-1.351	-0.239	-0.238

TABLE III (Continued)
LVDT CALIBRATION

DATA FROM 11-10-75

Counterweight Angle	Blade Angle	Excitation Voltage	Output Voltage Total		Output Voltage Volts/Volt	
			LVDT1	LVDT2	LVDT1	LVDT2
-70.0	-95.0	5.665	-1.520	-1.514	-0.268	-0.267
-75.0	-100.0	5.665	-1.686	-1.683	-0.298	-0.297
-80.0	-105.0	5.665	-1.850	-1.847	-0.327	-0.326
-85.0	-110.0	5.665	-2.007	-2.003	-0.354	-0.354
-90.0	-115.0	5.665	-2.153	-2.150	-0.380	-0.380
-95.0	-120.0	5.665	-2.290	-2.284	-0.404	-0.403
*-98.7	-123.7	5.665	-2.382	-2.378	-0.420	-0.420

*Mechanical Stop

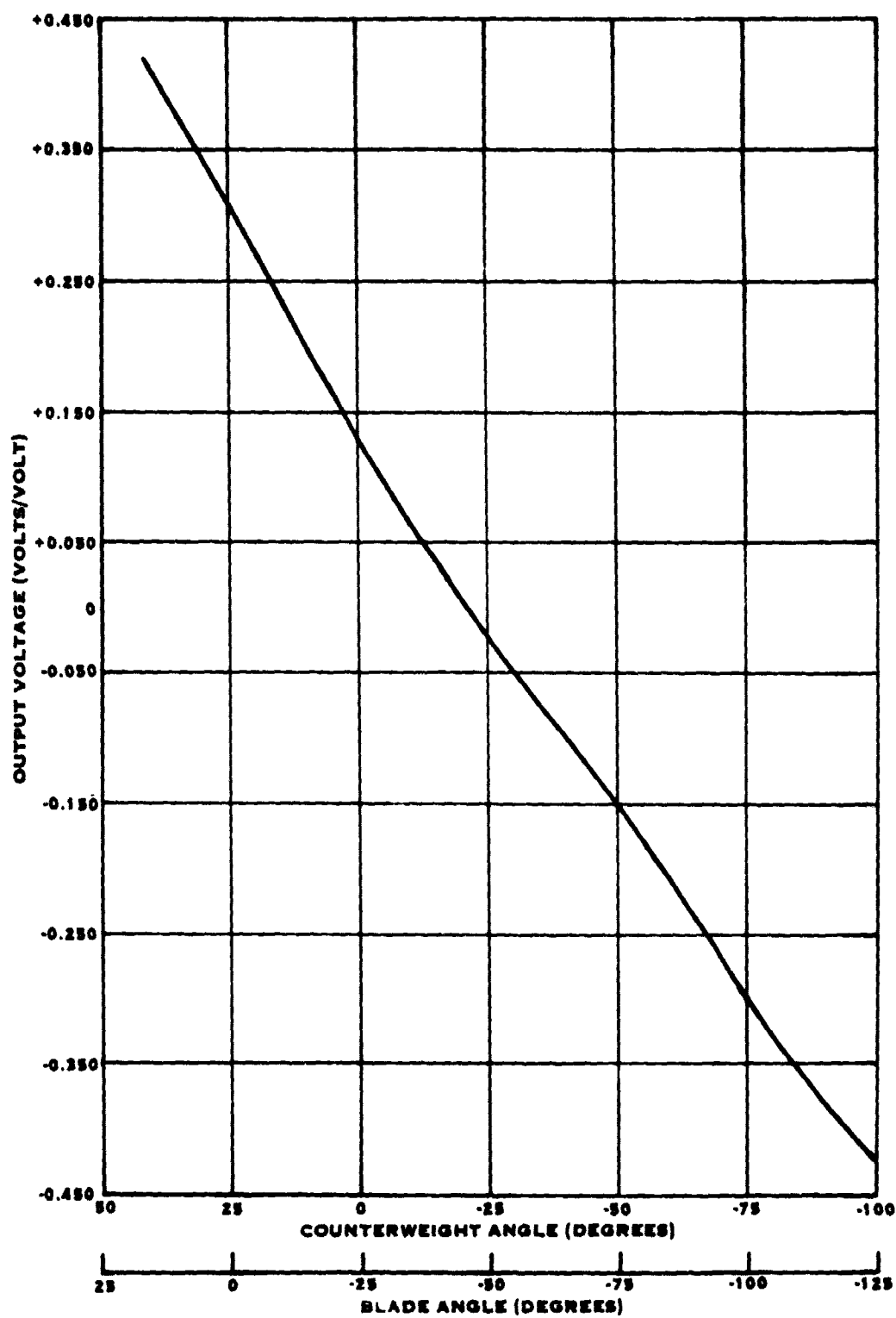


FIGURE 12. OUTPUT VOLTAGE VS. BLADE ANGLE LVDT #1 11-10-75
DATA TAKEN FROM CLOSE TO OPEN

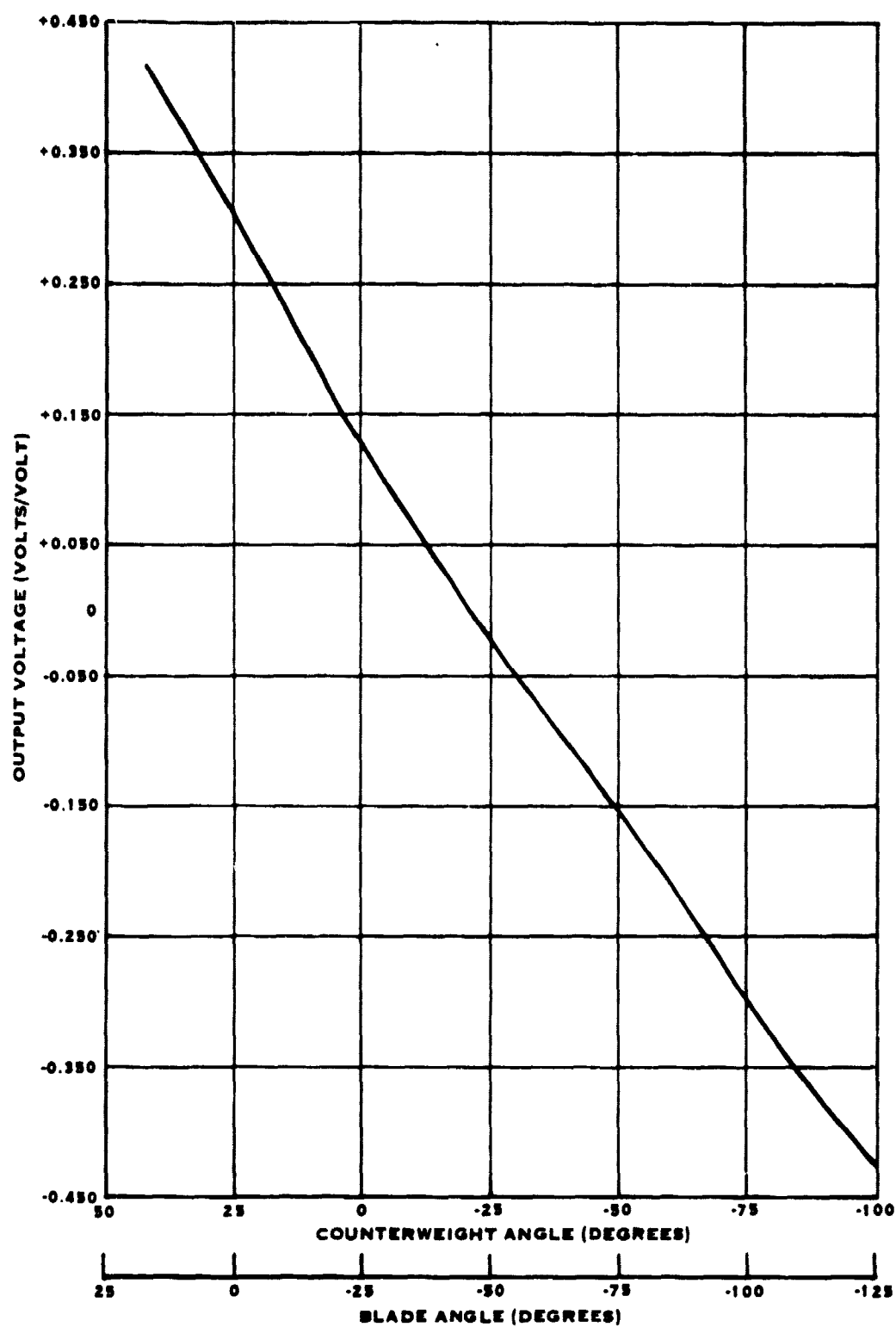


FIGURE 13. OUTPUT VOLTAGE VS. BLADE ANGLE LVDT #2 11-10-75
DATA TAKEN FROM CLOSE TO OPEN

6.0

(Continued)

The data available from the travel limit switch tests indicates that the blade overtravel after a switch actuation at maximum pitch change rate was within the calculated value (6.5° - 7.0°), when the data is adjusted for the higher pitch change rate and the effect of the motor back pressure is taken into account.

Table IV is a summary of the data taken during the tests. The data shows that the overtravel and the flex shaft torque are greater at the open end of travel than at the close end. The reason for this has not been determined. Overtravel and flex shaft torque are a function of the pitch change rate, the servo valve time constant, and the drag torque of the torque limiter brake. The higher the pitch change rate, the greater the overtravel and the higher the shaft torque. The greater the valve time constant, the greater the overtravel and the lower the shaft torque. The higher the drag of the torque limiter, the less the overtravel and the lower the shaft torque. Figure 14 is a curve of calculated overtravels and torques versus valve time constants.

In setting the torque limiter brake drag, variations amounting to 1 n-m (10 in. lb) of flex shaft torque from one direction to the other occurs. This does not account for the differences noted in the test. It is felt that the difference is a result of different dynamics in the no-back operation from one direction to the other. Sanborn traces of a travel limit switch stop at both the open and close ends of travel are included in Appendix C.

The rotating blade angle position accuracy test showed a maximum deviation of 1.5° between the set (LVDT) blade angle and the angle determined by the photo diode system. Tables V, VI, and VII are summaries of the data. The deviation noted is within that expected based on estimates of the mechanical and hydraulic hysteresis, the accuracy of the LVDT calibration, and the accuracy of the photo diode system. The three points which show the photo diode sensor angle to be closer to open than the LVDT angle are considered to be bad data points and should be ignored.

The static blade angle position accuracy test showed that the correlation between the set and resultant blade angles were good. In the close direction over a 4° range from 2° open to 2° close the resultant angle deviated from the set angle by a total of 0.25° . This deviation is within the accuracy of the LVDT calibration.

The test also showed that there is slightly less than 1 degree of hysteresis in the system when reversing the direction of blade angle change. This is somewhat greater than the expected value of 0.79 degrees. The expected value consists of a mechanical error of 0.48 degrees, a feedback backlash

**TABLE IV
TRAVEL LIMIT SWITCH**

DATA FROM 2-13-75

Step Blade Angle Command

Time Constant = 25 milliseconds

Fan Speed = 0 rpm

Blade Angle Travel Prior to Stop - 30 degrees

Actuator with Snubber

<u>Switch Setting</u>		Beta Stop (degrees)	Beta Overtravel (degrees)	Pitch Change Rate (degrees/sec)	<u>Peak Shaft Torque</u>	
Open (degrees)	Close (degrees)				(in-lbs)	(N-m)
-115.1		-119.0	3.9	101.2	260	29.4
		-120.5	5.4	106.5	300	33.9
		-121.1	6.0	116.2	340	38.4
	+10.2	+12.3	2.1	103.2	230	26.0
		+15.5	5.3	123.8	250	28.2
		+15.6	5.4	123.8	250	28.2

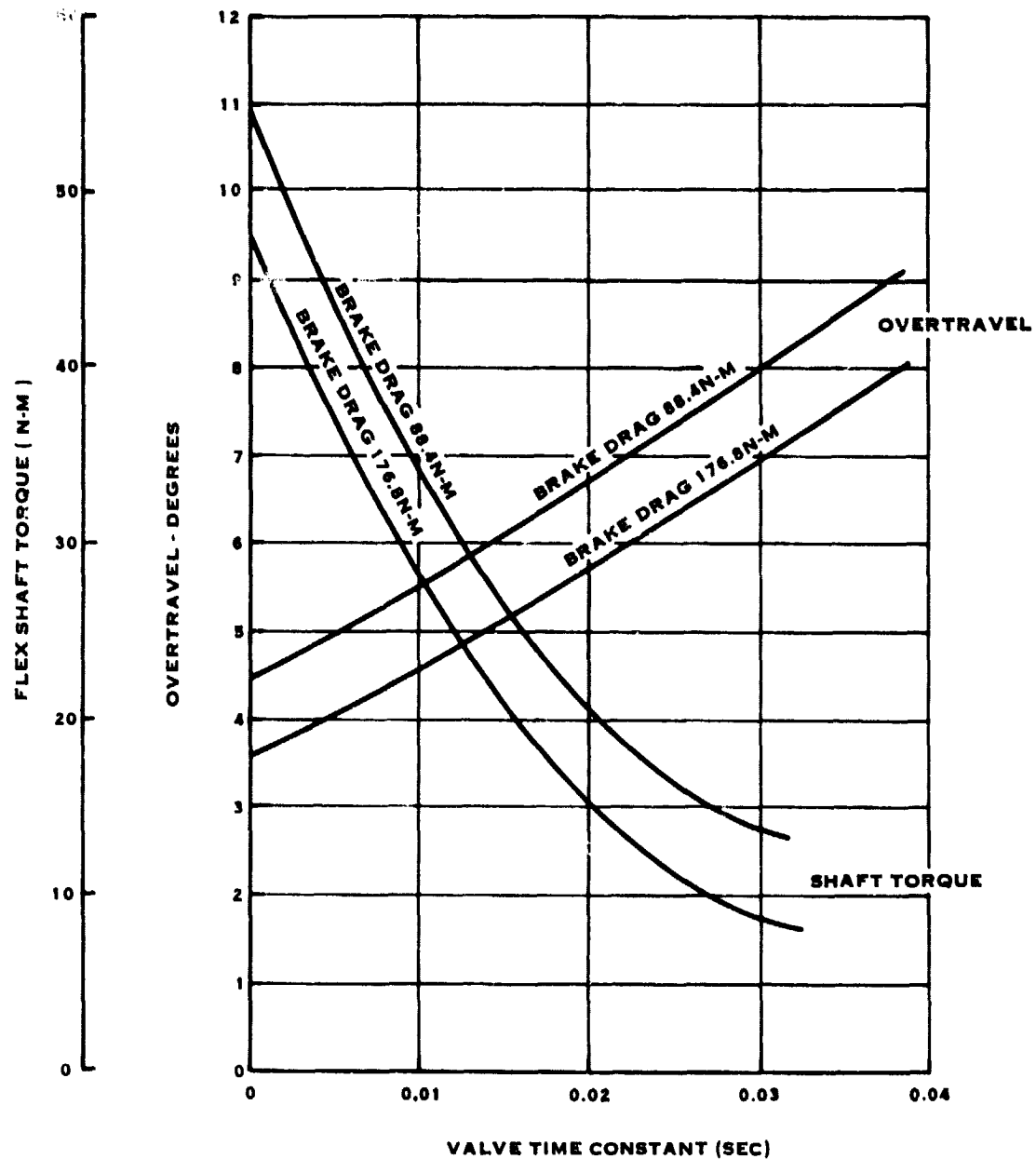


FIGURE 14. CURVE - OVERTRAVEL & SHAFT TORQUE VS VALVE TIME CONSTANT

TABLE V
 ANGLE POSITION ACCURACY
 (ROTATING)
 DATA FROM 12-30-75

	Photo Diode Blade Angle <u>(degrees)</u>	Fan Speed <u>(rpm)</u>
	+ 13.0	2700
	- 2.5	3068
	+ 0.8	3068
	+ 8.0	3068
	+ 4.0	3068
	+ 7.5	3068
	+ 9.5	3068
	+ 7.5	3068
00	-100.5	3068
12.0	+ 13.0	3068

TABLE VI
BLADE ANGLE POSITION ACCURACY
(ROTATING)
DATA FROM 12-30-75

<u>LVDT Blade Angle (degrees)</u>	<u>Photo Diode Blade Angle (degrees)</u>	<u>Fan Speed (rpm)</u>
+12.0	+13.0	2700
- 3.0	- 2.2	2700
0	+ 1.0	2700
+ 7.0	+ 8.5	2700
+ 5.0	+ 6.0	2700
+ 7.0	+ 8.0	2700
+ 9.0	+10.0	2700
+ 7.0	+ 8.0	2700
- 100	-99.5	2700
+12.0	+13.5	2700

TABLE VII
BLADE ANGLE POSITION ACCURACY
(ROTATING)

DATA FROM 12-31-75

<u>LVDT Blade Angle (degrees)</u>	<u>Photo Diode Blade Angle (degrees)</u>	<u>Fan Speed (rpm)</u>
+12.0	+13.0	3068
+ 9.0	+10.5	3068
+ 7.0	+ 8.0	3068
+ 5.0	+ 6.0	3068
0	+ 0.5	3068
- 3.0	- 2.0	3068
- 100	-99.5	3068
- 3.0	- 2.5	3068
0	- 1.0	3068
+ 5.0	+ 5.5	3068
+ 7.0	+ 8.0	3068
+ 9.0	+10.0	3068
+12.0	+13.0	3068

6.0 (Continued)

of 0.07 degrees, a backlash of the trunnion roller to the cam track of 0.14 degrees, and a calibration inaccuracy of 0.10 degrees. The reason for the difference between the measured and expected value is not known, but could be the result of larger than designed mechanical errors or backlash.

Figure 15 is a sketch of the test setup, Table VIII is a summary of the data taken during the test, and Figure 16 is a plot of the data. It should be noted that this is the maximum hysteresis and would only occur at full reverse during normal operation. During forward thrust operation, the actuator is always loaded towards close.

The results of testing to determine the pressure required to start and sustain blade motion are listed in Table IX. In those cases where more than one set of data is given for an excursion, the blades moved a few degrees, stopped, and then moved again as pressure was raised. The data given as "To Sustain" should have been taken when the blades were moving at a constant rate. As most of the excursions were very short, this was not the case. Even in the excursions to and from reverse, the motor flow could not be restricted enough for a constant pitch change rate to be established. The data given for sustaining was taken at a point where the pressure was constant, or almost constant, for a short period of time. The pressures required to start and sustain motion was well within the 3000 psi available for all cases tested. Sanborn traces of this test are included in Appendix C.

Actuator efficiency was determined at the input to the differential gear train where the actual torque on the ground sun gear was measured. Efficiencies were calculated based on data obtained during transient operation of the pitch change actuator. Since these were not steady state pitch change rates, the possibility of errors in the absolute numbers are greater and the results should therefore be used in a manner which reflects this possibility. The efficiencies determined were higher than anticipated, and were in the 70% range. The following tabulation summarizes the measured efficiencies.

Blade Angle (deg)	Direction of Motion	Fan Speed (rpm)	Efficiency (%)
-110	Open	3000	76
-100	Close	3000	73
- 66	Close	2500	71
- 50	Close	2350	75
+ 10	Open	2500	73

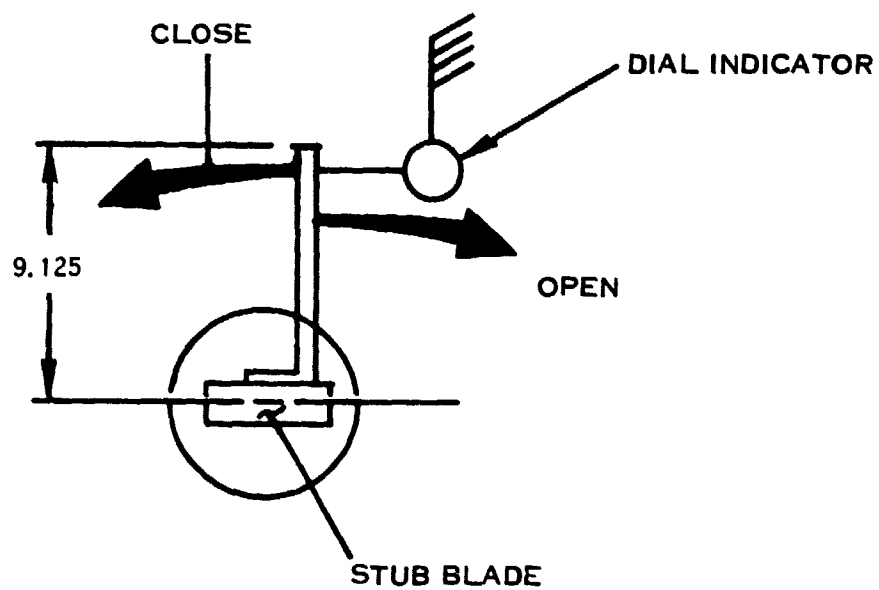


FIGURE 15. TEST SETUP BLADE ANGLE POSITIONING ACCURACY (STATIC)

TABLE VIII
BLADE ANGLE POSITION ACCURACY
STATIC
DATA FROM 2-14-76
BASED ON LVDT #1 CALIBRATION 2-5-76

LVDT Reading (volts)	Set Blade Angle (degrees)	Dial Indicator Reading (inches)	Δ Dial Indicator Reading (inches)	Δ Blade Angle (degrees)	Resultant Blade Angle (degrees)
1.670	-2.000	0.758	0	0	-2.000
1.678	-1.787	0.730	0.028	0.176	-1.824
1.686	-1.574	0.690	0.040	0.250	-1.574
1.693	-1.387	0.666	0.024	0.151	-1.423
1.700	-1.200	0.638	0.028	0.176	-1.247
1.708	-0.987	0.612	0.026	0.163	-1.084
1.715	-0.800	0.582	0.030	0.188	-0.896
1.723	-0.587	0.548	0.034	0.213	-0.683
1.730	-0.400	0.522	0.026	0.163	-0.520
1.738	-0.187	0.486	0.036	0.226	-0.294
1.745	0	0.461	0.025	0.157	-0.137
1.753	+0.213	0.426	0.035	0.220	+0.083
1.760	+0.400	0.400	0.026	0.163	+0.246
1.768	+0.613	0.369	0.031	0.195	+0.441
1.776	+0.826	0.335	0.034	0.213	+0.654
1.784	+1.039	0.306	0.029	0.182	+0.836
1.791	+1.226	0.280	0.026	0.163	+0.999
1.798	+1.413	0.253	0.027	0.170	+1.169

TABLE VIII (Continued)

LVDT Reading (volts)	Set Blade Angle (degrees)	Dial Indicator Reading (inches)	Δ Dial Indicator Reading (inches)	Δ Blade Angle (degrees)	Resultant Blade Angle (degrees)
1.805	+1.600	0.225	0.028	0.176	+1.345
1.813	+1.813	0.189	0.036	0.226	+1.571
1.820	+2.000	0.160	0.029	0.182	+1.753
1.813	+1.813	0.160	0	0	+1.753
1.805	+1.600	0.160	0	0	+1.753
1.798	+1.413	0.160	0	0	+1.753
1.791	+1.226	0.160	0	0	+1.753
1.784	+1.039	0.158	0.002	0.013	+1.740
1.776	+0.826	0.183	0.025	0.157	+1.583
1.768	+0.613	0.213	0.030	0.188	+1.395
1.760	+0.400	0.245	0.032	0.201	+1.194
1.753	+0.213	0.276	0.031	0.195	+0.999
1.745	0	0.306	0.030	0.188	+0.811
1.738	-0.187	0.332	0.026	0.163	+0.648
1.730	-0.400	0.365	0.033	0.207	+0.441
1.723	-0.587	0.390	0.025	0.157	+0.284
1.715	-0.800	0.426	0.036	0.226	+0.058
1.708	-0.987	0.457	0.031	0.195	-0.137
1.700	-1.200	0.488	0.031	0.195	-0.332
1.693	-1.387	0.515	0.027	0.170	-0.502
1.686	-1.574	0.540	0.025	0.157	-0.659
1.678	-1.787	0.573	0.033	0.207	-0.866
1.670	-2.000	0.606	0.033	0.207	-1.073

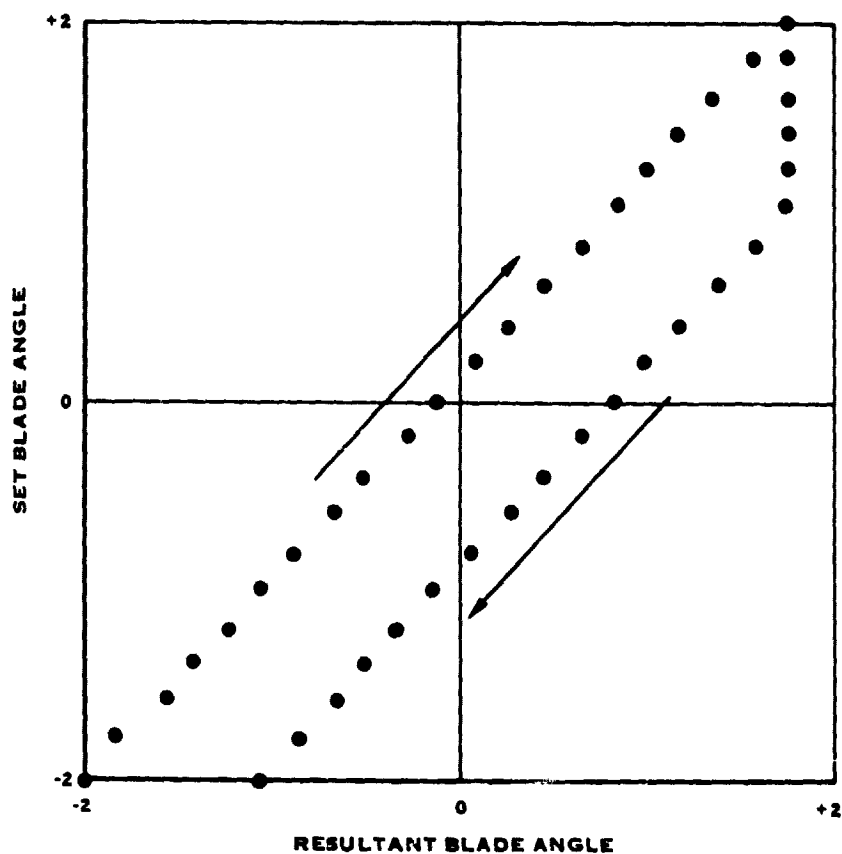


FIGURE 16. BLADE ANGLE POSITION ACCURACY DATA FROM 2-14-76
SET BLADE ANGLE VS. RESULTANT BLADE ANGLE

TABLE IX. PERFORMANCE

Data from 12-31-75

Blade Angle Excursion (degrees)	Fan Speed (rpm)	Pressure to		Torque to		Pitch Change Rate (max) (degrees/ sec)				
		Start Motion (psig)	(newtons/ cm ²) (psig)	Sustain Motion (newtons/ cm ²) (in-lb)	Start Motion (newton meter) (in-lb)		Sustain Motion (newton meter)			
+12 to -3	2700	950	655.0	1000	689.4	22	2.5	34	3.8	3.75
(+10.5)	2700	1100	758.4	1100	758.4	26	2.9	40	4.5	22.5
-3 to 0	3408	400	275.8	250	172.4	4	0.5	6	0.7	11.25
0 to +7	3068	450	310.2	250	172.4	4	0.5	10	1.1	18.75
+7 to +5	3068	1600	1103.1	1000	689.4	50	5.6	42	4.7	7.5
+5 to +7	3068	400	275.8	200	137.9	4	0.5	4	0.5	3.75
+7 to +9	3068	300	206.8	200	137.9	4	0.5	6	0.7	11.25
+9 to +7	3068	1000	689.4	1000	689.4	50	5.6	40	4.5	5.25
	3068	1500	1034.2	1200	827.3	76	8.6	60	6.8	11.25
+7 to -100	3068	1600	1103.1	400	275.8	50	5.6	4	0.5	75.0
-100 to +7	2700	1000	689.4	1000	689.4	18	2.0	34	3.8	22.5
	2700	1600	1103.1	1000	689.4	42	4.7	20	2.3	67.5

6.0 (Continued)

The average pitch change rate for a blade angle excursion from -3 degrees to -100 degrees at 3315 fan rpm with a EHV supply pressure of 2378.6 ± 34.4 newtons per square centimeter (3450 ± 50 psig) was 116 degrees per second. The maximum rate attained was 135 degrees per second. A Sanborn trace of this test is included in Appendix C. The design objective was 135 degrees per second maximum.

The minimum blade angle change which could be achieved around 0 degrees with a fan speed of 3408 rpm and a EHV supply pressure of 2378.6 ± 34.4 newtons per square centimeter (3450 ± 50 psig) was 0.17 degrees in the open direction and 0.26 degrees in the close direction based on LVDT motion. The design objective was 0.5 degrees.

With the blade angle set at -100 degrees, EHV supply pressure at 0, and the fan speed increased from 0 to 3578 rpm, no blade angle change occurred based on LVDT readout indicating that the no back mechanism did not slip.

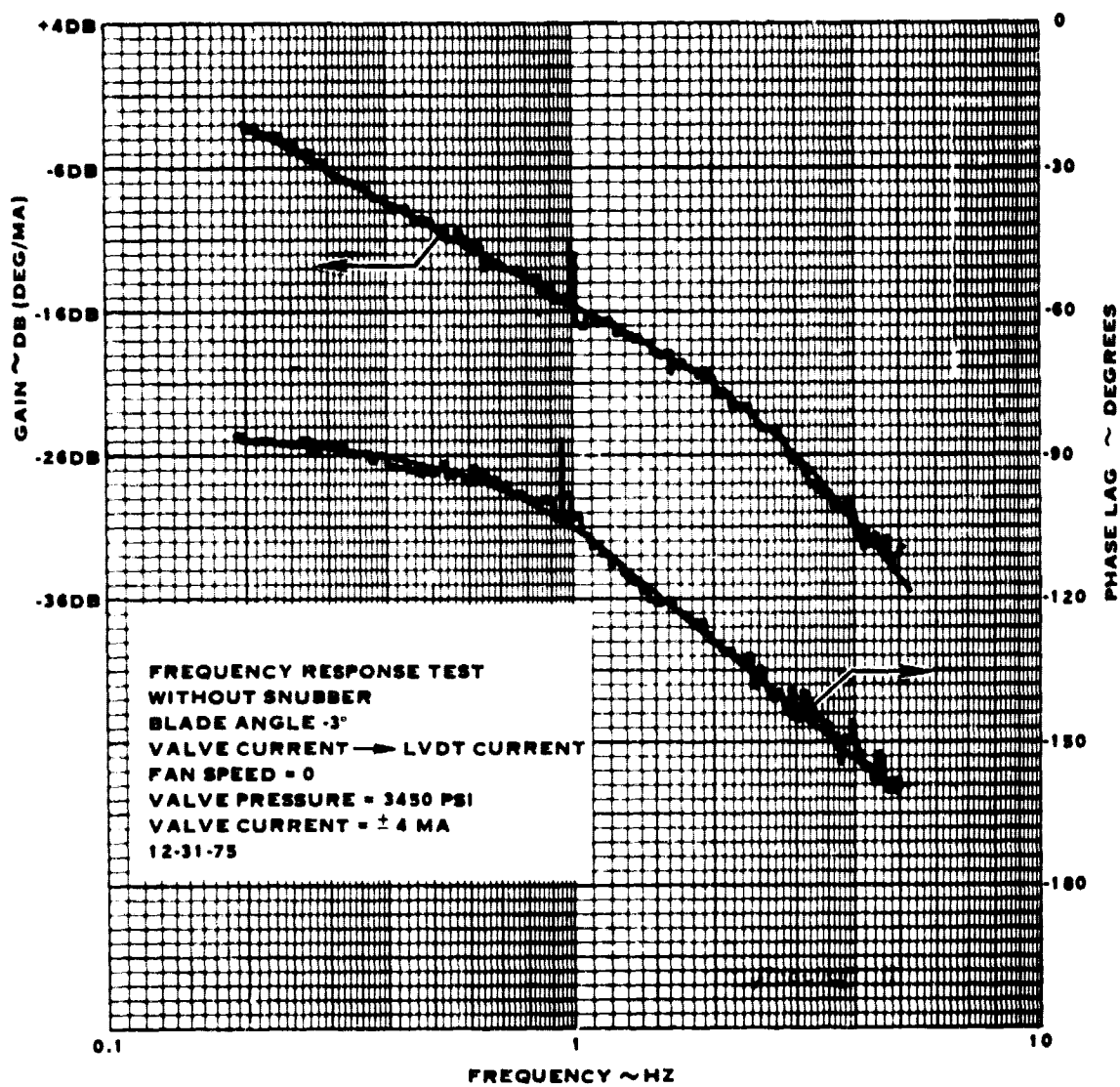
With the blade angle set at 0 degrees, EHV supply pressure at 0, and fan speed increased from 0 to 3408 rpm, no blade angle change occurred based on LVDT readout indicating that the no back mechanism did not slip.

The results of the frequency response testing are presented in Figures 17 through 22. The data in Figures 17 through 20 is for the actuator without a snubber while the data in Figures 21 and 22 is for the actuator with a snubber. In general, the actuator without the snubber indicated reasonable correlation with the predicted performance in the frequency range up to 1 Hertz; magnitude ratio was lower and phase shift was higher than at frequencies above 1 Hertz. The actuator with the snubber indicated reasonable correlation in the frequency range up to 1 Hertz when excitation magnitudes were ± 8 ma. However for ± 4 ma excitation the magnitude ratio was down and there was considerable phase shift.

Possible causes of the deviation between the test results and the design intent are high internal leakage in the hydraulic motors, higher than anticipated friction values, and lags due to the snubber.

A total of 500 endurance cycles at pitch change rates up to 75 degrees/second, were conducted on the actuator prior to installation of the snubber, and an additional 50 cycles at pitch change rates up to 135 degrees/second after snubber installation. Sanborn traces of a typical cycle are included in Appendix C.

Copies of the log sheets generated during the test are included in Appendix D, and a test chronology is included in Appendix E.



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FIGURE 17. QCSEE FREQUENCY RESPONSE

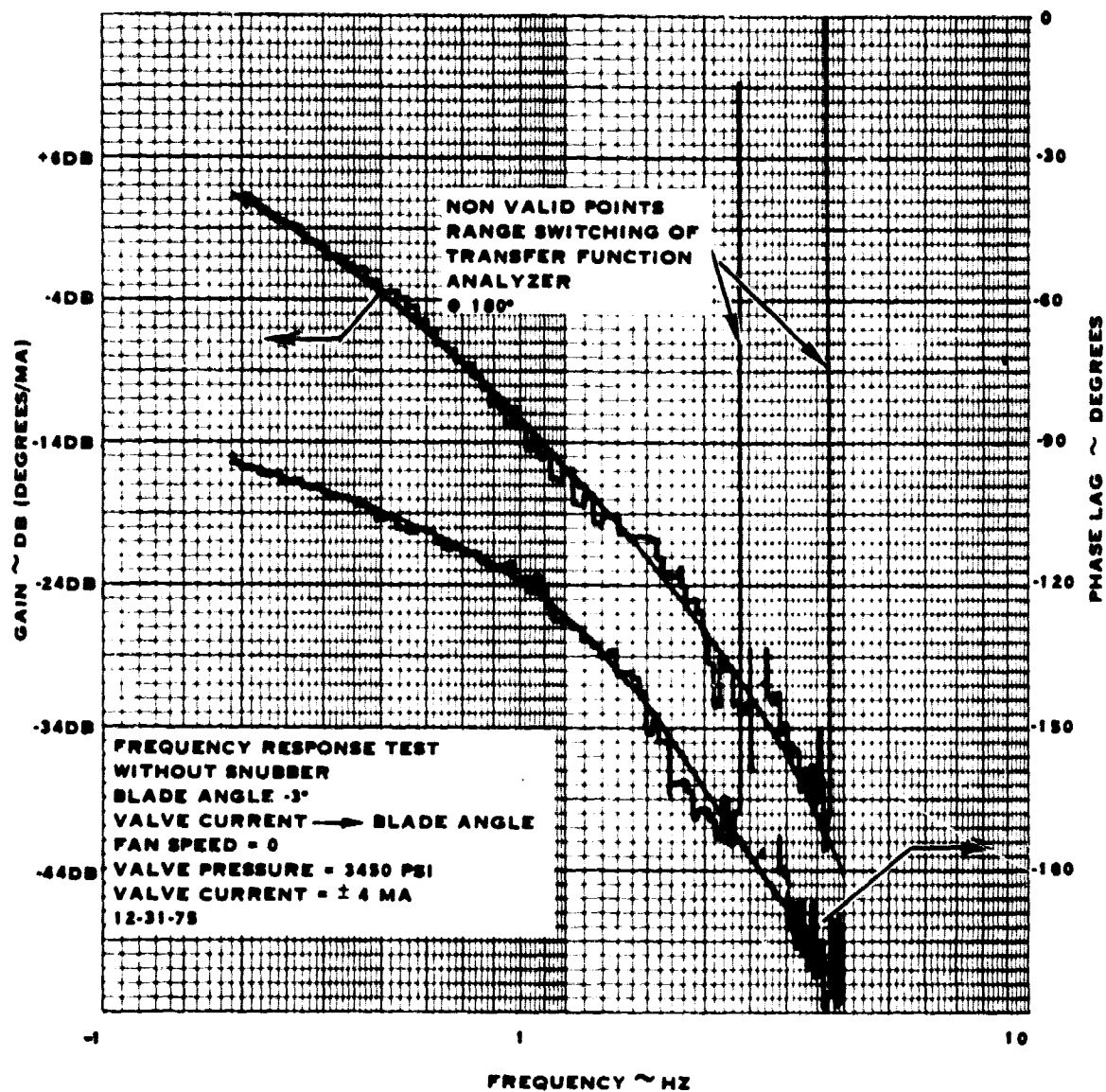


FIGURE 18. QCSEE FREQUENCY RESPONSE

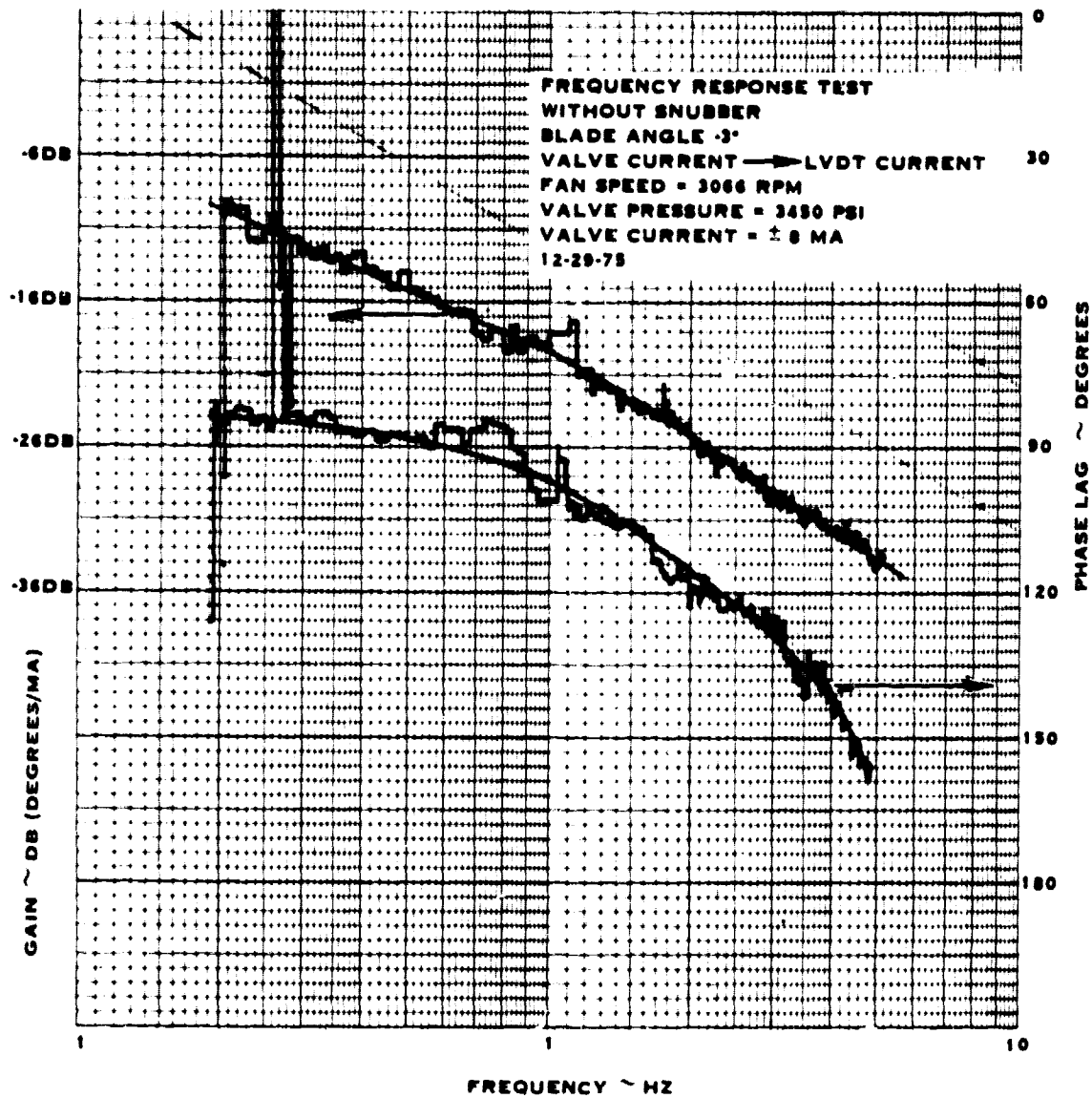


FIGURE 19. QCSEE FREQUENCY RESPONSE

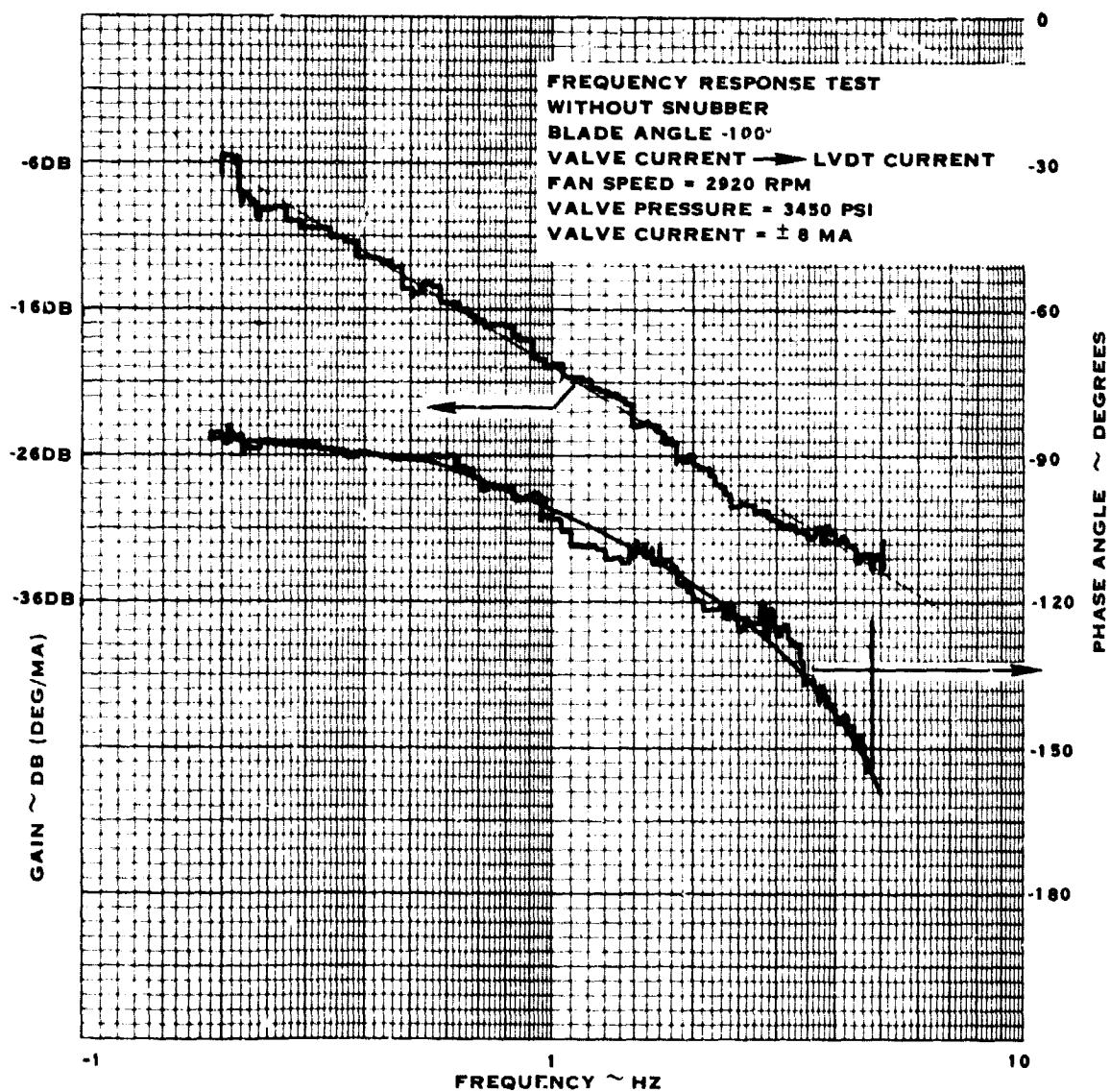


FIGURE 20. QCSEE FREQUENCY RESPONSE

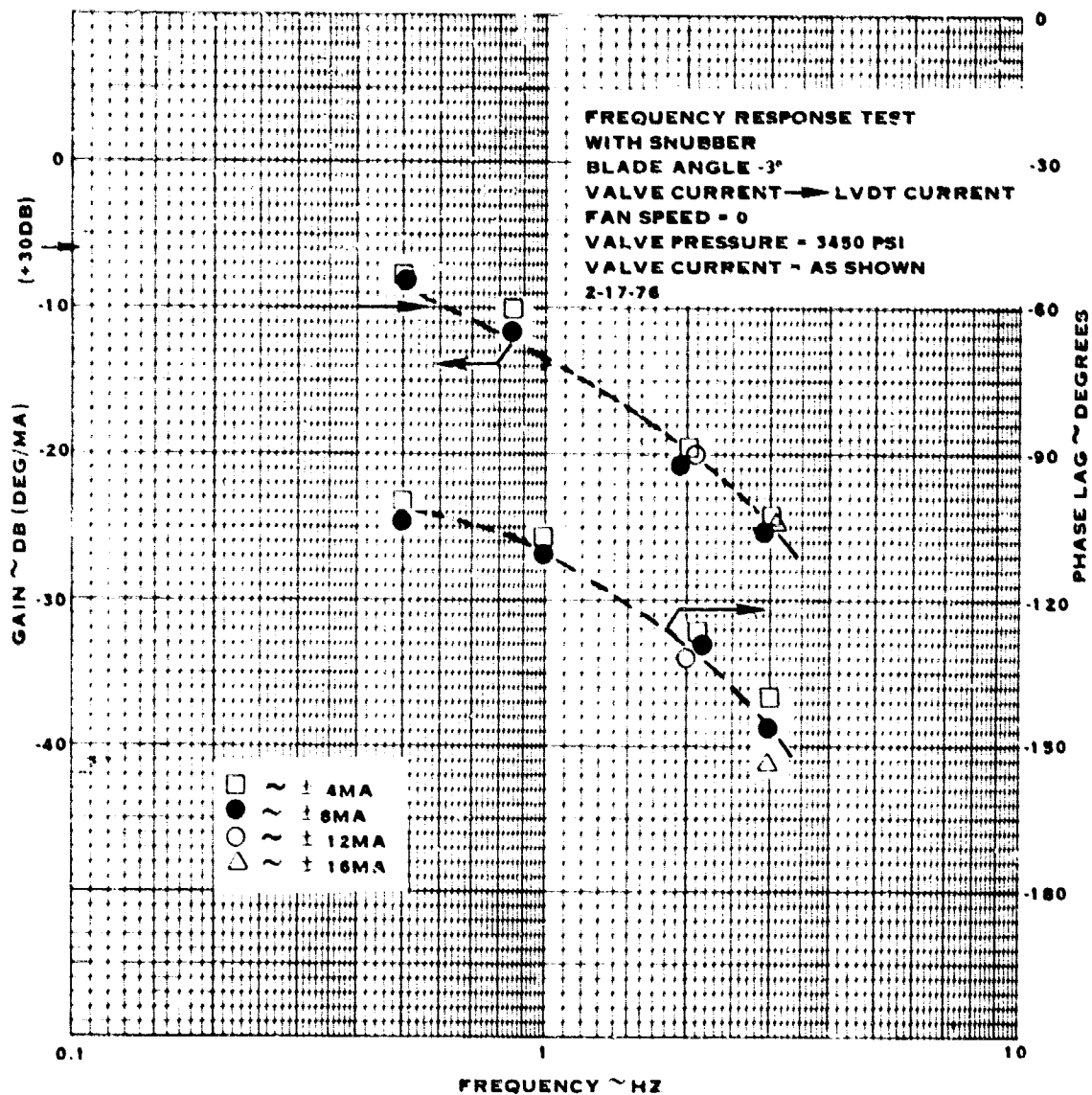


FIGURE 21. QCSEE FREQUENCY RESPONSE

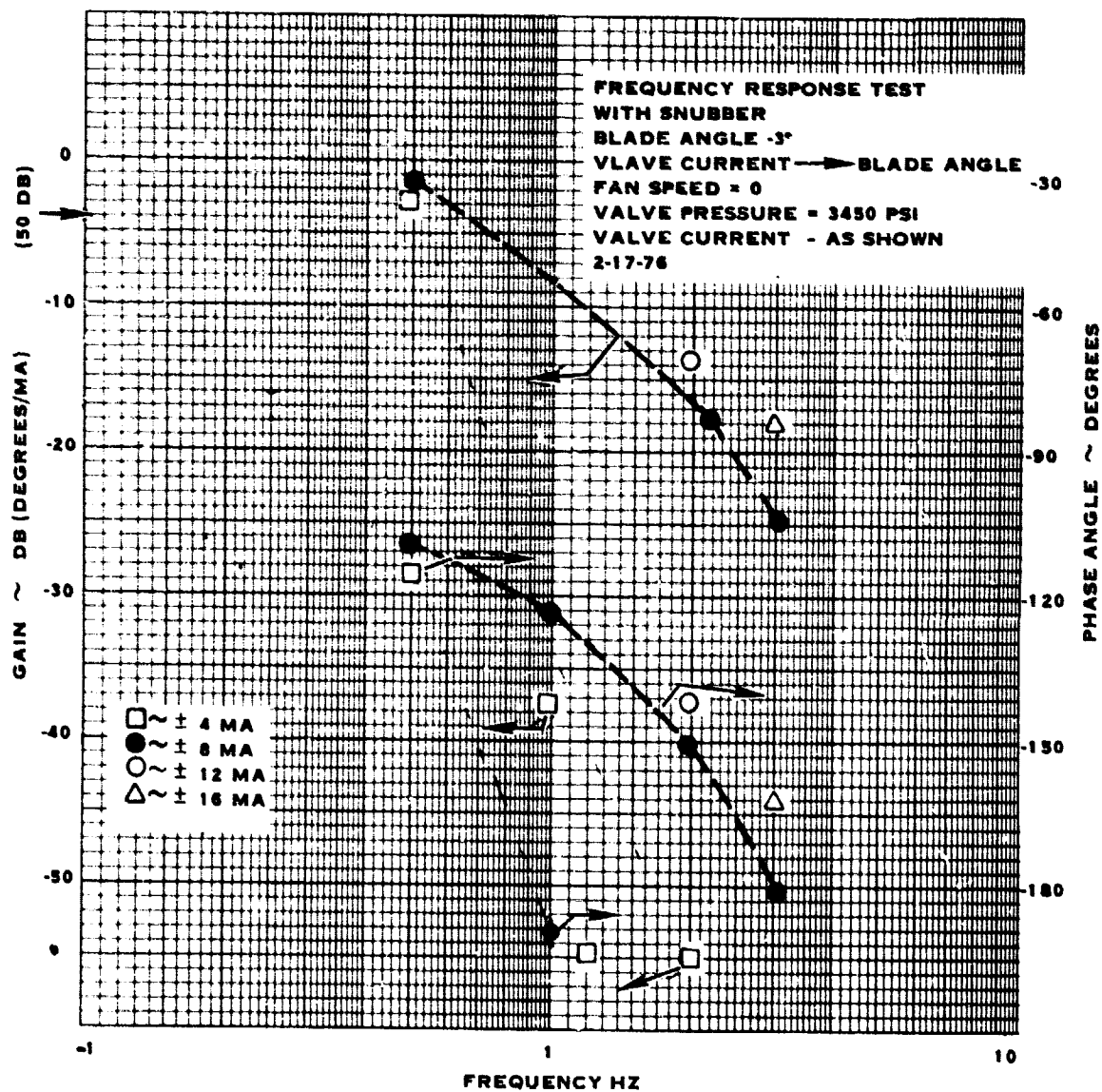


FIGURE 22. QCSEE FREQUENCY RESPONSE

7.0 CONCLUSION

The results of the whirl rig testing shows that the pitch change actuator system, incorporating the snubber, satisfies the design requirements and is structurally adequate for use on the QCSEE being developed for NASA.

The pitch change actuator system was subsequently shipped to General Electric for installation in the engine.

8.0

APPENDICES

222PT-37

OPERATING PROCEDURE

FOR

QCSEE ACTUATOR

WHIRL RIG

November 5, 1975

Prepared by: R) 20.2 - 251

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CONTENTS

- 1.0 GENERAL
- 2.0 RESPONSIBILITIES
- 3.0 RIG OPERATION
 - 3.1 General
 - 3.2 Test Item
 - 3.3 Pre Run Inspection
 - 3.4 Rig Start-up
 - 3.5 Rig Shutdown
 - 3.6 Emergency Shutdown
 - 3.7 After Operation Inspection
 - 3.8 Operating Limits
- 4.0 INSPECTION OF HARDWARE
- 5.0 RIG INSTRUMENTATION
- 6.0 LOG SHEETS
 - 6.1 Frequency
 - 6.2 Content
 - 6.3 Recorded Data

1.0 GENERAL

The purpose of this document is to define a procedure for operating the QCSEE pitch change actuator on the Hamilton Standard whirl test rig (G-7 in the Hydraulics Lab). Copies of this operating procedure will be distributed as follows:

- Test Rig - 2 copies
- Facilities Group - 1 copy
- Engineering - 6 copies (Project and Design)
- Lab Supervision - 2 copies
- Instrumentation - 2 copies

This document takes precedence over test plans as far as rig operating procedure is concerned. The Test Director will resolve all conflicts.

2.0 RESPONSIBILITIES

All persons associated with the QCSEE actuator test program will be required to conform to the operating principles defined in this document. The actual conduct of the test, in accordance with an approved test plan, will be under the control of a Test Director appointed from the Propeller Project Group. Conduct of the test will be the responsibility of this Test Director or his designated representative.

3.0 RIG OPERATION

3.1 General - The rig will be operated, at all times, in accordance with these instructions.

3.2 Test Item - The actuator assembly is defined by drawings 763499 (Beta Regulator) and 763500 (Actuator). Installation and removal of this hardware will be accomplished in accordance with HS 6971 - "Assembly and Test of QCSEE Actuator".

3.3 Pre-Run Inspection - Immediately prior to starting the rig, an inspection must be performed and a "Pre-Run Check List" filled out and signed by both the Rig Operator and the cognizant Engineer conducting the test. A new check list must be filled out if any work is done on instrumentation, rig or test item.

3.4 Rig Start-Up

3.4.1 Check to insure that the following has been accomplished:

- a) Gear box lube system on.
- b) Clutch water on.
- c) Actuator control system on.
- d) Rig speed control set for "manual".
- e) Drive motor on.

Energize clutch control and bring speed up to 500 rpm. If operation is satisfactory, increase speed to 2000 rpm and record a set of data per paragraph 6.0 before proceeding to test plan.

3.5 Rig Shutdown - Normal rig shutdown will be accomplished, with the rig speed control set at the manual position, by reducing rig speed setting to zero and turning off the clutch and drive motor.

3.6 Emergency Shutdown - If an incident or change in readings occur which the Engineer or Operator judge requires an emergency shutdown, the following procedure will be followed:

- a) Turn drive motor power off.
- b) After disc coasts down, turn off gear box lube, actuator lube and actuator hydraulic system.
- c) Immediately write down all observations noted at the time the incident occurred and mark Sanborn record with time and character of incident.

3.7 After Operation Inspection - Immediately following rig shutdown, when it is intended that some changes will be made on the test item, or when the rig will be down for more than 30 minutes, a "Post Run Check List" must be filled out by the Engineer and the Operator.

3.8 Operating Limits - The following are the operating limits which should not be exceeded at any time during operation of this rig:

Fan Speed	3600 rpm max.
EHV Supply Pressure	3800 psi max.
EHV Supply Temperature	250°F max.
Beta Regulator Speed	22,000 rpm max.
Lube Oil Flow	.8 - 1.0 qts/min.
Lube Oil Temperature (Actuator)	250°F max.
Cell Temperature	150°F max.
Vibration	2 mils max.
Clutch Water Temp.	180°F max.
Shaft Torque	125 in-lbs. max.

4.0 INSPECTION OF HARDWARE

Hardware inspection intervals will be established by the Test Director based on results obtained during the test program.

5.0 RIG INSTRUMENTATION

Instrumentation will be provided on the rig to obtain the data defined in Table I. All measurements noted as recording will be continuously recorded at a paper speed of .1 in/sec.

6.0 LOG SHEETS

A log sheet shall be maintained for all running of the actuator or its components on this rig.

6.1 Frequency - Entries shall be made on this log sheet in accordance with the following schedule:

- a) For each start.
- b) Each new functional test condition being evaluated or at 15 minute intervals.
- c) For the first endurance cycle of the run and for every fifth endurance cycle thereafter. Readings to be taken at the start and completion of each cycle.
- d) Prior to shutdown.
- e) As requested by Test Director.

6.2 Content - The log sheets will include the following information:

- a)* Date and time of entry.
- b) Name of test - G.E. QCSEE Actuator - Functional (or Endurance) Test.
- c) Rig Speed
- d) Blade Angle (from control readout)
- e)* Lube oil flow
- f)* Lube oil temperature
- g)* Lube oil pressure
- h)* EHV Supply Pressure
- I)* EHV Supply Temperature
- j) Cell temperature
- k)* Vibration - horizontal and vertical
- l) Clutch temperature
- m) G.B. oil pressure
- n) Test plan paragraph
- o)* Cycle number
- p) Operator and Engineer's name

* Record only these for 6.1(c).

6.3 Recorded Data - Data noted as recording on Table I will be recorded continuously at a record speed of 0.1 in/sec. unless a faster speed is required for the particular test being conducted. All records will be suitably marked with test plan paragraph number or cycle number and date and time for identification and to permit correlation with the rig log sheets.

TABLE 1

<u>Measurement</u>	<u>Range</u>	<u>Type</u>
EHV Supply Pressure	0-4000 psig	Visual
EHV Current Signal	± 100 ma	Recording
Flow to EHV	0-45 gal/min	Recording
Δ P Across Motor (1)	0-3500 psig	Recording
Fluid Temperature	0-300°F	Visual
Blade Angle Command	+20° to -120°	Visual and Recording
LVDT Feedback Voltage (1)	± 5 V dc	Recording
Flex Shaft Speed	0-24,000 rpm	Recording
Flex Shaft Torque	0-200 in.lb.	Recording
Lube Oil Flow	0-1 qt/min.	Visual
Lube Oil Pressure	0-100 psig	Visual
Lube Oil Temperature	0-300°F	Visual
Fan Speed	0-3700 rpm	Visual and Recording
Cell Temperature	0-300°F	Visual
Vibration - Horizontal		Visual
Vibration - Vertical		Visual
Fan Blade Angle	+20° to -120°	Visual

HSER 7002
11/4/75

POST RUN CHECK LIST
QCSEE ACTUATOR - G-7 RIC

Date: _____
Rig Time: _____
Flight Cycles: _____

Item	Condition	Initial	
		Operator	Engineer
1 All hardware appears structurally sound.			
2 No evidence of oil leakage.			
3 Arm, disc and cam area clean, dry and free of foreign objects.			
4 All visible bolts, nuts, mounts, etc. appear secure.			
5 All pumps shut off.			
6 Disc and actuator covered up if unit will be shut down for any period of time and is not being worked on.			
7 All data recorded and records properly marked.			

REMARKS -

HSER 7002

11/4/75

FRE RUN CHECK LIST

QCSEE ACTUATOR - G-7 RIC

Date: _____

Rig Time: _____

Flight Cycles: _____

Item	Condition	Initial	
		Operator	Engineer
1 Disc uncovered.			
2 Instrumentation connected and operating.			
3 Arm, disc and cam area clean, dry and free of foreign objects.			
4 All visible bolts, nuts, mounts, etc. appear secure.			
5 Stop switches correctly set and Beta Regulator indexed to actuator (feedback and actual blade angle agree).			
6 Hydraulic pumps on, bypass closed and correct pressure at servo valve (per test plan).			
7 Actuator lube pump on and set for _____ psi at Beta Regulator.			
8 All personnel and loose material out of cell and cell doors secured.			

REMARKS -

APPENDIX B

TEST PLANS

Hamilton Standard

WINDSOR LOCKS, CONNECTICUT • U.S.A.

DIVISION OF UNITED AIRCRAFT CORPORATION

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A

HSER 7002

PAGE 1 OF 12

No. 222PT-31 Rev. ADATE: 10/28/75**PLAN OF TEST**ITEM: 763500 Actuator (QCSEE)PREPARED BY: D. LeishmanCONTRACT: GE 200-4XX-14G-38570APPROVED BY: [Signature]

TEST PERIOD: _____

1. WHAT IS ITEM BEING TESTED?
2. WHY IS TEST BEING RUN? WHAT WILL RESULTS SHOW OR BE USED FOR?
3. DESCRIBE TEST SETUP INCLUDING INSTRUMENTATION, ATTACH SKETCH OF INSTALLATION.
4. ITEMIZE RUNS TO BE MADE GIVING LENGTH OF EACH AND READINGS TO BE TAKEN.
5. SPECIAL INSTRUCTIONS: SAFETY PRECAUTIONS FOR OPERATORS AND HANDLING EQUIPMENT. OBSERVATIONS BY SIGHT, FEEL, OR HEARING. LIST POINTS OF OBSERVATION WHICH MIGHT CONTRIBUTE TO ANALYSIS OF (A) PERFORMANCE OF UNITS. (B) INCIPIENT TROUBLE BEFORE IT OCCURS, AND (C) CAUSE OF FAILURE.
6. HOW WILL DATA BE USED OR FINALLY PRESENTED? GIVE SAMPLE PLOT, CURVE, OR TABULATION AS IT WILL BE FINALLY PRESENTED.

NUMBER ENTRY AS LISTED ABOVE AND DESCRIBE BELOW

1.0	The item being tested is the pitch change actuator for the QCSEE assembled for reverse through stall operation.
2.0	The test is being run to determine the operating characteristics of the actuator, verify that it satisfies the design requirements, and assure its structural adequacy for use in an engine test.
3.0	The actuator, together with a disc and stub blades supplied by GE will be mounted in G-7 Whirl Rig which has been modified to accept the unit. Reference Figure 1. A closed loop variable gain control system with a capability to vary gain between 570 and 2700 ma/volt/volt excitation will be utilized for the test. The instrumentation to be used during the test is listed in Table 1. Figure 2 is a drawing showing the hardware necessary to convert the actuator to a front flex shaft input, and Figure 3 is a lubrication schematic of the actuator.
4.0	The following tests will be conducted. All blade angles are in GE terms. Figure 4 is a plot of blade angle vs. counterweight angle.

73

TABLE 1

<u>Measurement</u>	<u>Range</u>	<u>Type</u>
EHV Supply Pressure	0-4000 psig	Visual
EHV Current Signal	<u>+100</u> ma	Recording
Flow to EHV	0-45 gal/min	Recording
Δ P Across Motor (1)	0-3500 psig	Recording
Fluid Temperature	0-300°F	Visual
Blade Angle Command	+20° to -120°	Visual and Recording
LVDT Feedback Voltage (1)	<u>+5</u> V dc	Recording
Flex Shaft Speed	0-24,000 rpm	Recording
Flex Shaft Torque	0-200 in.lb.	Recording
Lube Oil Flow	0-1 qt/min.	Visual
Lube Oil Pressure	0-100 psig	Visual
Lube Oil Temperature	0-300°F	Visual
Fan Speed	0-3700 rpm	Visual and Recording
Cell Temperature	0-300°F	Visual
Vibration - Horizontal		Visual
Vibration - Vertical		Visual
Fan Blade Angle	+20° to -120°	Visual

- 4.1 Lubrication Flow Check
 - 4.1.1 With the flex drive shaft disconnected from the actuator, determine the pressure setting necessary at the beta regulator to obtain a flow of .85 qts/min through the shaft at a shaft speed of 0 rpm.
- 4.2 LVDT Null & Calibration (fan speed = 0 rpm)
 - 4.2.1 Using the manual input to the Beta Regulator, determine the LVDT output and blade angle at the mechanical stops of the actuator. Reset the LVDT null so that the output varies an equal amount on either side of null as the blade moves through the full range of travel.
 - 4.2.2 Using the manual input to the Beta Regulator, calibrate actual blade angle versus LVDT output voltage every 5° over the full range of travel in both increasing and decreasing pitch directions. During this calibration, set the travel limit switch cams to actuate at -8° and -96° blade angle.
- 4.3 Travel Limit Switch
 - 4.3.1 With the travel limit switch cams set for -8° and -96°, and a fan speed of 0 rpm, determine the actual blade angle at which the blades stop when the travel limiting switch is actuated at flex shaft speeds of approximately 6000 rpm, 12,000 rpm and 21,000 rpm. Regulate EHV supply pressure to control rate.
 - 4.3.2 With the travel limit switch cams set for -8° and -96°, and a fan speed of 2500 rpm, determine the actual blade angle at which the blades stop when the travel limit switch is actuated at flex shaft speeds of approximately 6000 rpm, 12,000 rpm and 21,000 rpm.
 - 4.3.3 Reset the travel limit switch cams for +12.5° and -116° or to a modified value if testing does not confirm the calculated values of travel required to stop the system (6.5 -7°).
- 4.4 Blade Angle Position Accuracy
 - 4.4.1 With the EHV inlet pressure set at 2000 +100 psig and a fan speed of 2500 rpm, cycle the actuator in accordance with Table 2. At each condition, record actual vs. LVDT blade angle.

Table 2

Step (Reference Table 5)	Blade Angle
1	+12°
3	-3°
5	0°
6	+7°
7	+5°
8	+7°
9	+9°
10	+7°
12	-100°
15	+12°

- 4.4.2 With the EHV inlet pressure set at 3450 +100 psig, and fan speed as shown, cycle the actuator in accordance with Table 2a. At each condition, record actual vs. LVDT blade angle.

Table 2a

Step (Reference Table 5)	Blade Angle	Fan Speed
1	+12°	2500
3	-3°	3068
5	0°	3068
6	+7°	3068
7	+5°	3068
8	+7°	3068
9	+9°	3068
10	+7°	3068
12	-100°	3068
15	+12°	2500

4.5 Performance

- 4.5.1 Determine the pressure required to start actuator motion in both increasing and decreasing pitch directions for the conditions specified in Table 3.

Table 3

Fan Speed	Starting Blade Angle
2500 rpm	+12° (increasing only)
3068 rpm	+5°
3068 rpm	+7°
3068 rpm	+9°
3408 rpm	0°
3408 rpm	-3°
2500 rpm	-100° (decreasing only)

- 4.5.2 Determine the pressure required to sustain actuator motion for the blade angle excursions specified in Table 4.

Table 4

Fan Speed	Blade Angle Excursion
2500 rpm	+12° to -3°
3408 rpm	-3° to +0°
3068 rpm	0° to +7°
3068 rpm	+7° to +5°
3068 rpm	+5° to +7°
3068 rpm	+7° to +9°
3068 rpm	+9° to +7°
3068 rpm	+7° to -100°
2500 rpm	-100° to +12°

- 4.5.3 Determine the average pitch change rate for a blade angle excursion from -3° to -100° at a fan speed of 3315 rpm. EHV supply pressure to be set at 3450 ±50 psig. (rate based on LVDT feedback voltage)

- 4.5.4 With the blade angle set at 0°, fan speed of 3408 rpm, and EHV supply pressure 3450 +50 psig, demonstrate the minimum blade angle change which can be obtained around 0°.
- 4.5.5 With the blade angle set at -100°, EHV supply pressure at 0 psig, increase fan speed to 3578 rpm and record any blade angle change.
- 4.5.6 With the blade angle set at 0°, EHV supply pressure at 0 psig, increase fan speed to 3408 rpm and record any blade angle change.
- 4.6 Frequency Response
 - 4.6.1 At a blade angle of -3° and with a fan speed of 0 rpm, determine B_f/ EHV and LVDT/ EHV. Static frequency response and phase angle shall be determined for EHV current peak to peak amplitudes not to exceed +40 ma or that current input which causes a B_f variation of +1.9 to +2.1 degrees at frequencies of 0.5, 1.0, 1.5, 2.0, 3.0, and 4.0 Hz.
 - 4.6.2 Rotating frequency response tests will be conducted to determine Δ LVDT/ Δ EHV.

Two base point conditions will be used:

- 1. Fan speed = 3066 rpm.
B_f = 3° open.
- 2. Fan speed = 2920 rpm.
B_f = 100° open.

Frequency response and phase angle for base point conditions 1 and 2 shall be determined for EHV current peak to peak amplitudes not to exceed +40 ma or that current input which causes a LVDT variation of +.0135 to +.0165 volts/volt at frequencies of 0.5, 1.0, 1.5, 2.0, 3.0, and 4.0 Hz.

4.7 Endurance Test

- 4.7.1 Prior to and at completion of the endurance test, the unit will be disassembled and the hardware will be examined to identify any potential problem areas.
- 4.7.2 The endurance test will consist of 500 cycles of the actuator in accordance with Table 5. During testing, the EHV supply pressure will be maintained at 3450 +50 psig. The cycles may be run faster than the normal anticipated engine duty cycle in order to shorten the required test time. The cycle frequency will be established during the functional test program. The limiting factor will be the ability of the unit to dissipate the heat generated in the no-back and the clutch. The blade angle must be allowed to stabilize at each point prior to going on to the next point except during modulating operation. (Steps 7-11 of Table 5)

5.0 Special Instructions

Prior to and following operation, the check list shown in Figure 5 must be completed. Note any unusual noises or vibrations, or any changes in noise

TABLE 51 cycle

<u>Step</u>	<u>Fan Speed</u>	<u>Blade Angle</u>
1	2500 rpm	+12°
2	2500	-3°
3	3408	-3°
4	3408	0°
5	3068	0°
6	3068	+7°
7	3068	+5°
8	3068	+7°
9	3068	+9°
10	3068	+7°
11	Repeat steps 7 thru 10 twenty times	
12	3068	-100°
13	3408	-100°
14	2500	-100°
15	2500	+12°

5.0 Continued

or vibration. During the static and performance testing, a log sheet shall be kept which contains the parameters denoted as visual in Table 1 for each test point. Functional test data denoted as recording shall be taken at each test point at a speed commensurate with the test being run.

During the endurance test, a log sheet shall be kept which contains the parameters denoted as visual in Table 1 for the first and each fifth cycle thereafter. Endurance test data denoted as recording shall be taken continuously at a speed of .1 in/sec.

In order to provide a complete time/rpm history for the fan rotor components, data denoted as recording shall be taken at a speed of .1 in/sec at all times when the fan is rotating except when higher recording speeds are needed for a specific test point.

- 6.0 A component test report will be prepared following the completion of the whirl rig tests. Discussions and data presented in the report will cover all tests conducted during the whirl rig test program. All test data will be available for review and use by GE and NASA representatives.

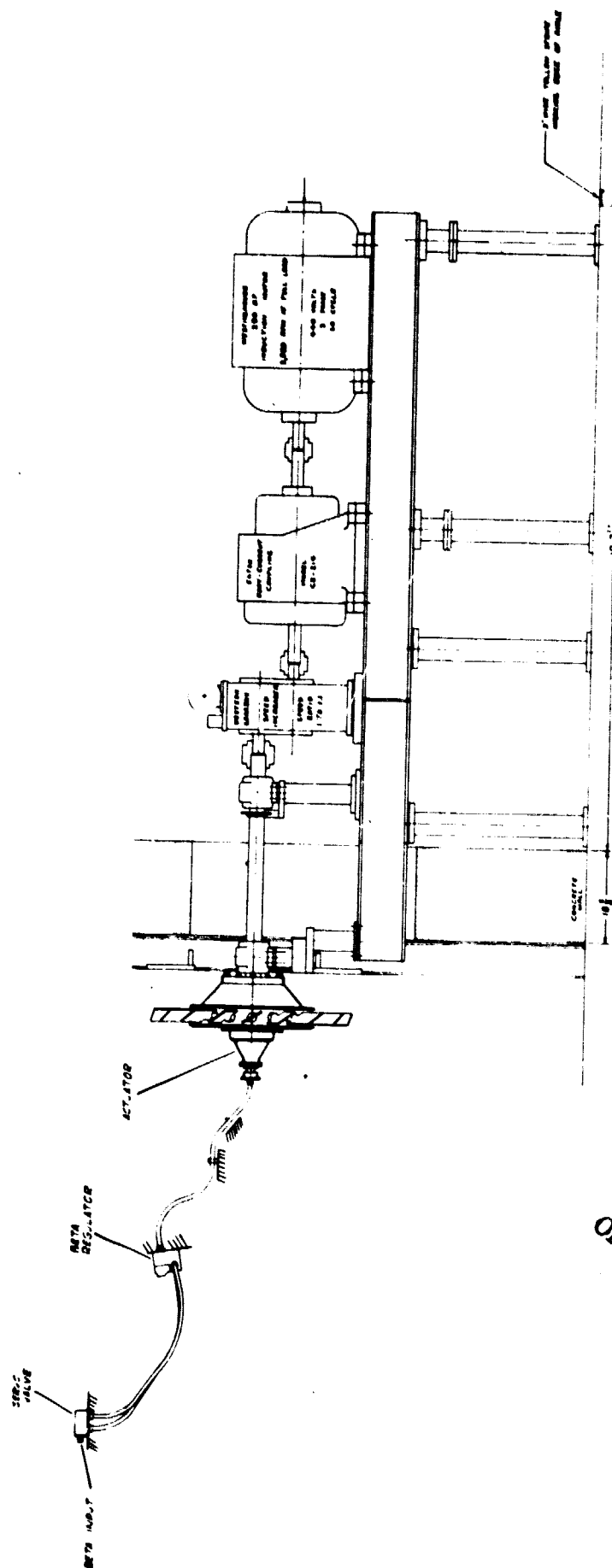


FIGURE 1. WHIRL RIG ARRANGEMENT

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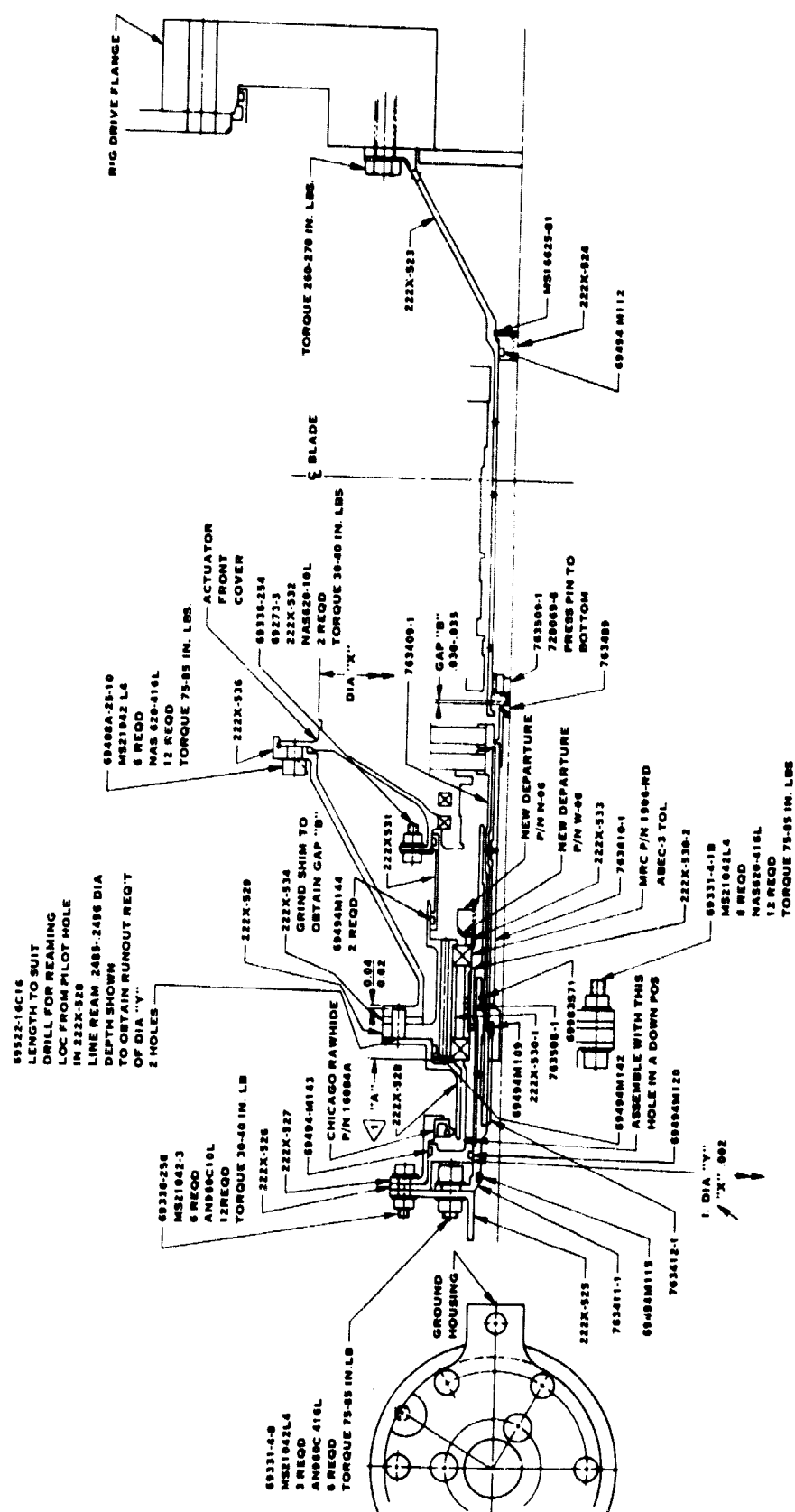


FIGURE 2. ASSEMBLY, FRONT INPUT HARDWARE

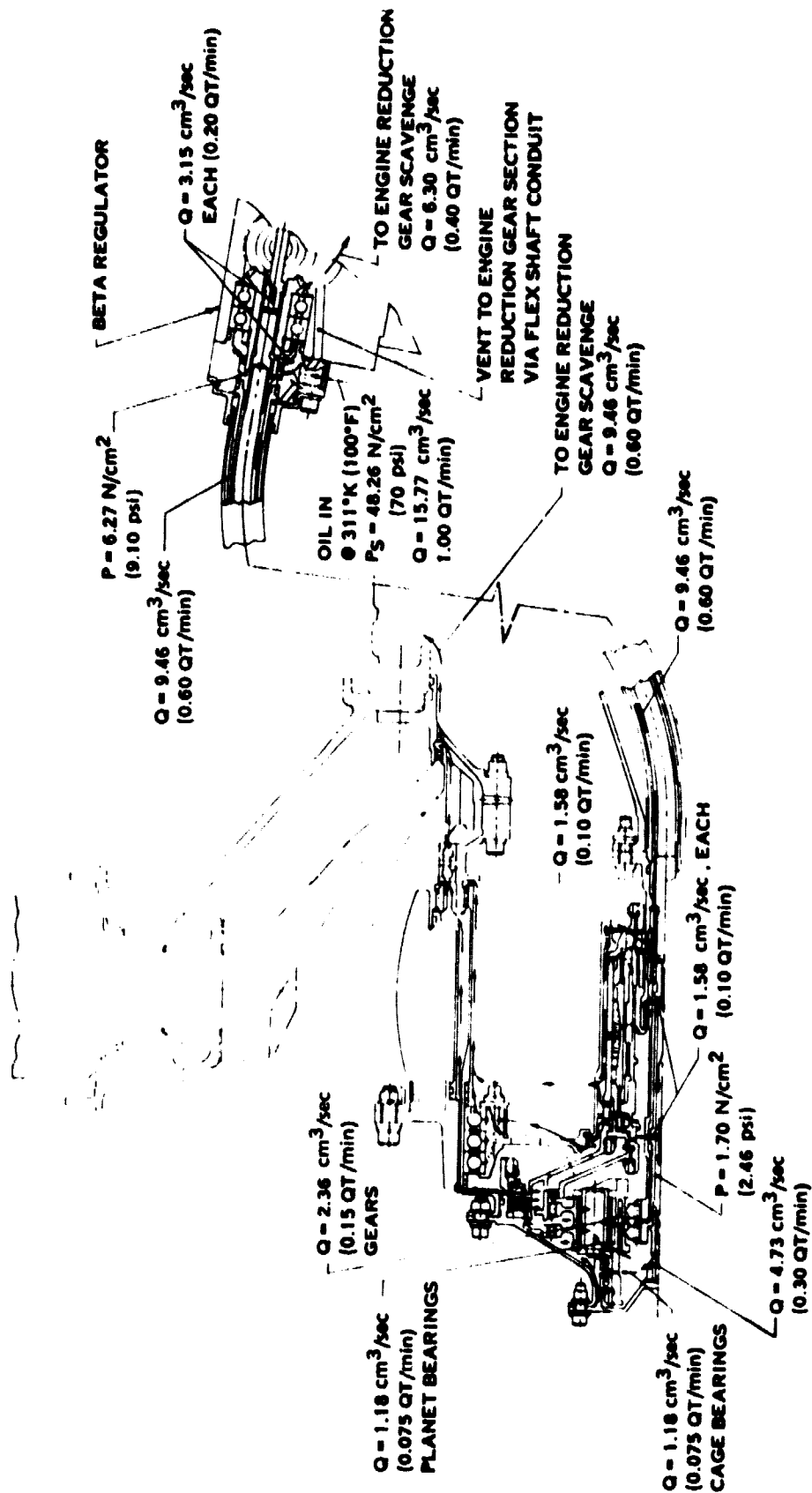


FIGURE 3. LUBRICATION SCHEMATIC

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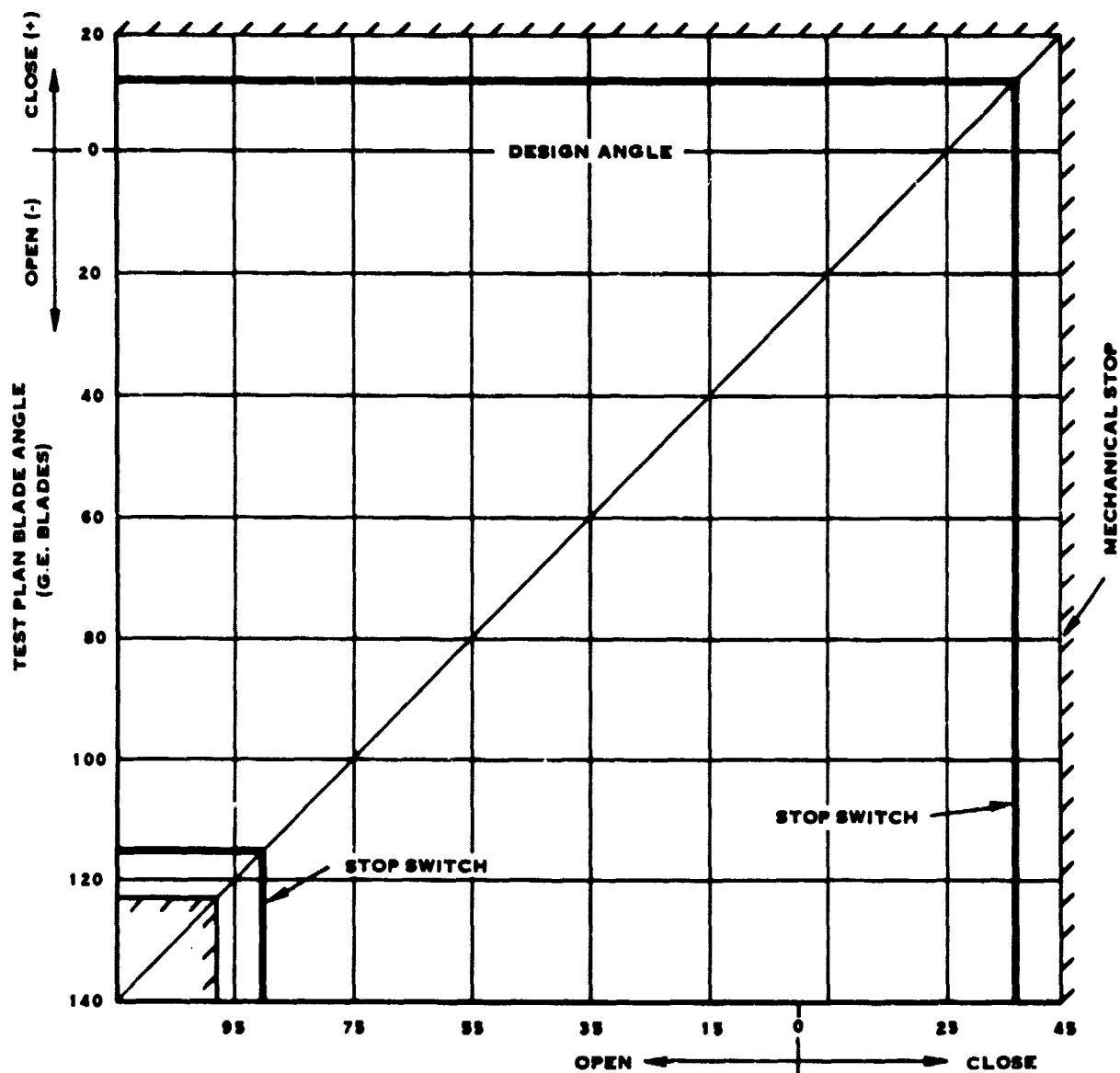


FIGURE 4. QCSEE PITCH CHANGE ACTUATOR TEST PLAN BLADE ANGLE VS. COUNTERWEIGHT ANGLE (TEST PLAN 222 Pt-31 REV. A)

QCSEE ACTUATOR
WHIRL RIG CHECK LIST

Pre Operation

1. Actuator assembled per HS6971
2. System is correctly rigged and indexed
3. Feedback blade angle agrees with actual angle
4. Instrumentation secured
5. Cell cleaned
6. Hydraulic supply pump on
7. Lubrication supply pump on
8. Scavenge pump on

Post Operation

1. Check for leaks
2. Check feedback vs. actual blade angle
3. All required data recorded

FIGURE 5

HAMILTON STANDARD

Test No. 222PT-38

PLAN OF TEST

Date: 1-30-76

Job: 763500 Actuator with Soft Quill Shaft

Prepared by: D. E. Smith

Project & Order GE 200-4XX-14G-38570

4.0 The following tests will be conducted.

4.1 System Losses

The torque to move the blades will be measured at the beta regulator manual drive when the installation is complete, after each reassembly and following completion of the 50 flight cycles. Torque will be measured in both directions of motion at $+10^\circ$, 0° and -100° of blade angle.

4.2 Blade Angle Calibration

The LVDT's will be calibrated against the position of the counterweights, for both directions of motion. Calibration will be in approximately 2° increments between $+12$ and -10° and 10° increments from -10° to -100° .

4.3 Stop Switches

Stop switches shall be set 6.5° - 7° from the mechanical stops. Stop angle and switch setting will be recorded.

4.4 Max Rate Testing (Ref. 4.5.3 of 222PT-31A)

After checking system operation over entire range and adjusting control settings, perform a reverse transient at 3315 fan rpm and 3450 psi EHV supply pressure. Pump stroke should be adjusted for $10,000 \pm 500$ rpm flex shaft speed. Reduce rig speed to 2700 rpm and unreverse at $10,000 \pm 500$ rpm. Repeat test to obtain two (2) cycles and remove and examine no back and snubber. Determine wind up which snubber experienced.

Reassemble no back and install in rig. Repeat test at $17,500 \pm 500$ flex shaft rpm. Remove and examine no back and snubber and record snubber wind up.

4.5 Endurance Test

Conduct fifty (50) cycles of endurance testing in accordance with paragraph 4.7.2 of 222PT-31A. Max flex shaft speed will be adjusted to achieve 17500 ± 500 rpm during reverse transient portion of run. Following the endurance test, the no back and snubber hardware will be examined.

Test No. 222PT-38

HAMILTON STANDARD

Page 3 of 3

Date: 1-30-76

HSER 7002

Job: 763500 Actuator with Soft Quill Shaft

Prepared by: D. E. Smith

Project & Order GE 200-4XX-14G-38570

4.6 Limit Switch Overtravel

The amount of blade travel required to stop, after tripping the travel limit switches, will be determined at both ends of the operating range. Test will be run statically. For each end of travel, the stopping distance will be determined for flex shaft speeds of 10,000, 12,000, 15,000 and 17,500 rpm (± 500 rpm). The control time constant will be set for .02 seconds initially. If necessary to increase this time constant, the new value shall be recorded on the log sheet.

4.7 Frequency Response

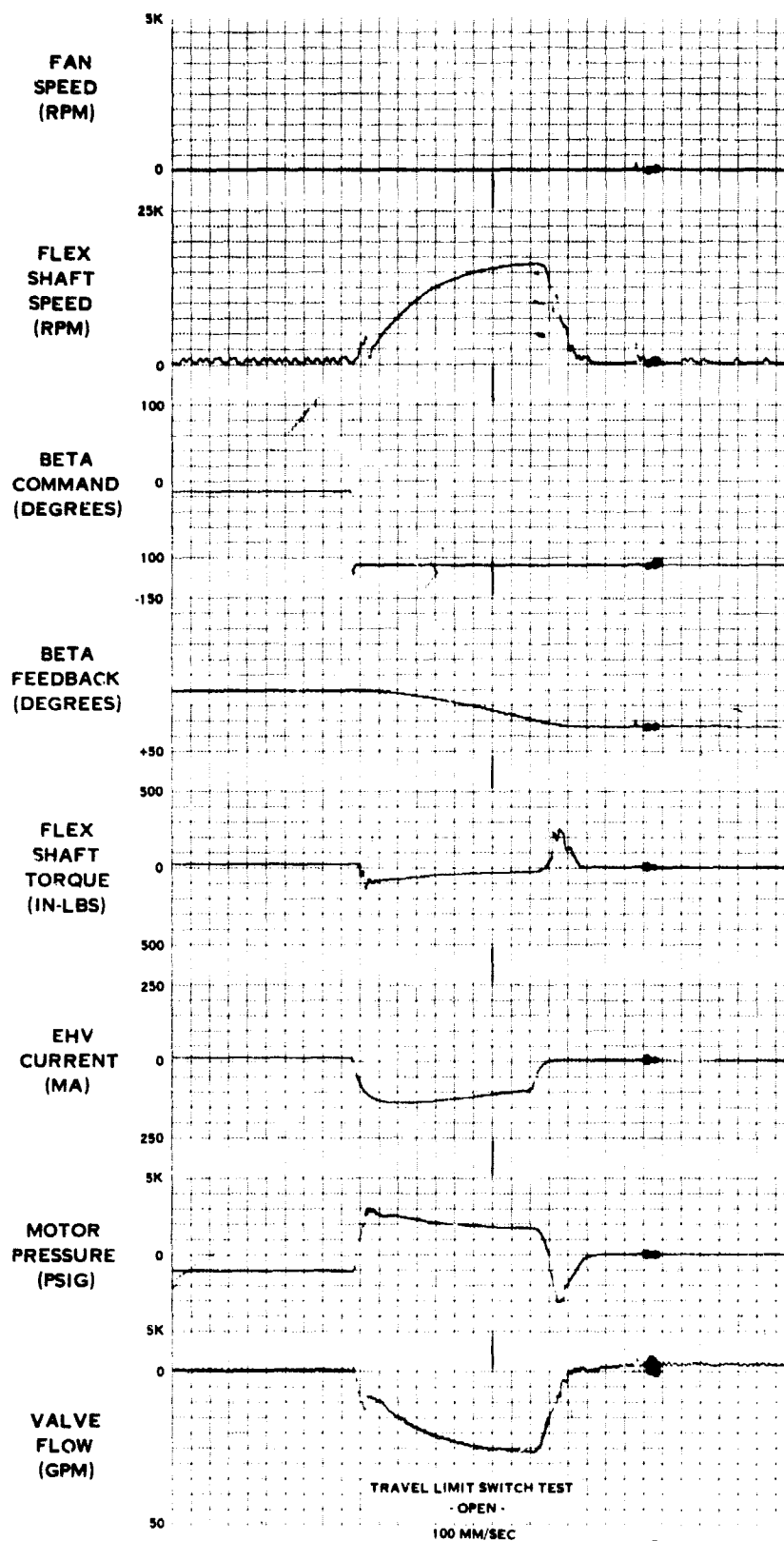
The static frequency response shall be measured as described in 4.6.1 of 222PT-31A.

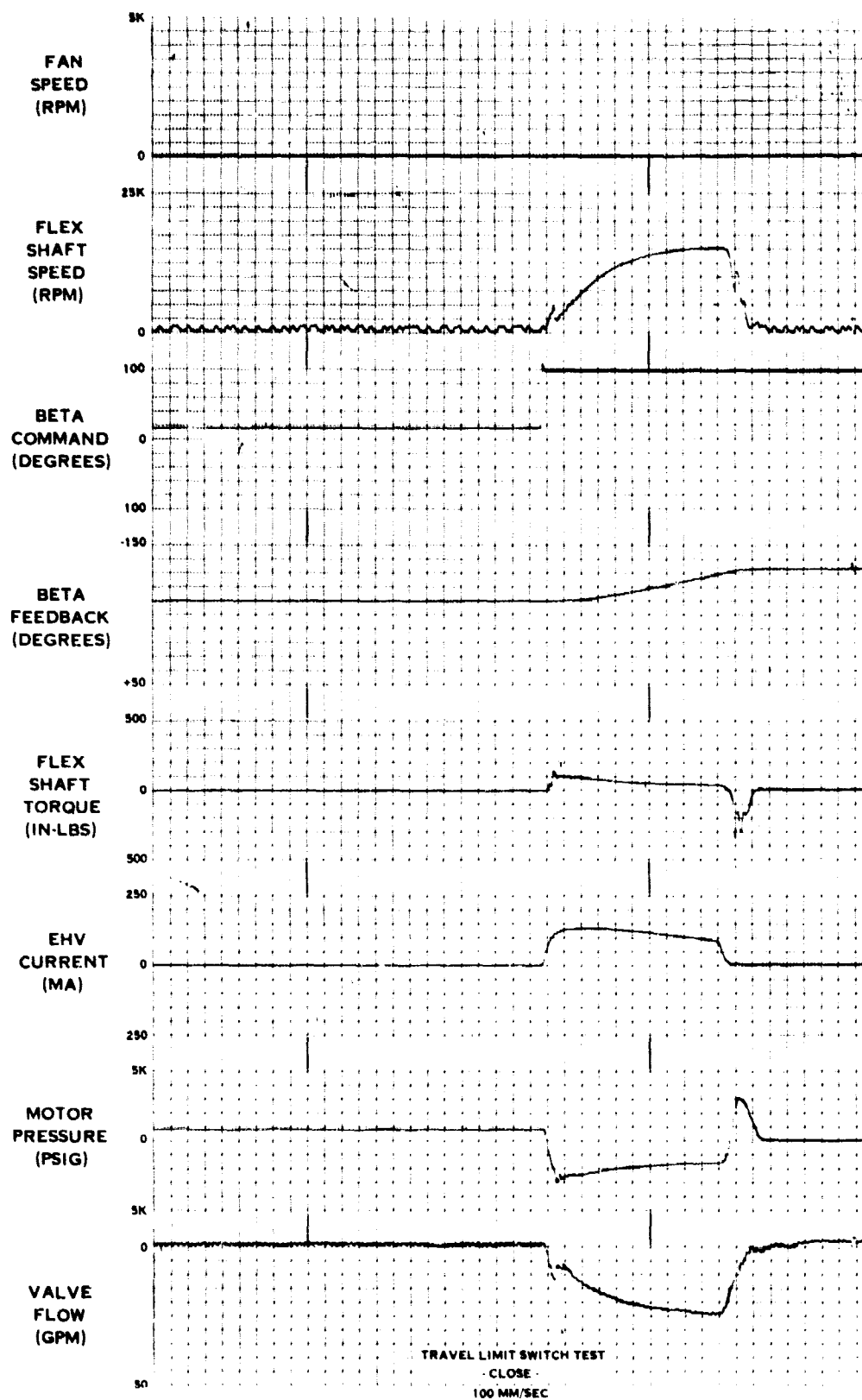
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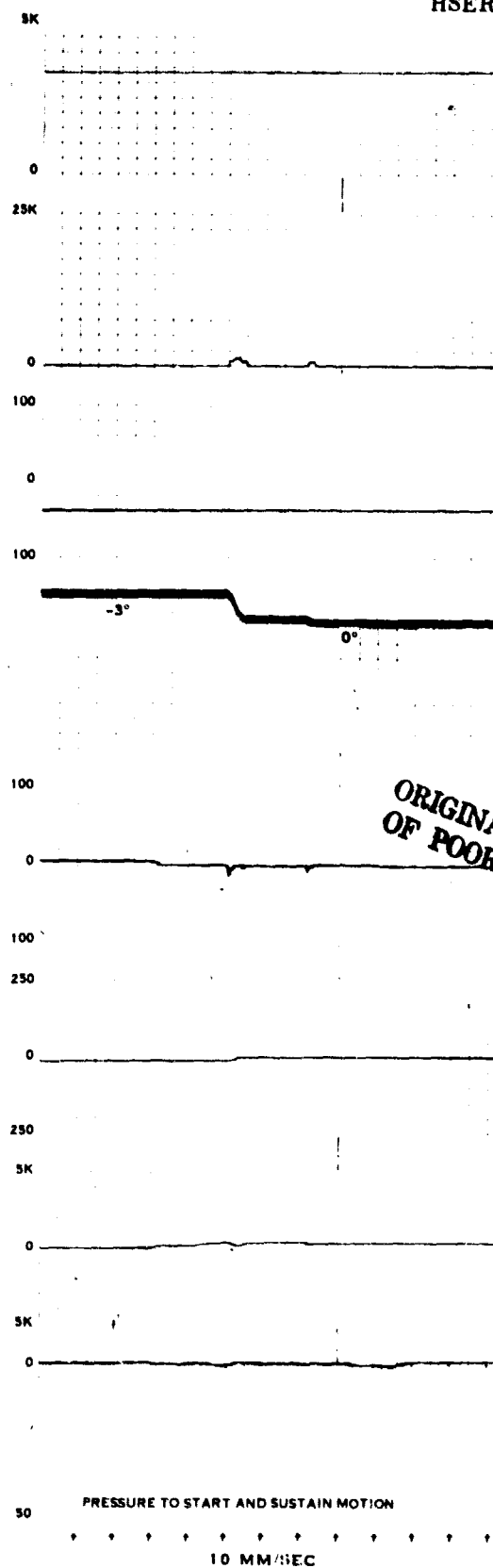
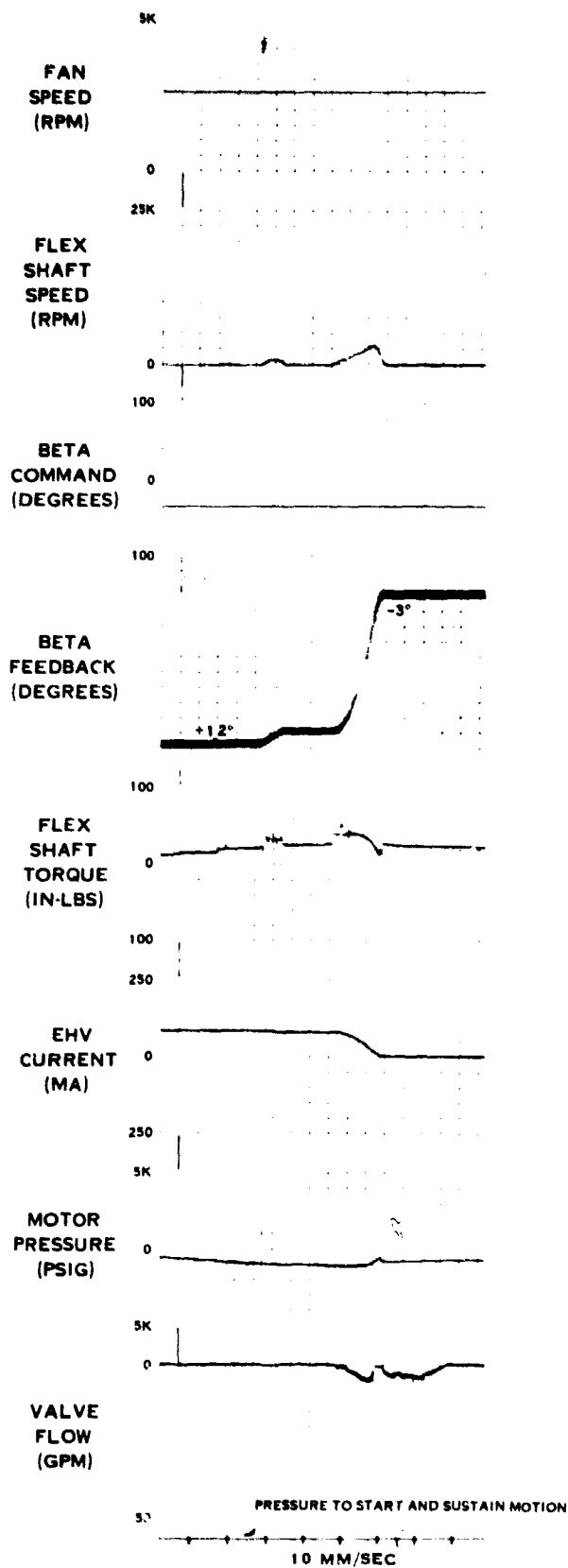
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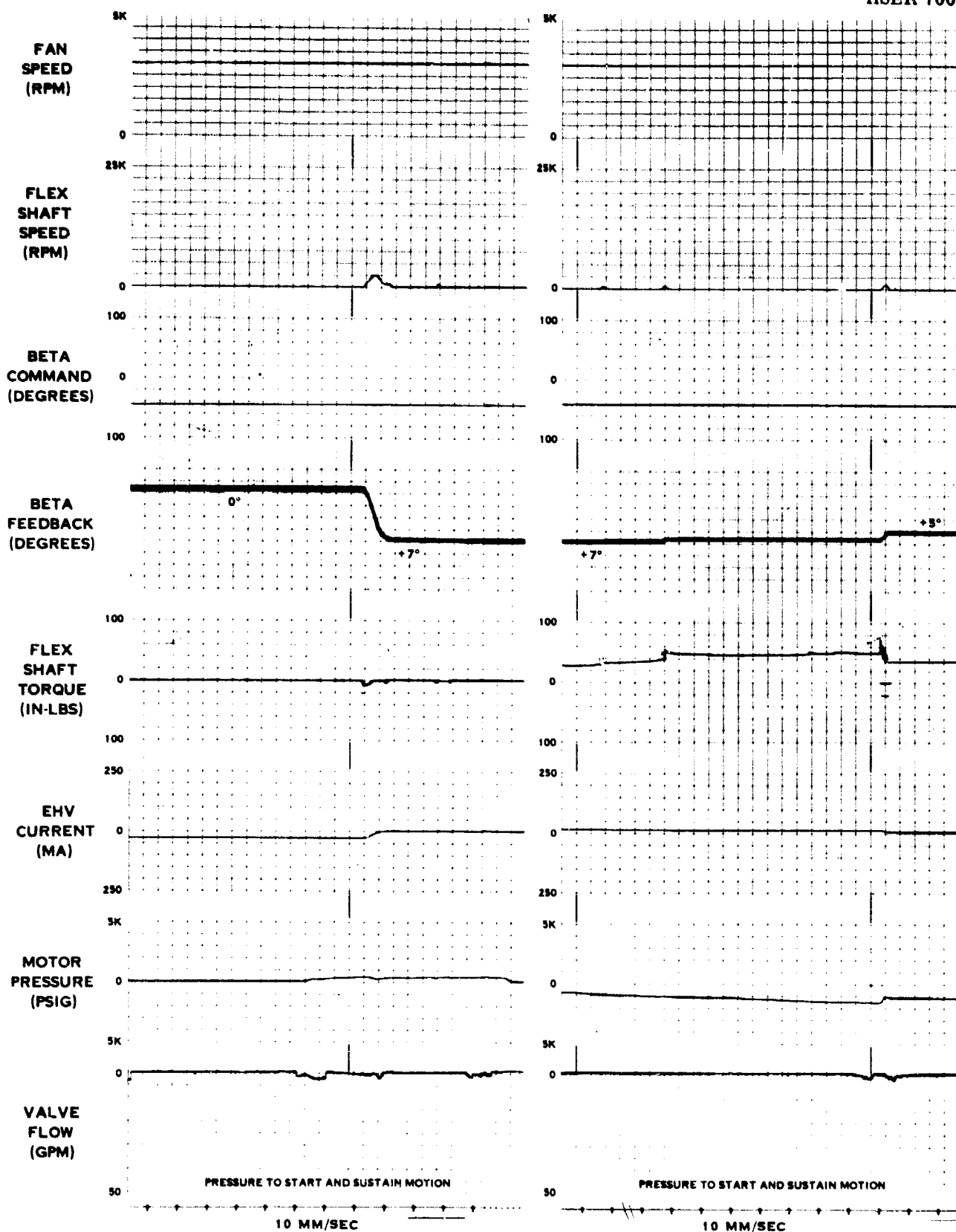
APPENDIX C

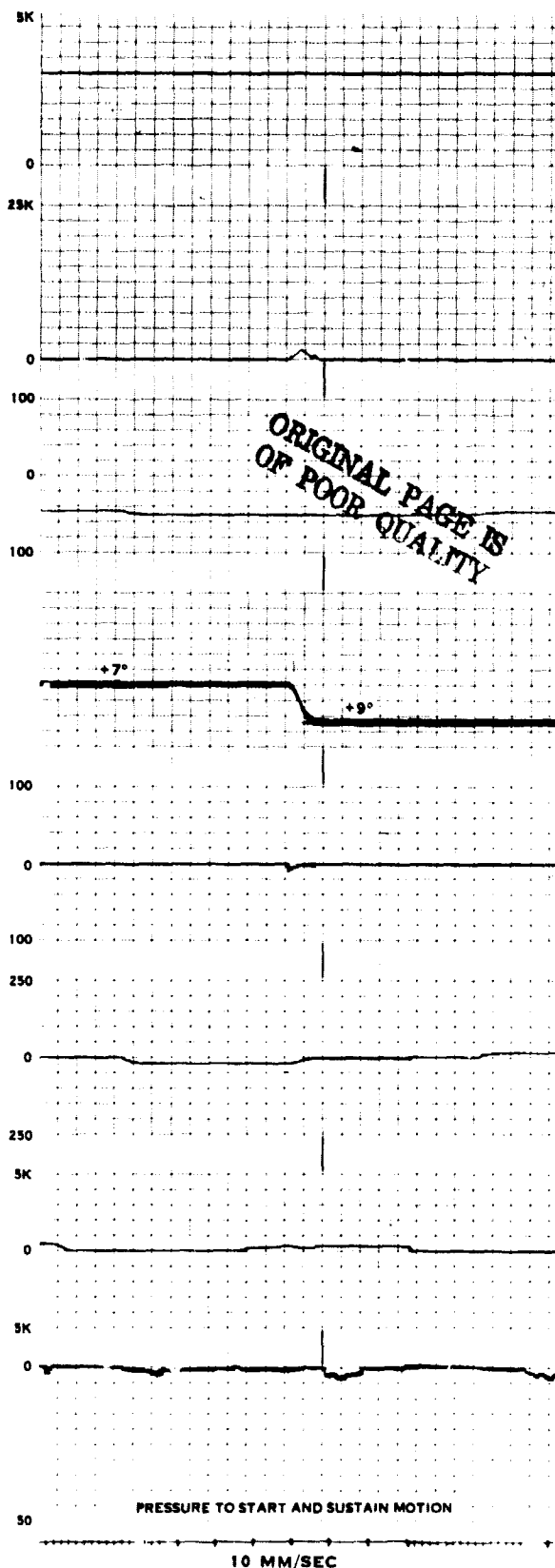
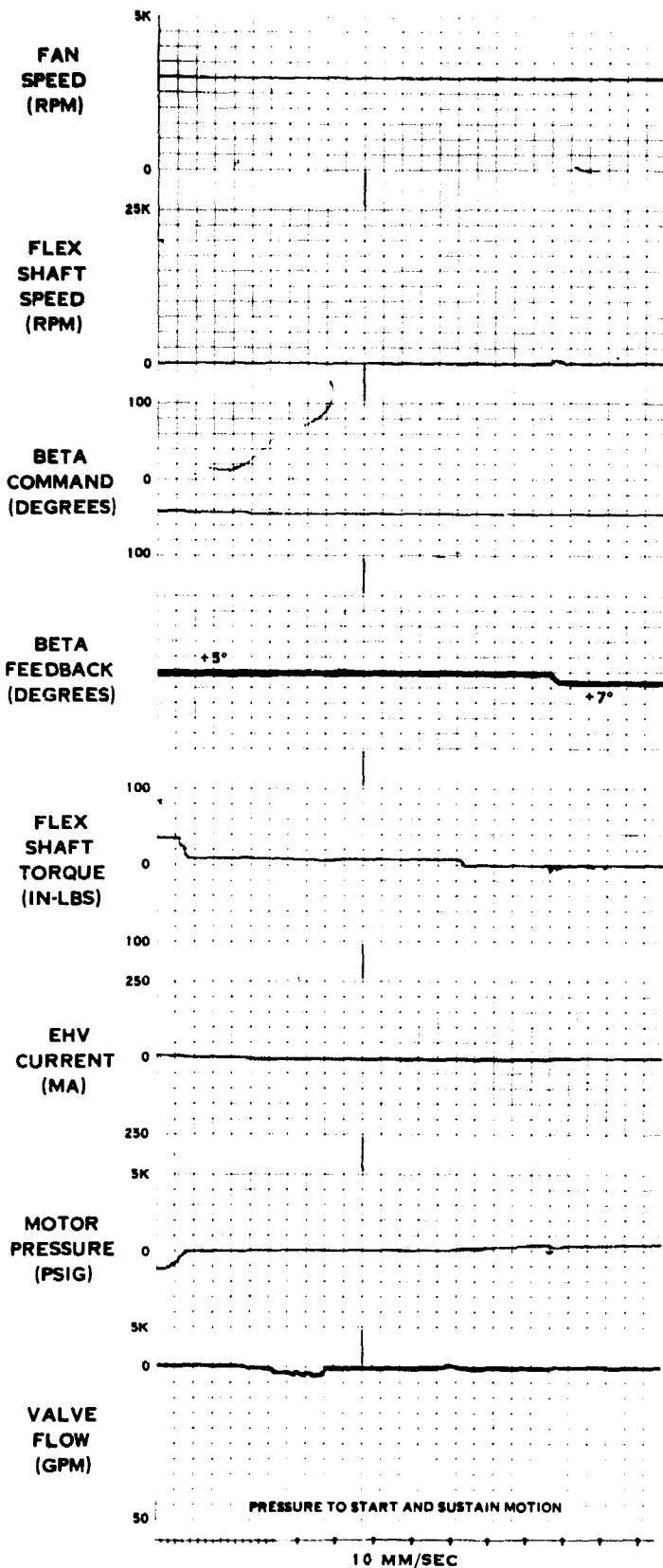
SANBORN RECORDS



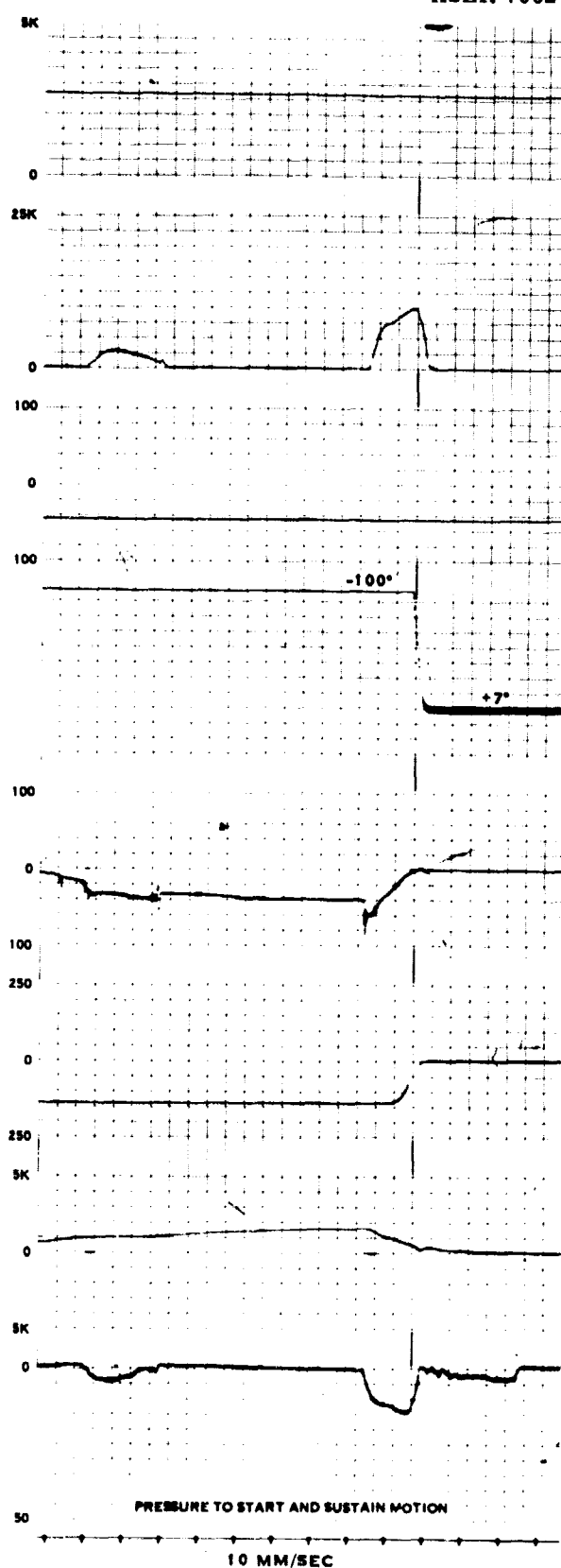
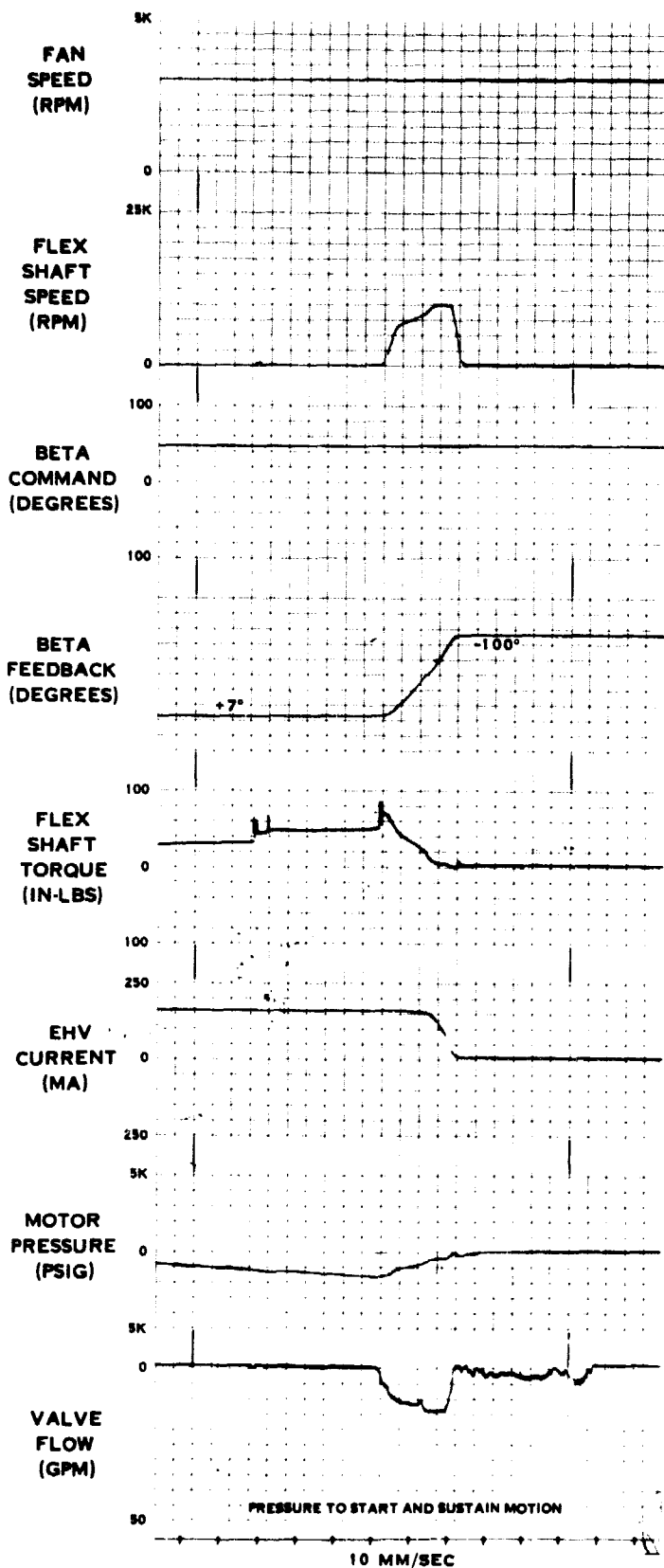


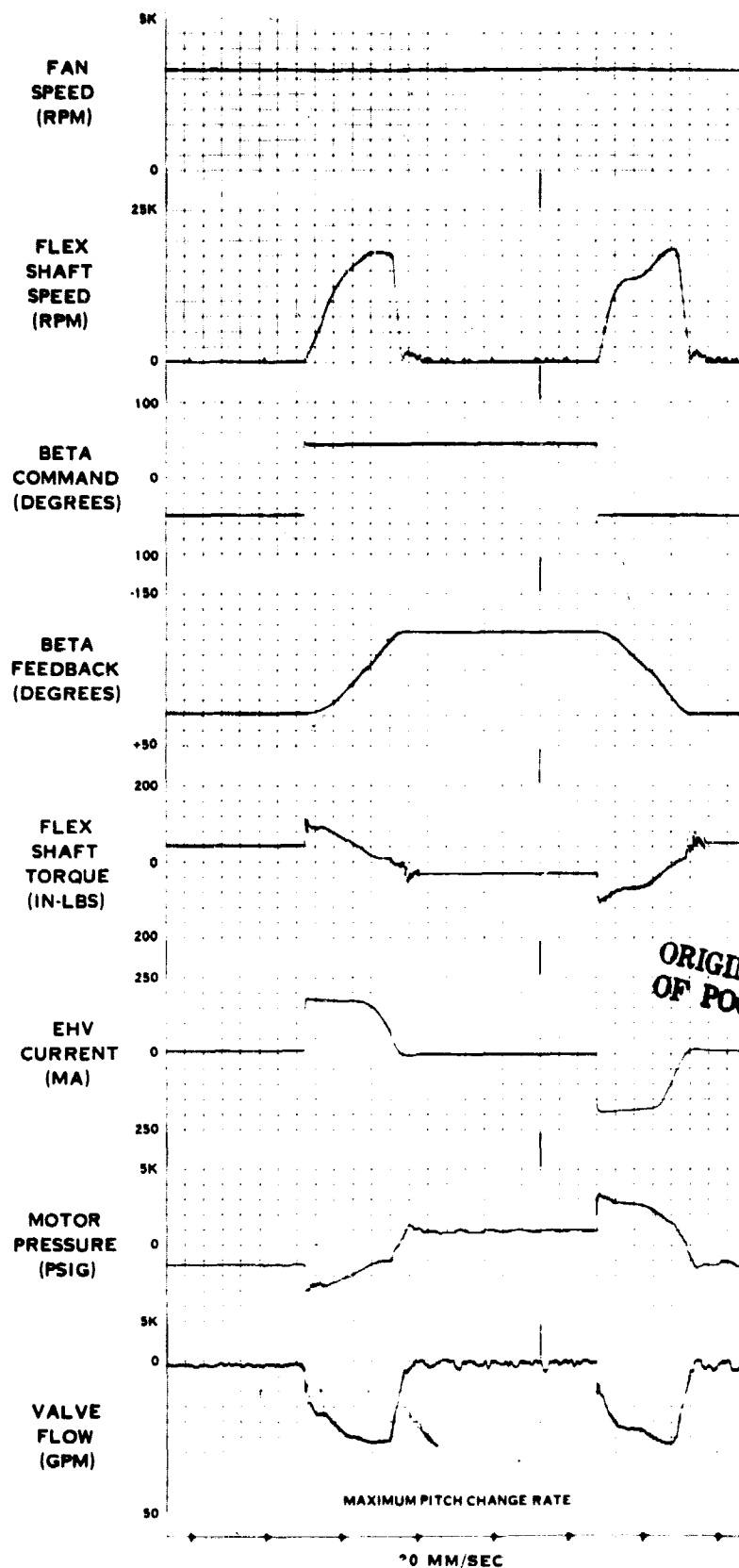






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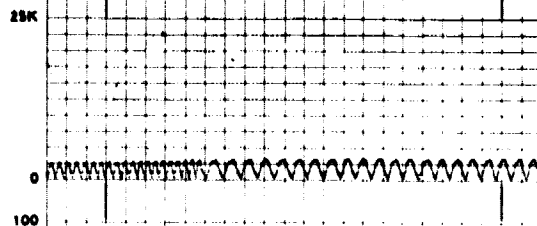


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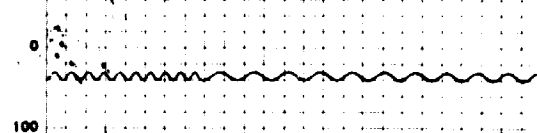
ACTUAL
BETA
(DEGREES)



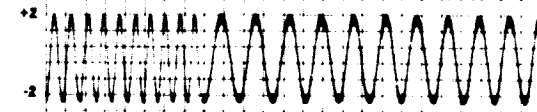
FLEX
SHAFT
SPEED
(RPM)



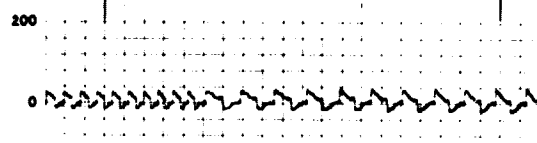
BETA
COMMAND
(DEGREES)



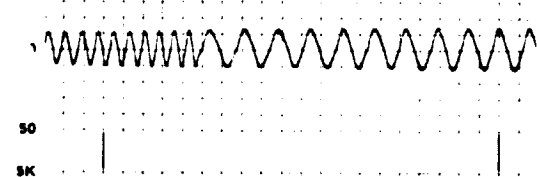
BETA
FEEDBACK
(DEGREES)



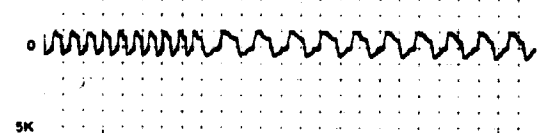
FLEX
SHAFT
TORQUE
(IN-LBS)



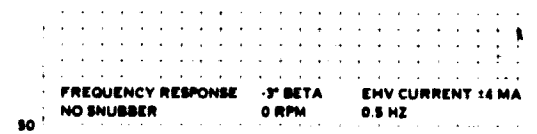
EHV
CURRENT
(MA)



MOTOR
PRESSURE
(PSIG)



VALVE
FLOW
(GPM)



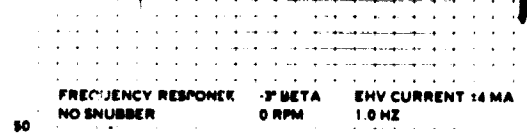
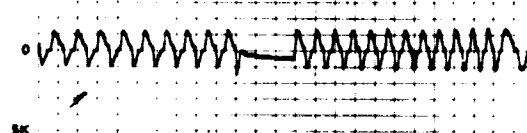
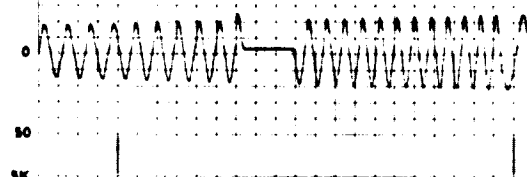
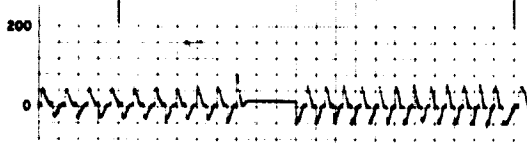
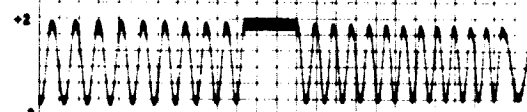
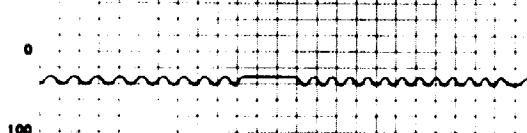
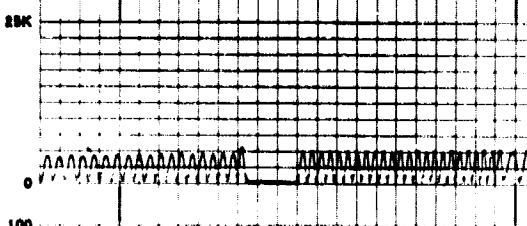
FREQUENCY RESPONSE
NO SNUBBER

-3° BETA
0 RPM

EHV CURRENT 14 MA
0.5 HZ

2 MM/SEC

5 MM/SEC



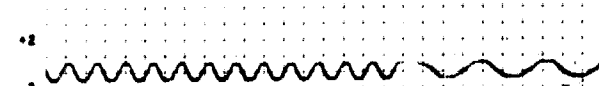
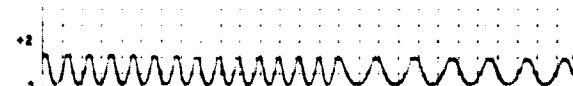
FREQUENCY RESPONSE
NO SNUBBER

-3° BETA
0 RPM

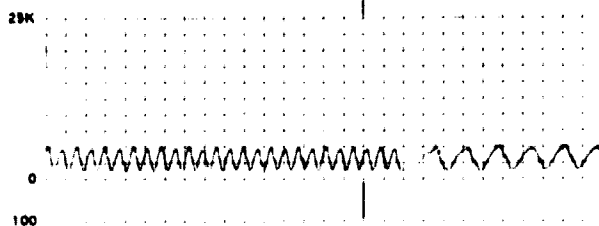
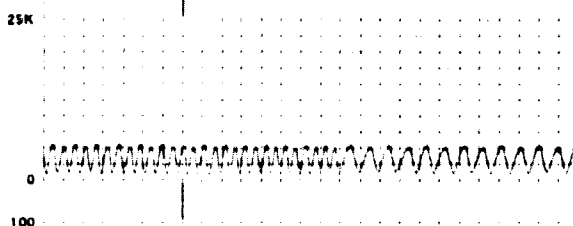
EHV CURRENT 14 MA
1.0 HZ

5 MM/SEC

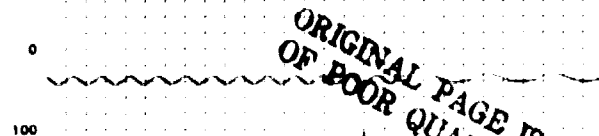
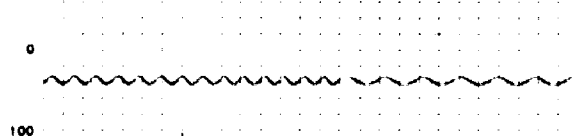
ACTUAL
BETA
(DEGREES)



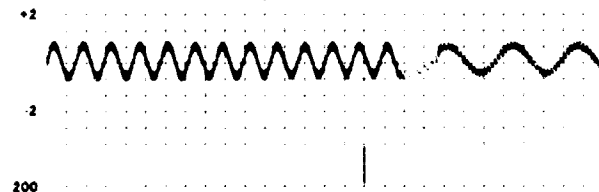
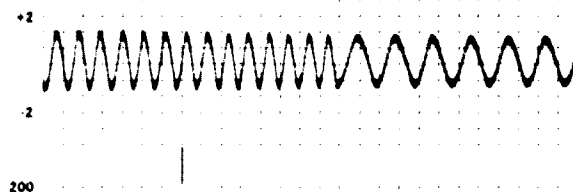
FLEX
SHAFT
SPEED
(RPM)



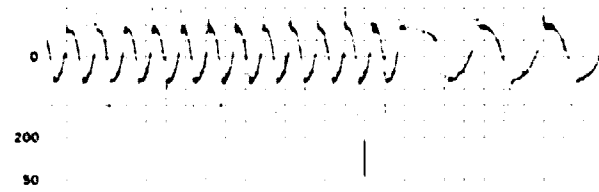
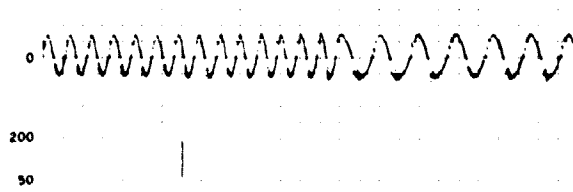
BETA
COMMAND
(DEGREES)



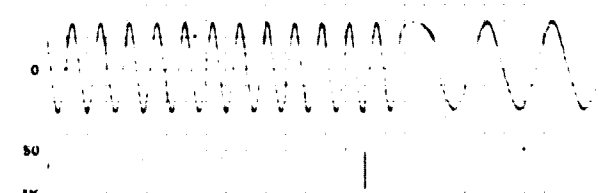
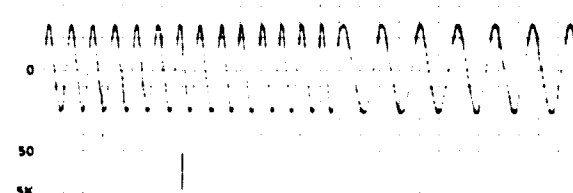
BETA
FEEDBACK
(DEGREES)



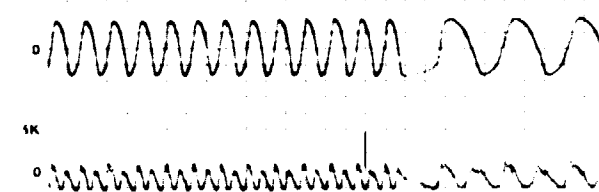
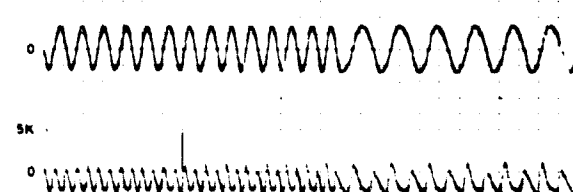
FLEX
SHAFT
TORQUE
(IN-LBS)



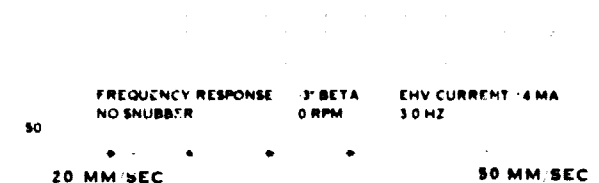
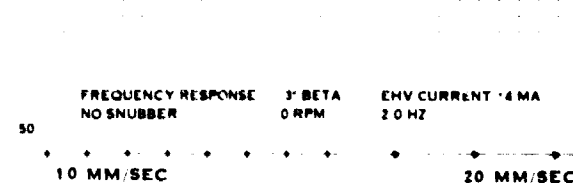
EHV
CURRENT
(MA)



MOTOR
PRESSURE
(PSIG)



VALVE
FLOW
(GPM)



ORIGINAL PAGE IS
OF POOR QUALITY

FREQUENCY RESPONSE
NO SNUBBER

3° BETA
0 RPM

EHV CURRENT 4 MA
20 HZ

FREQUENCY RESPONSE
NO SNUBBER

3° BETA
0 RPM

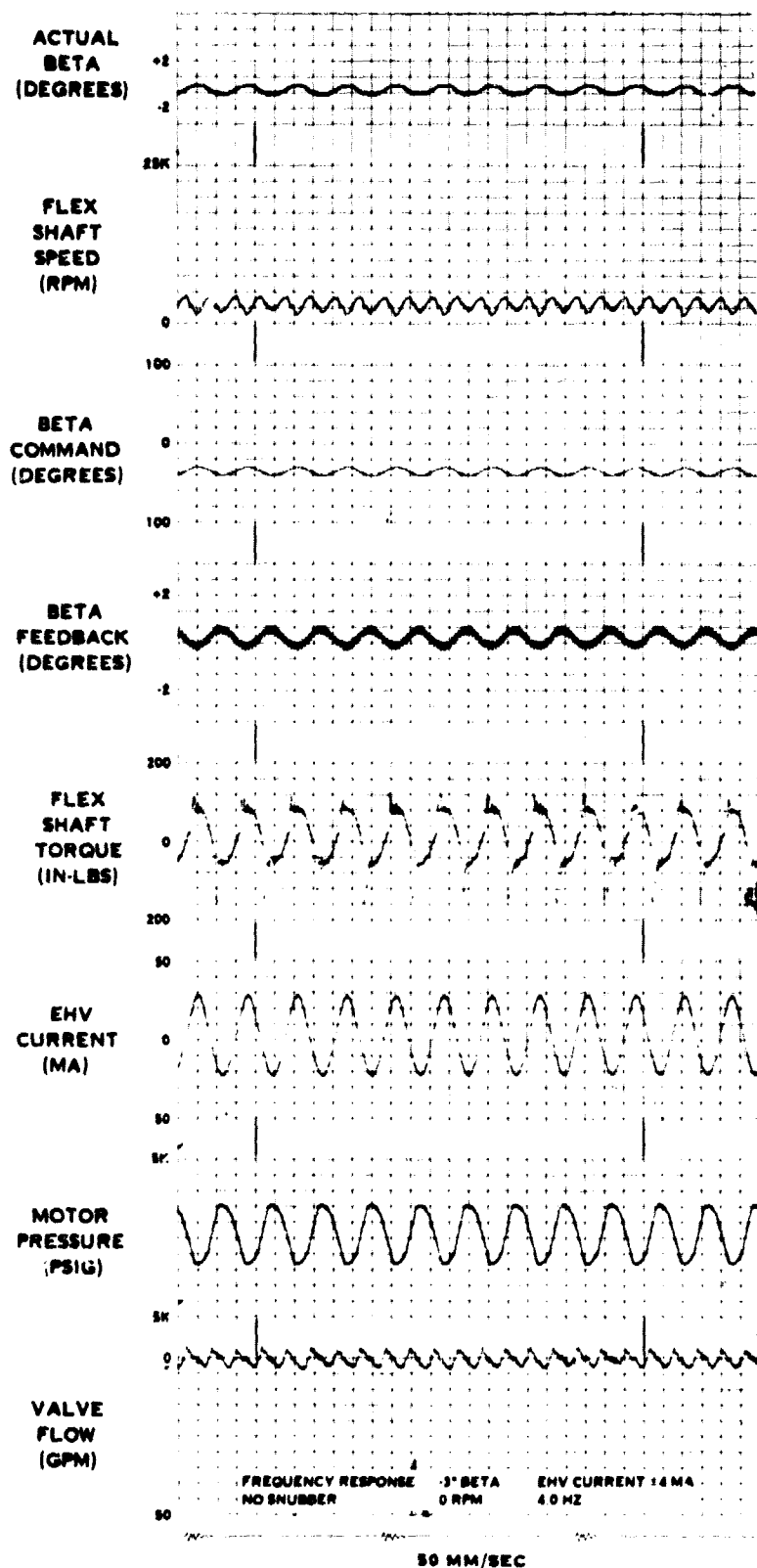
EHV CURRENT 4 MA
30 HZ

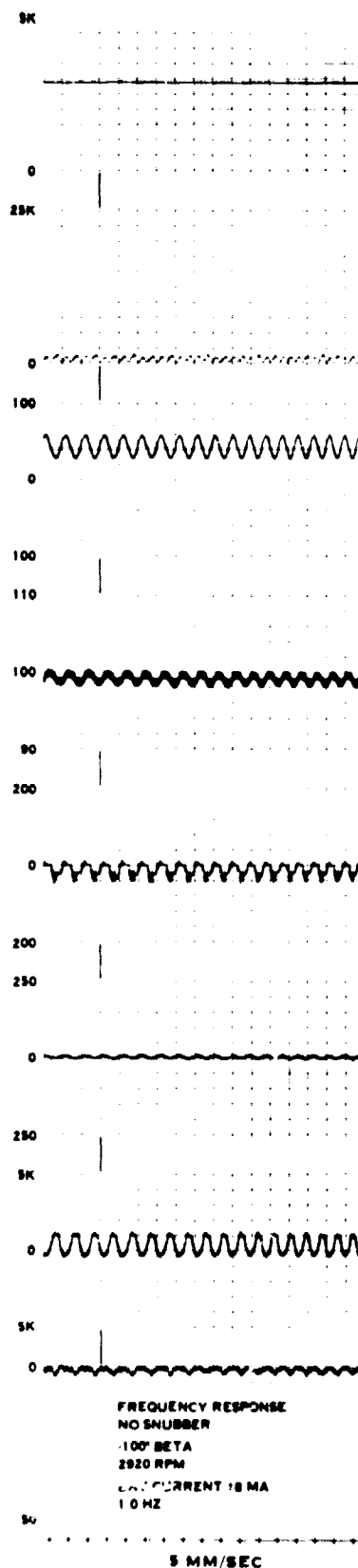
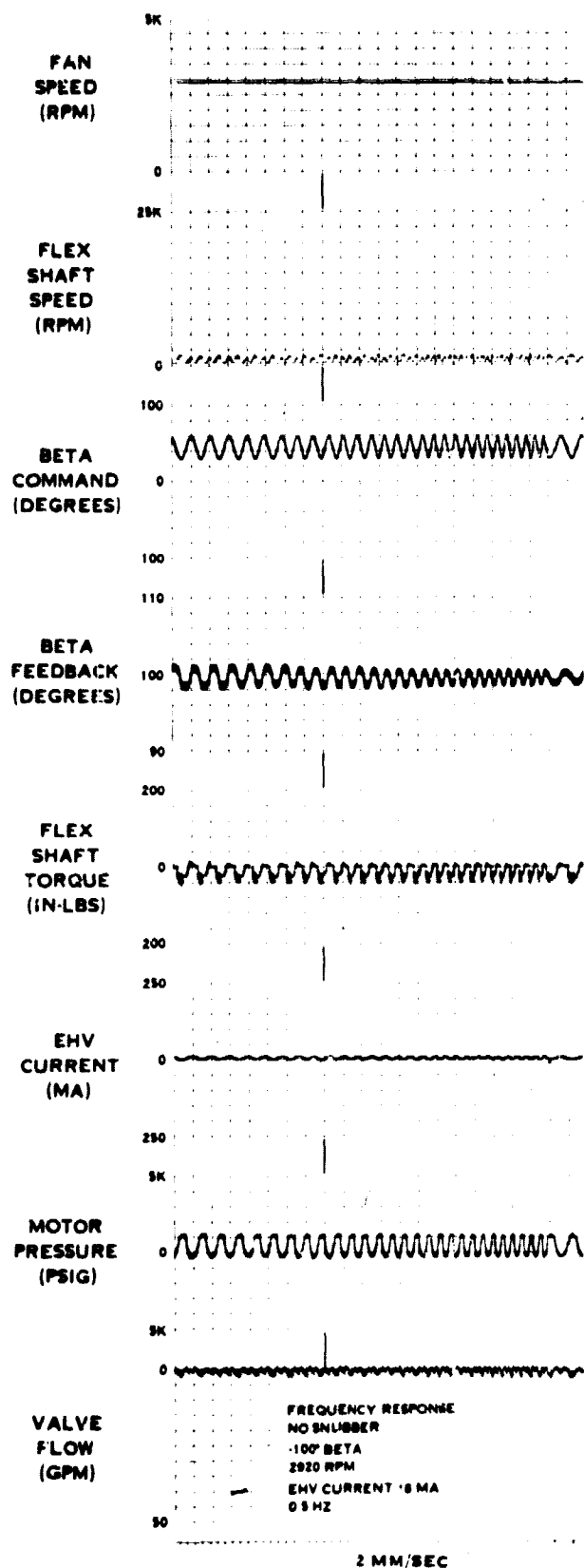
10 MM/SEC

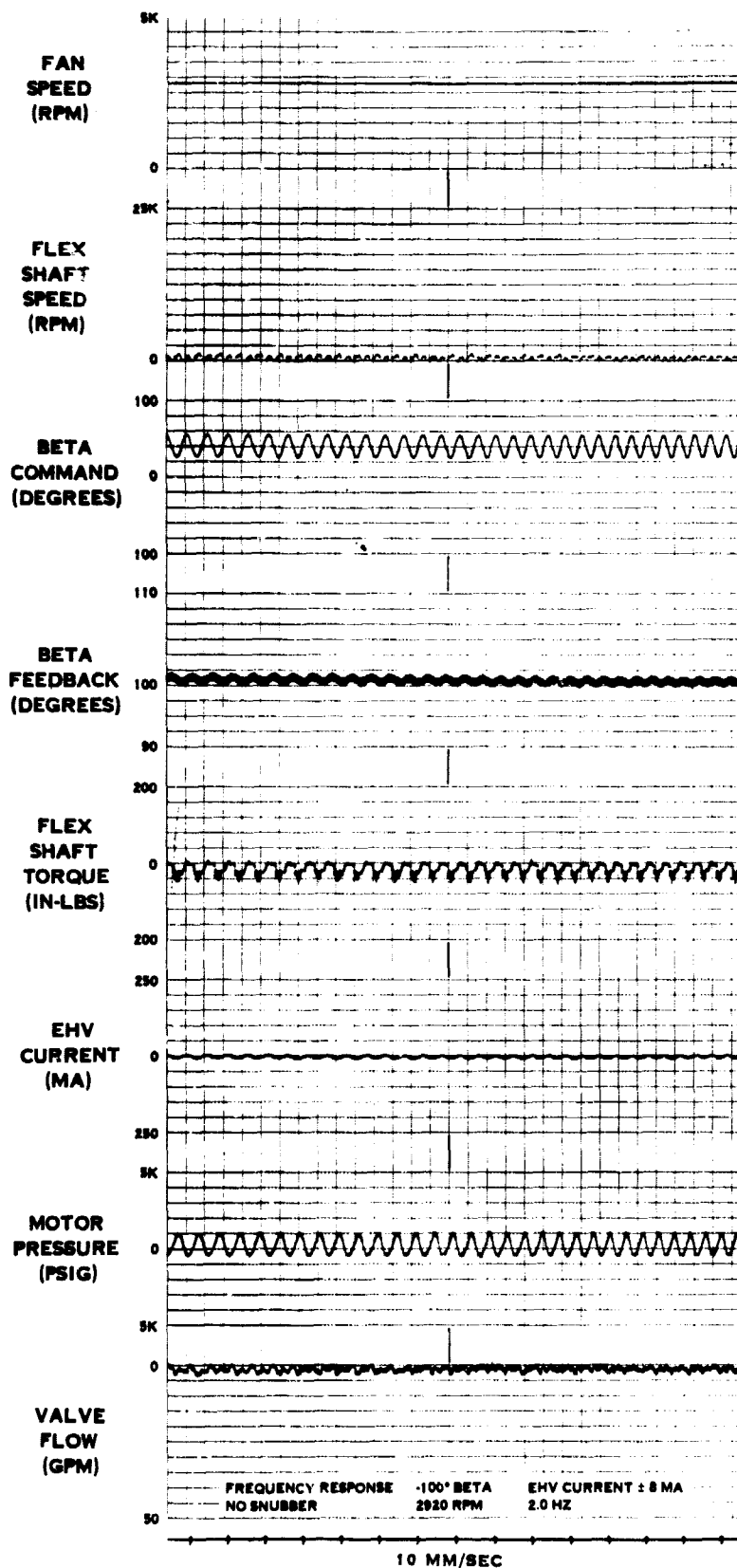
20 MM/SEC

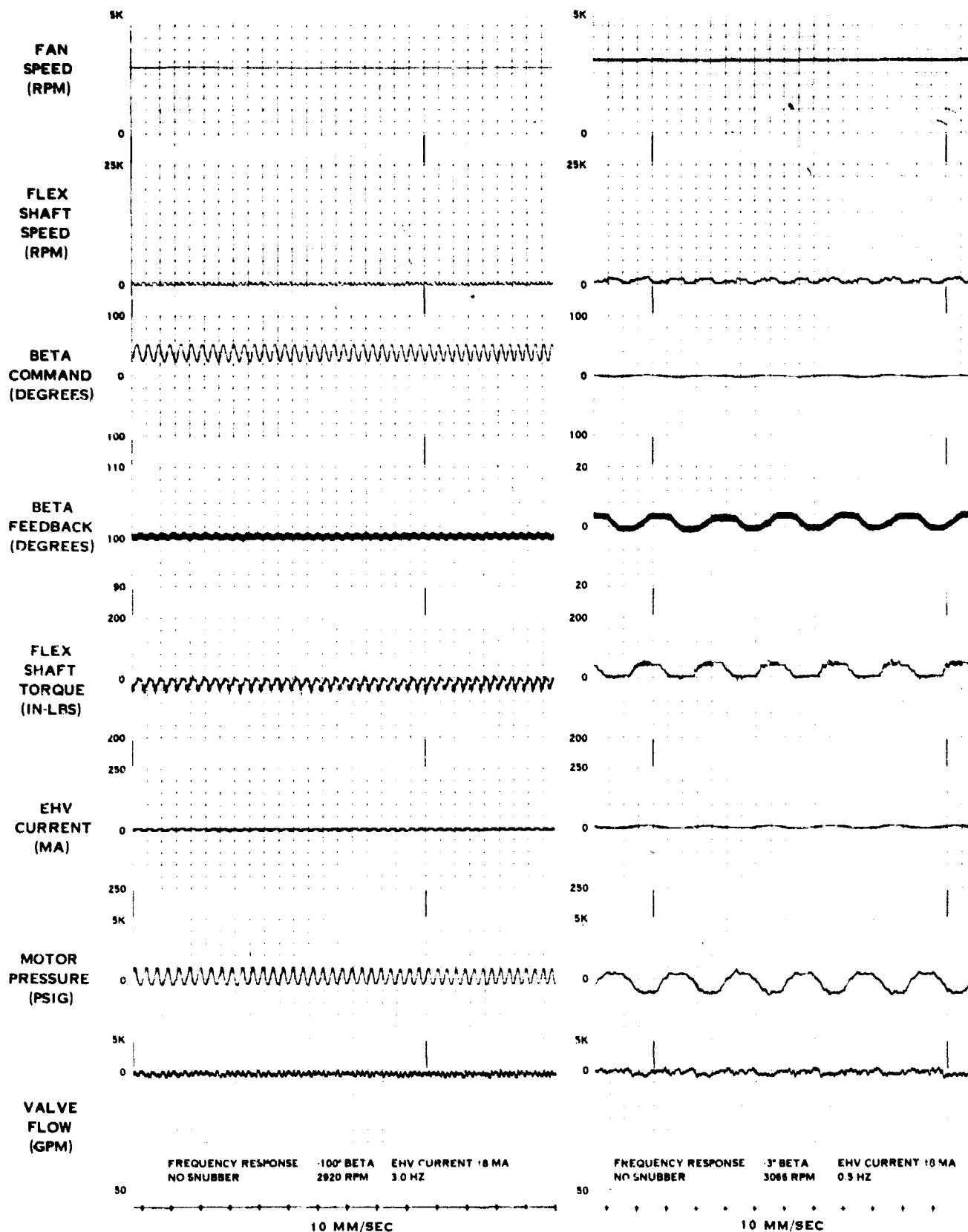
20 MM/SEC

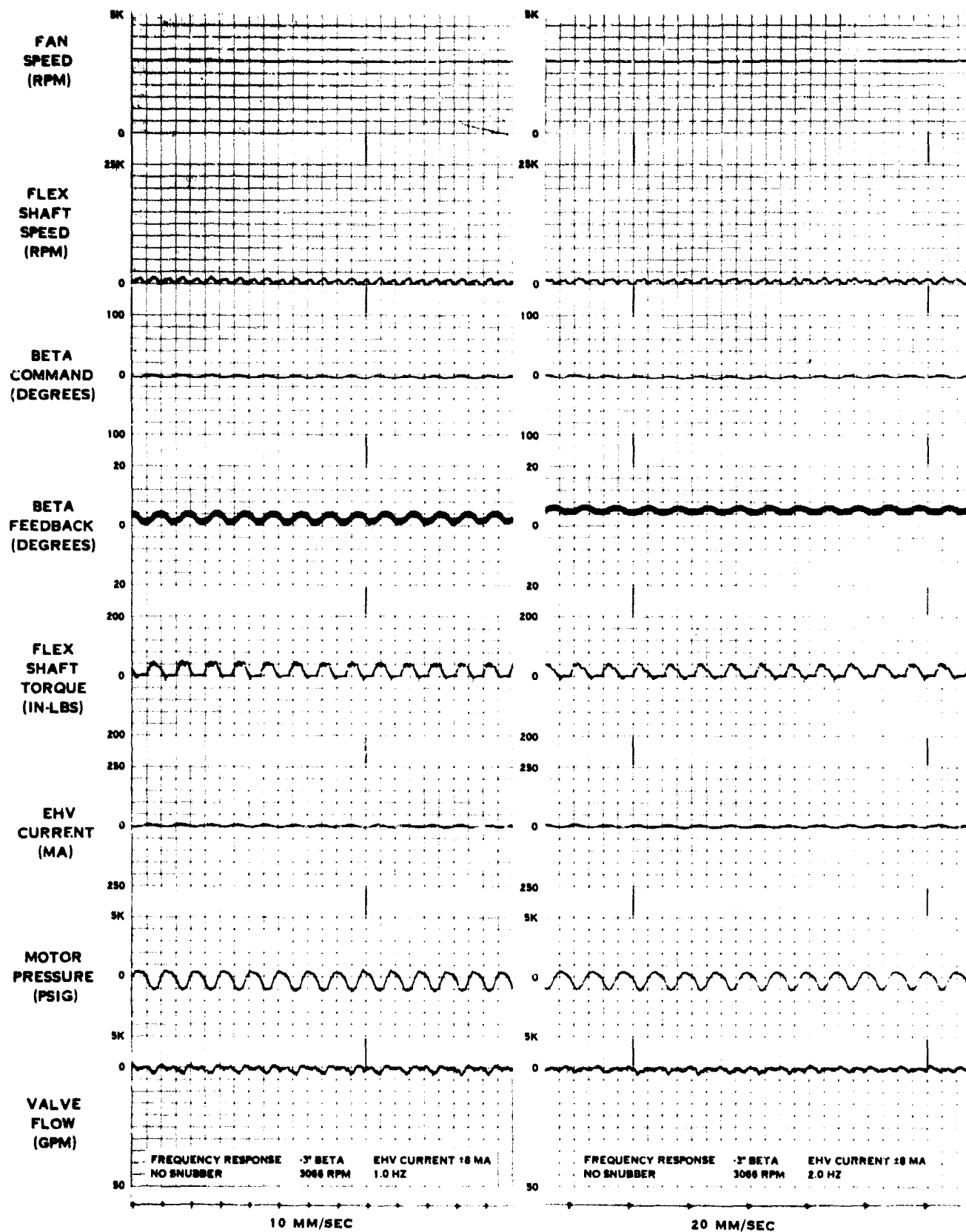
50 MM/SEC

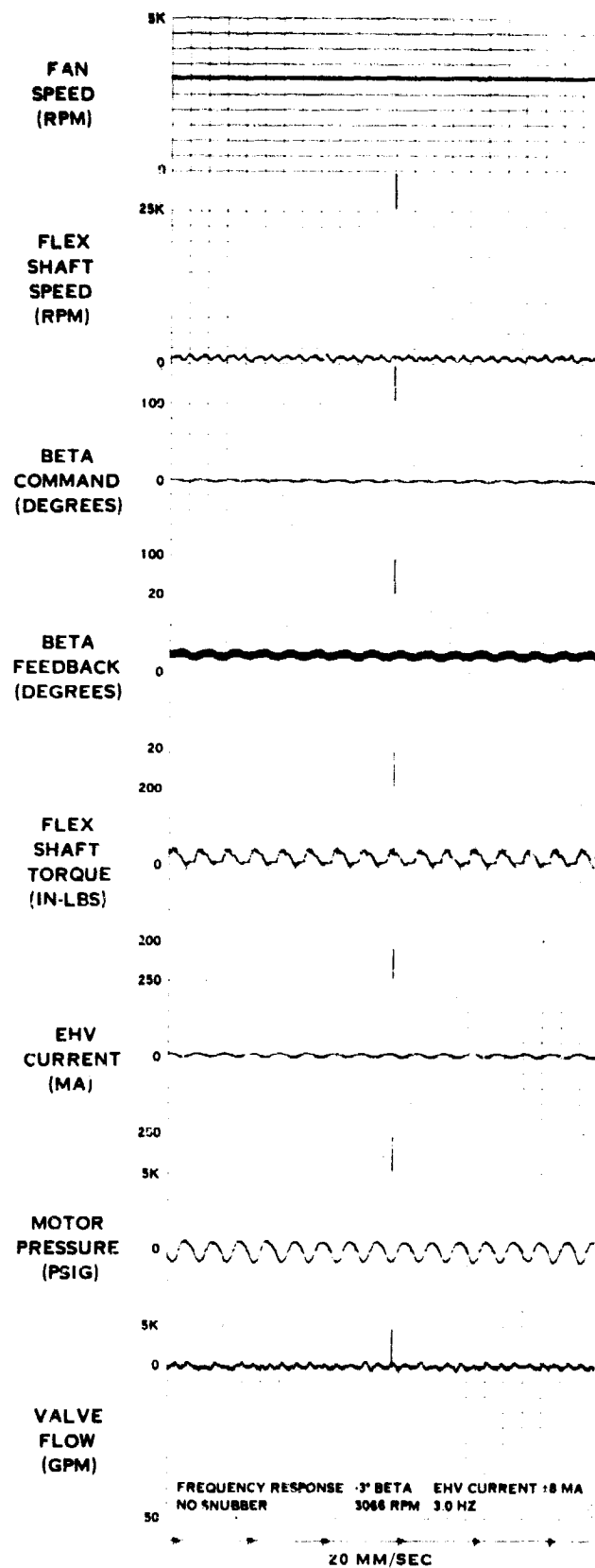


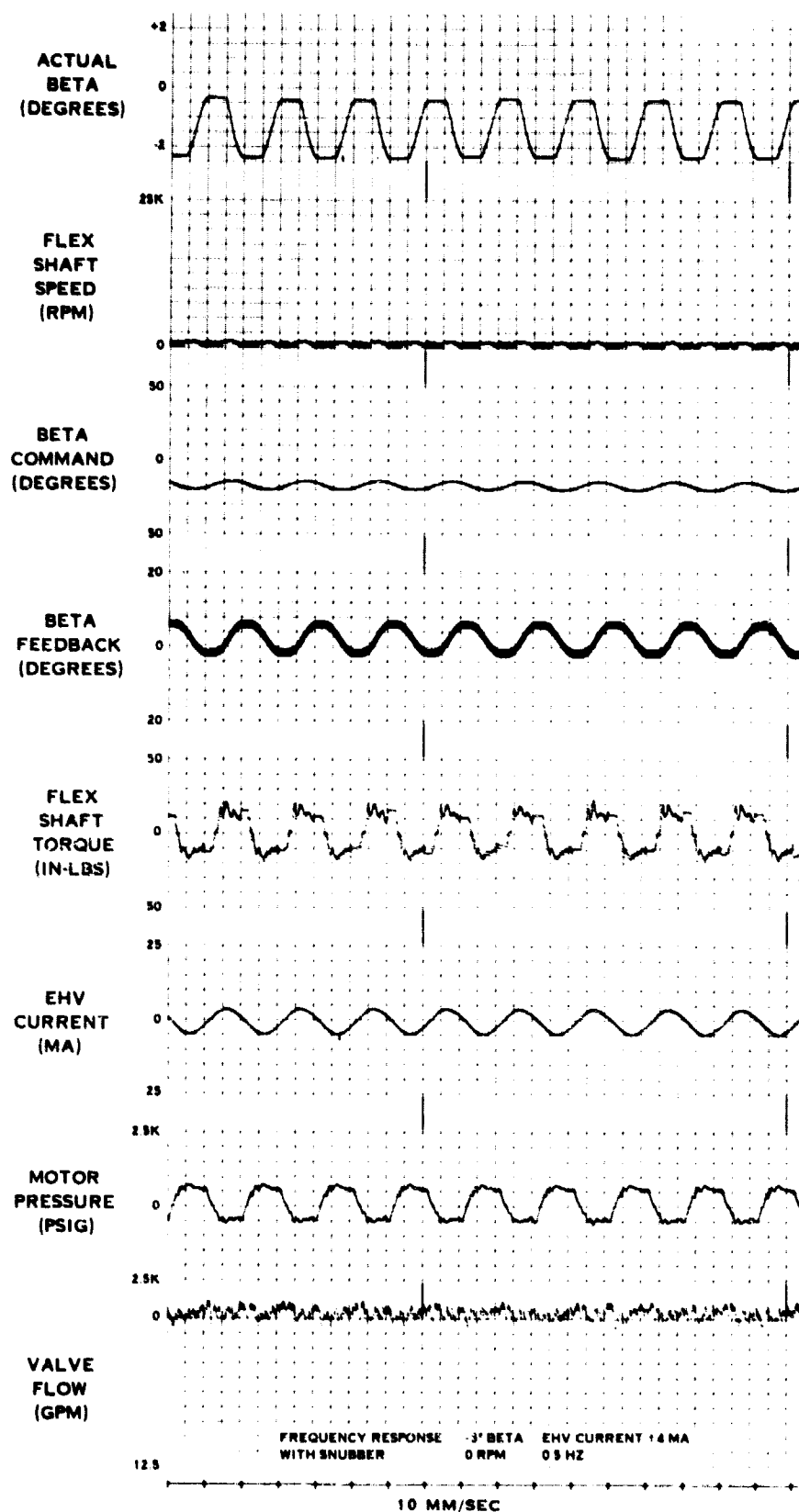


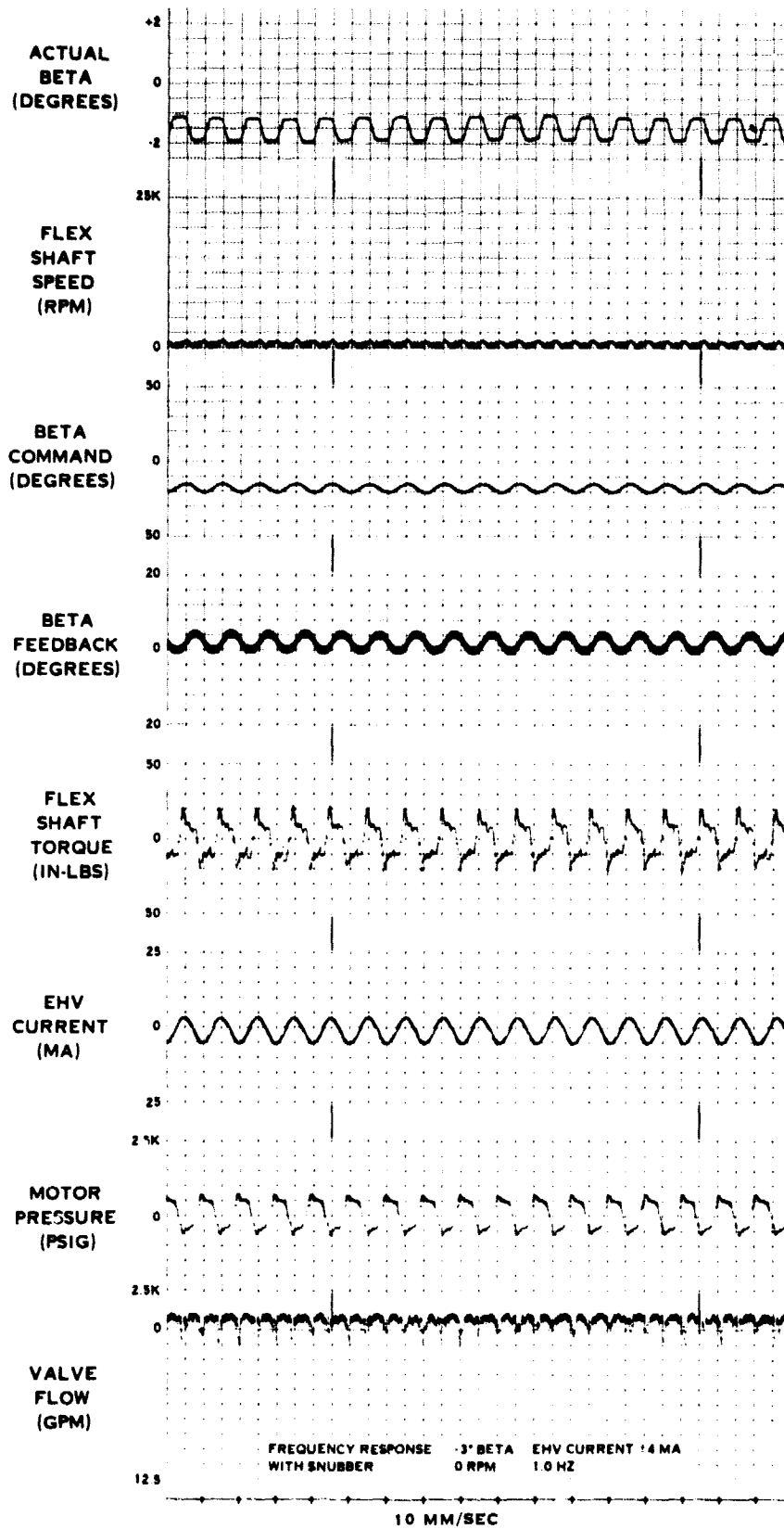


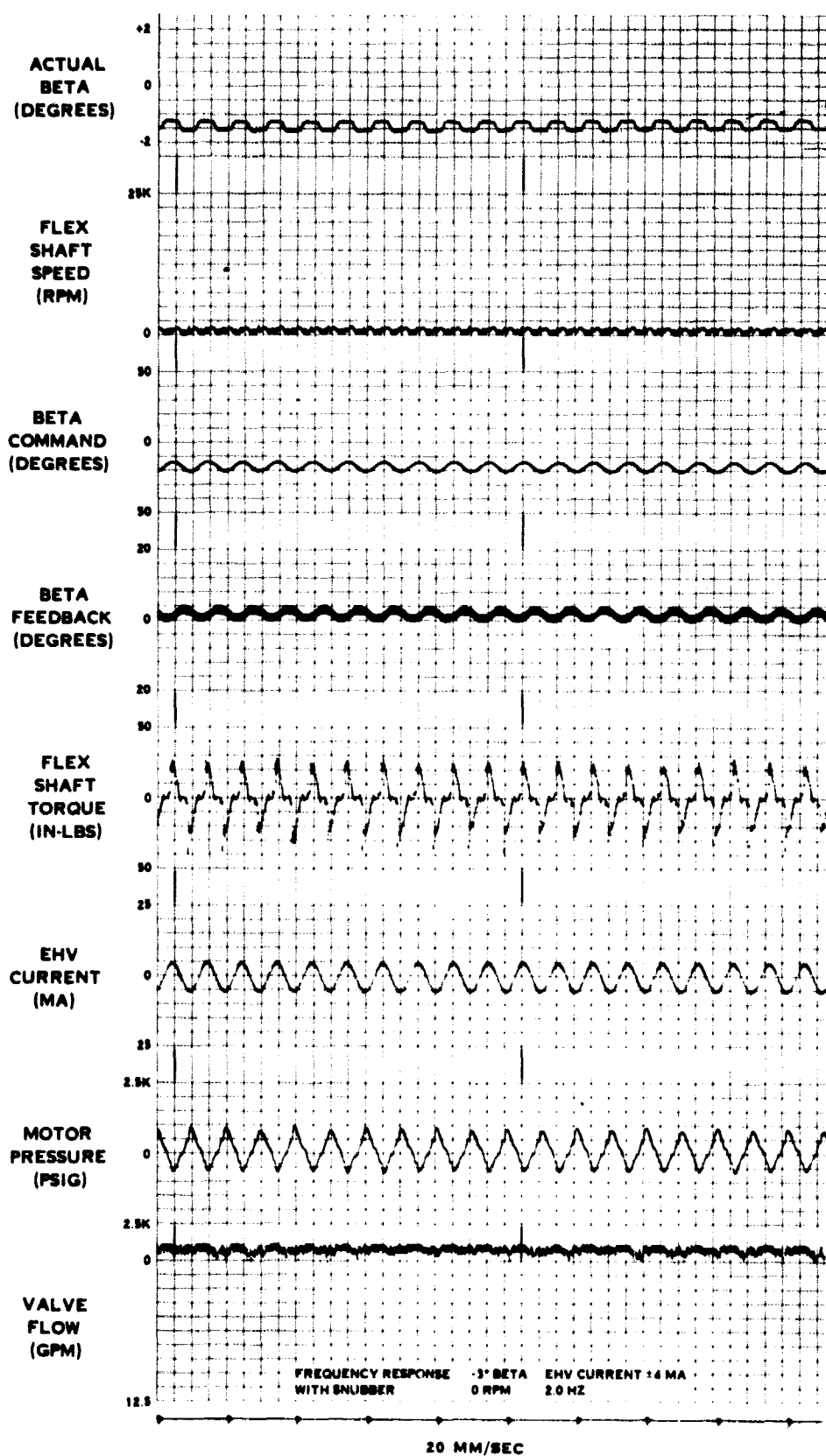


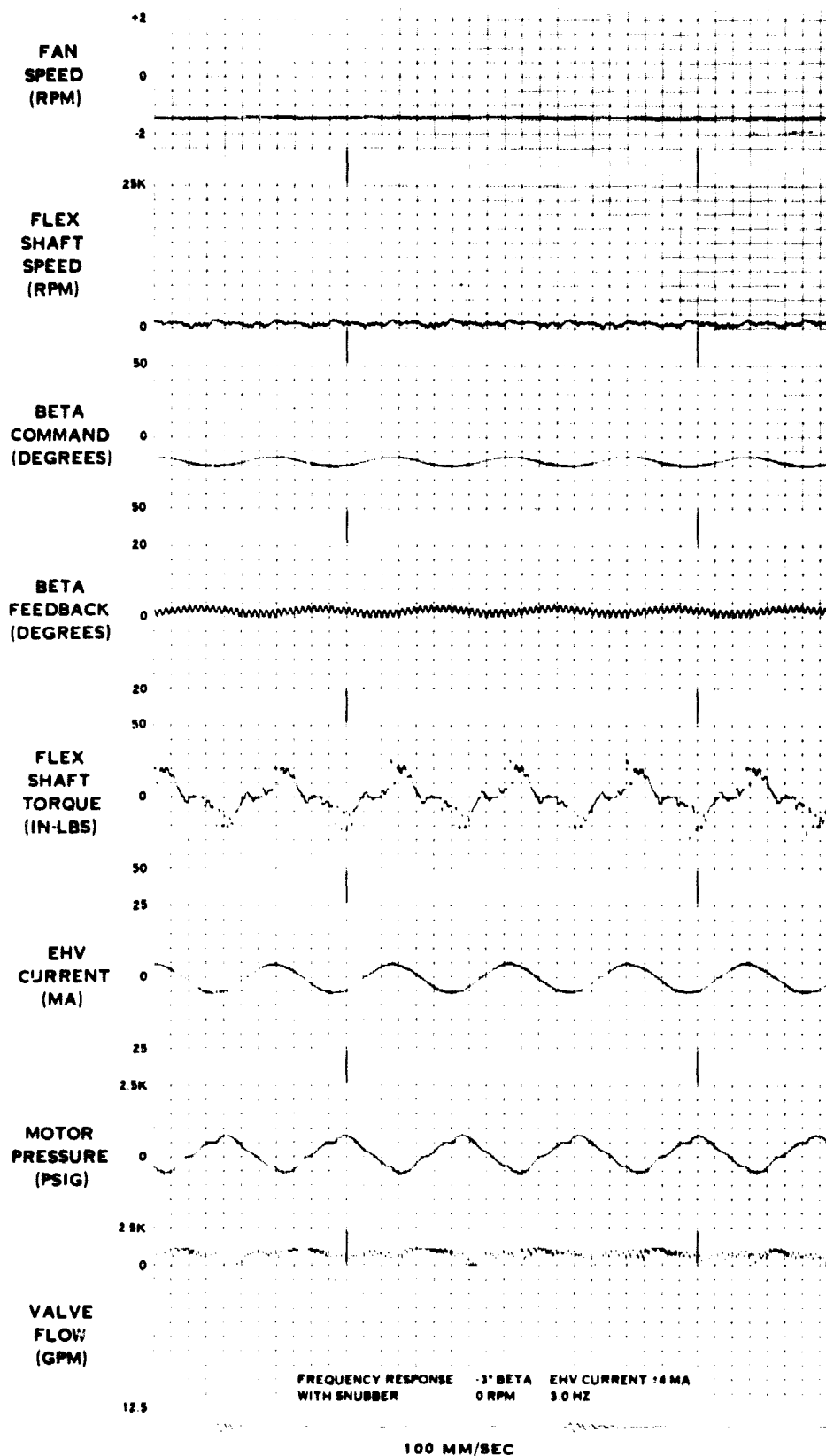


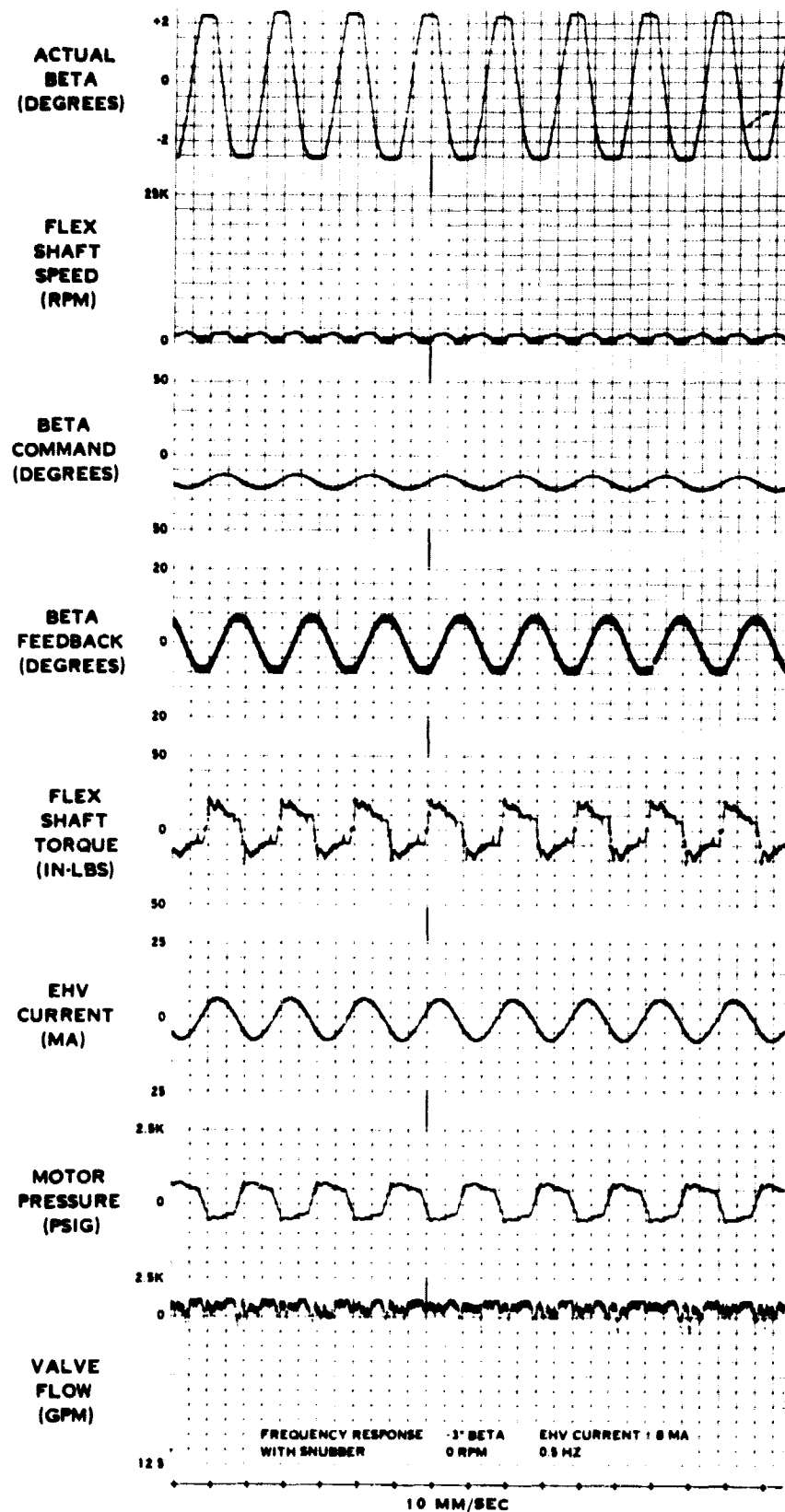


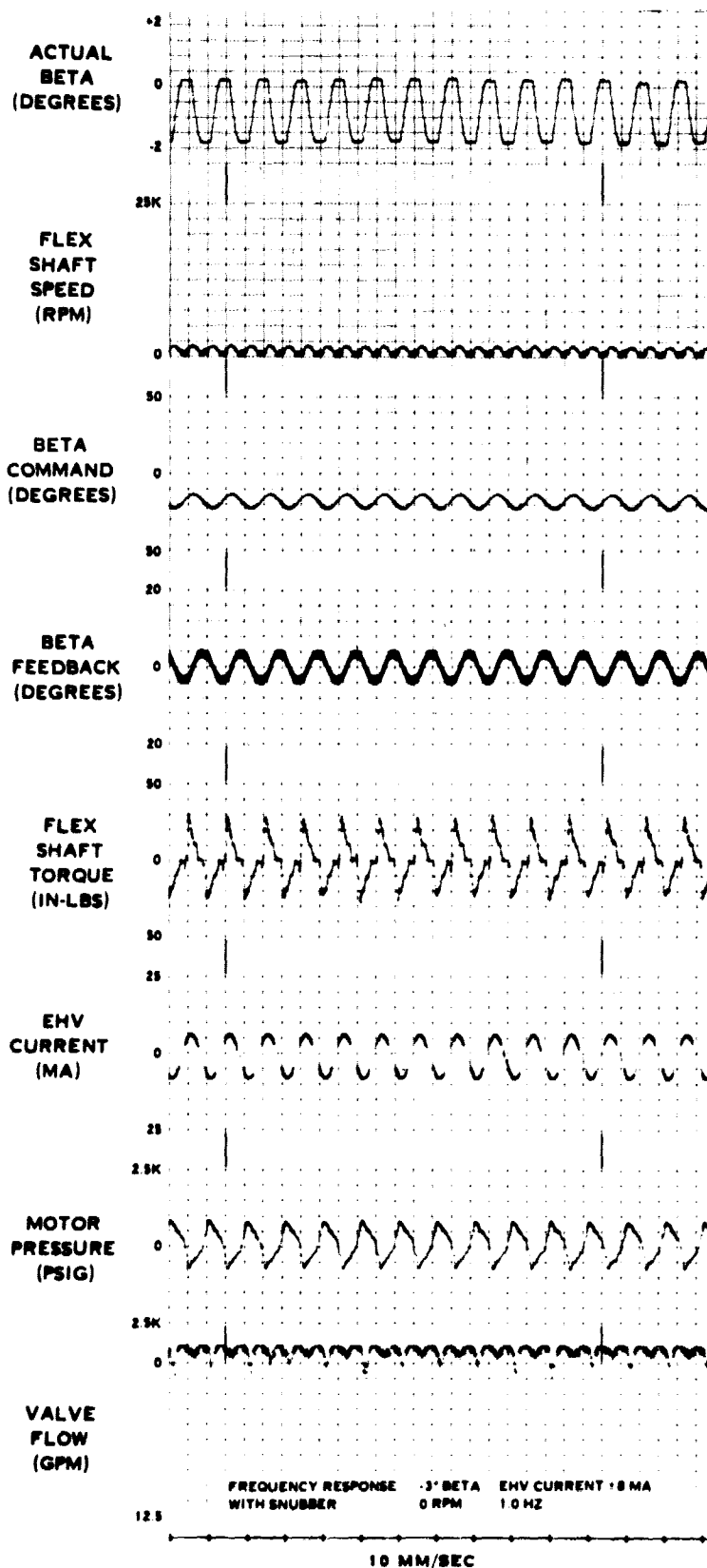


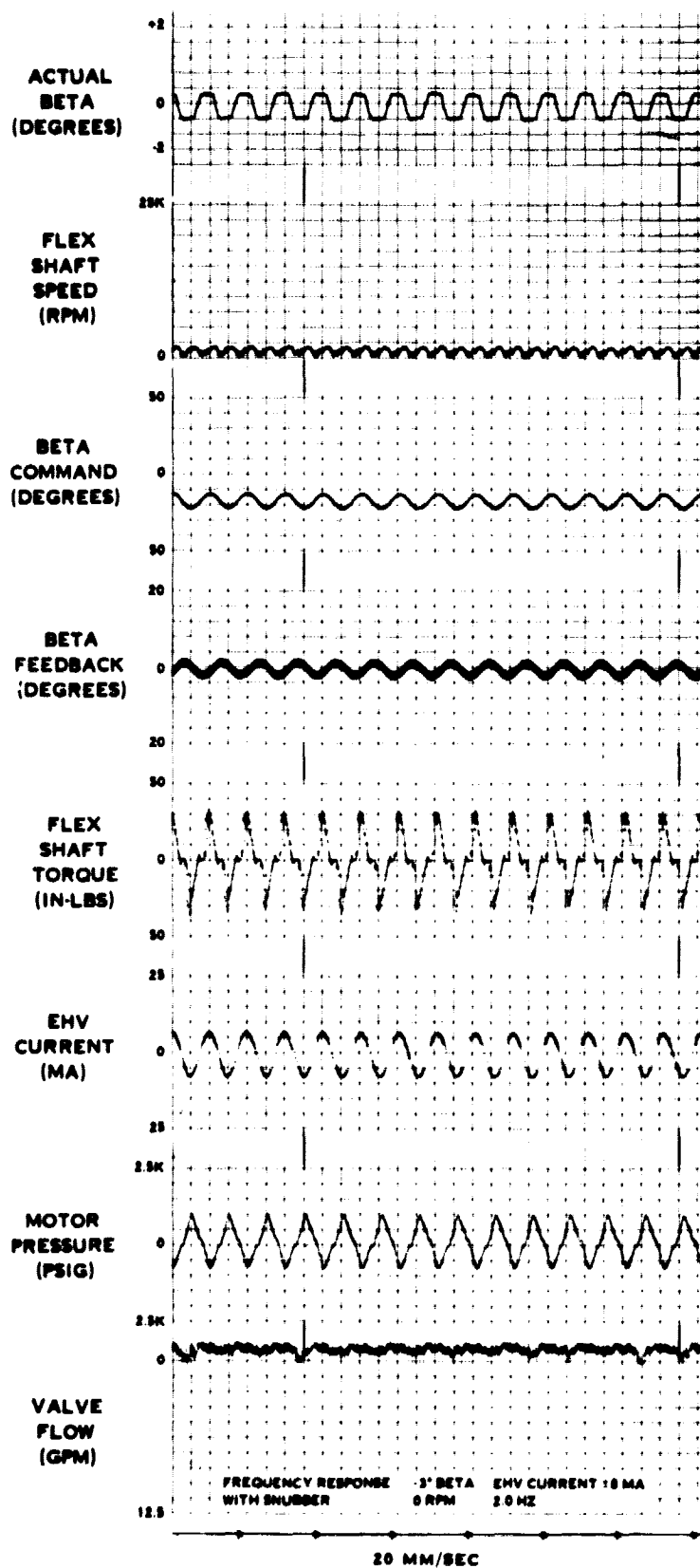


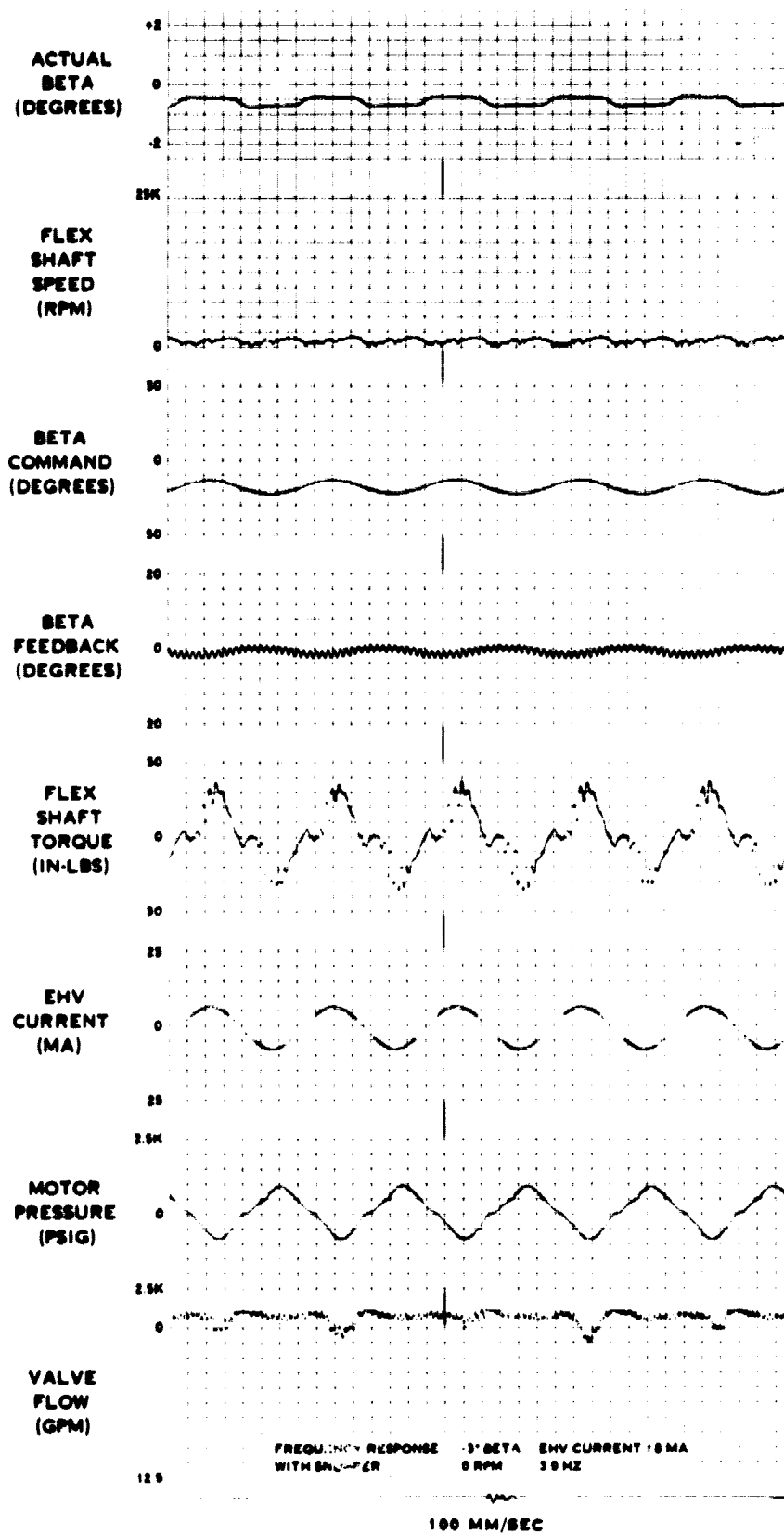


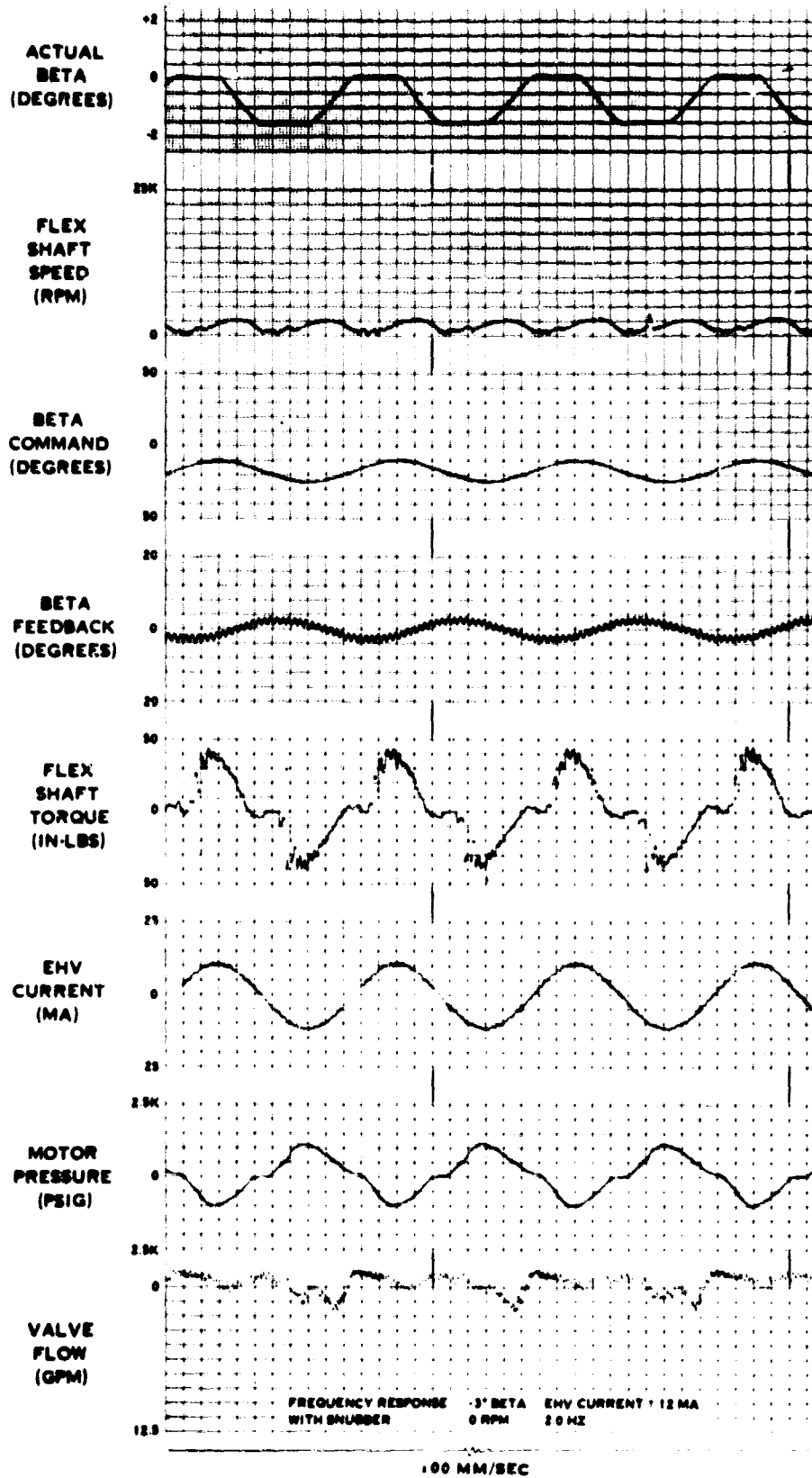


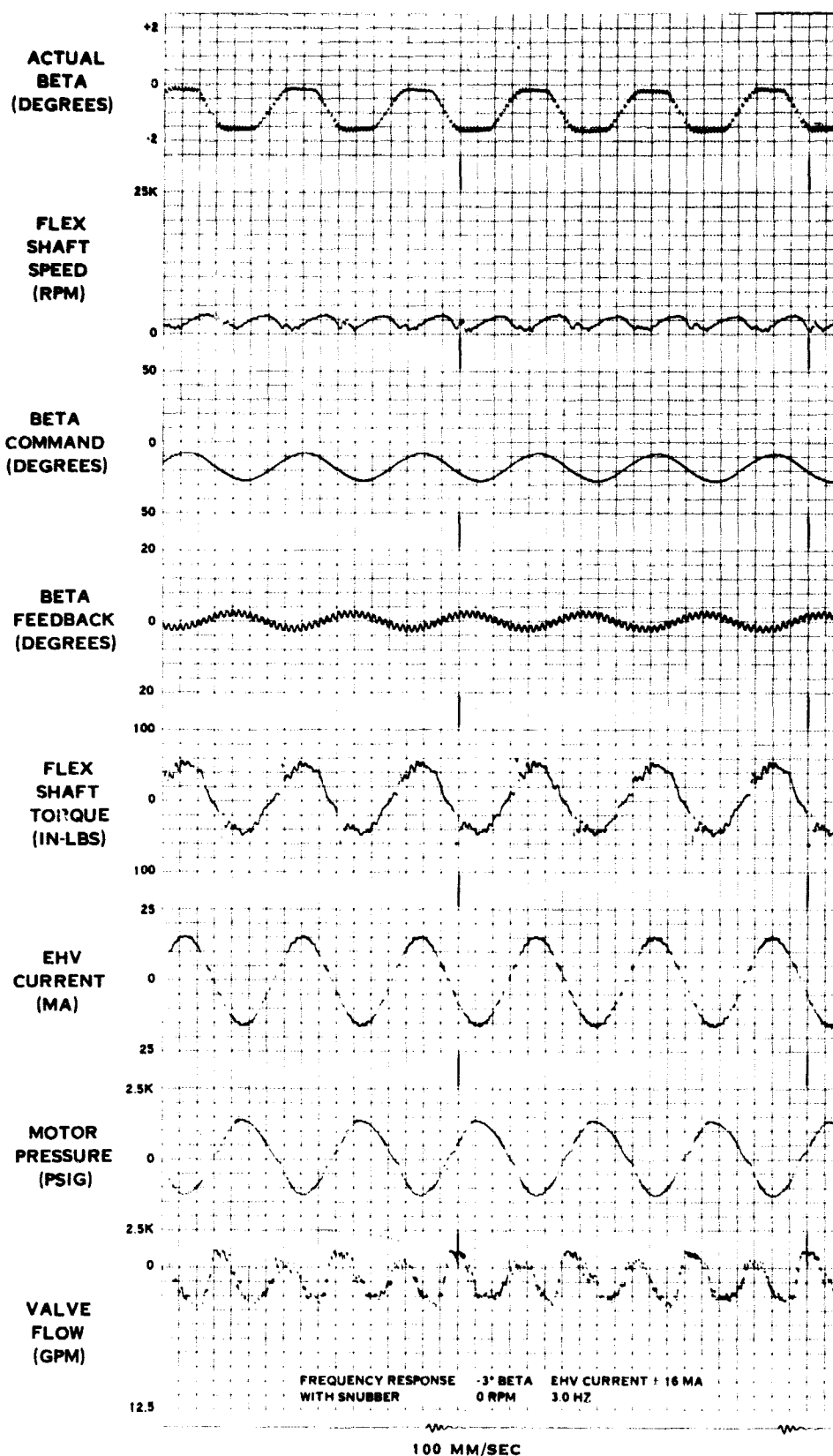


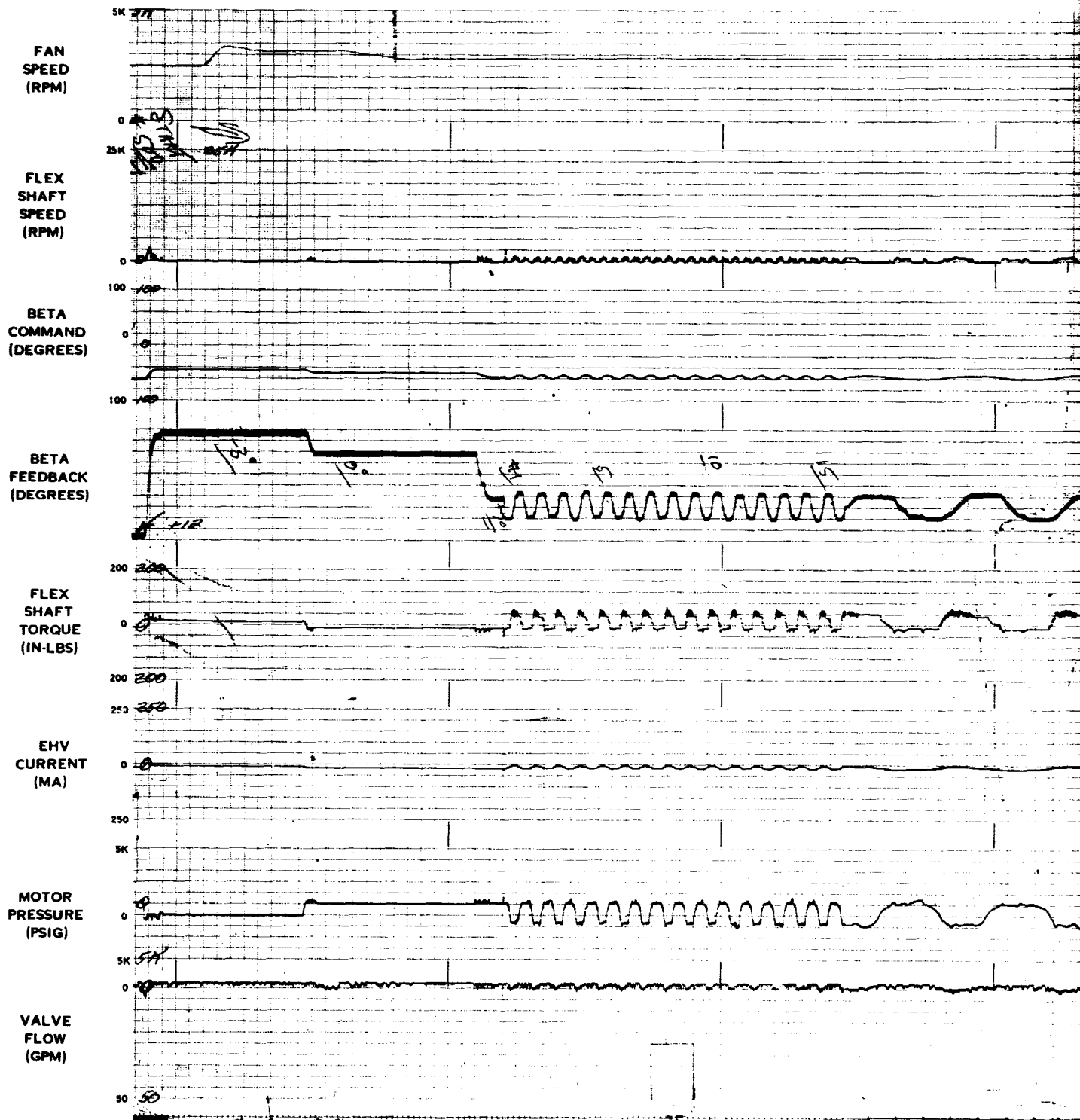








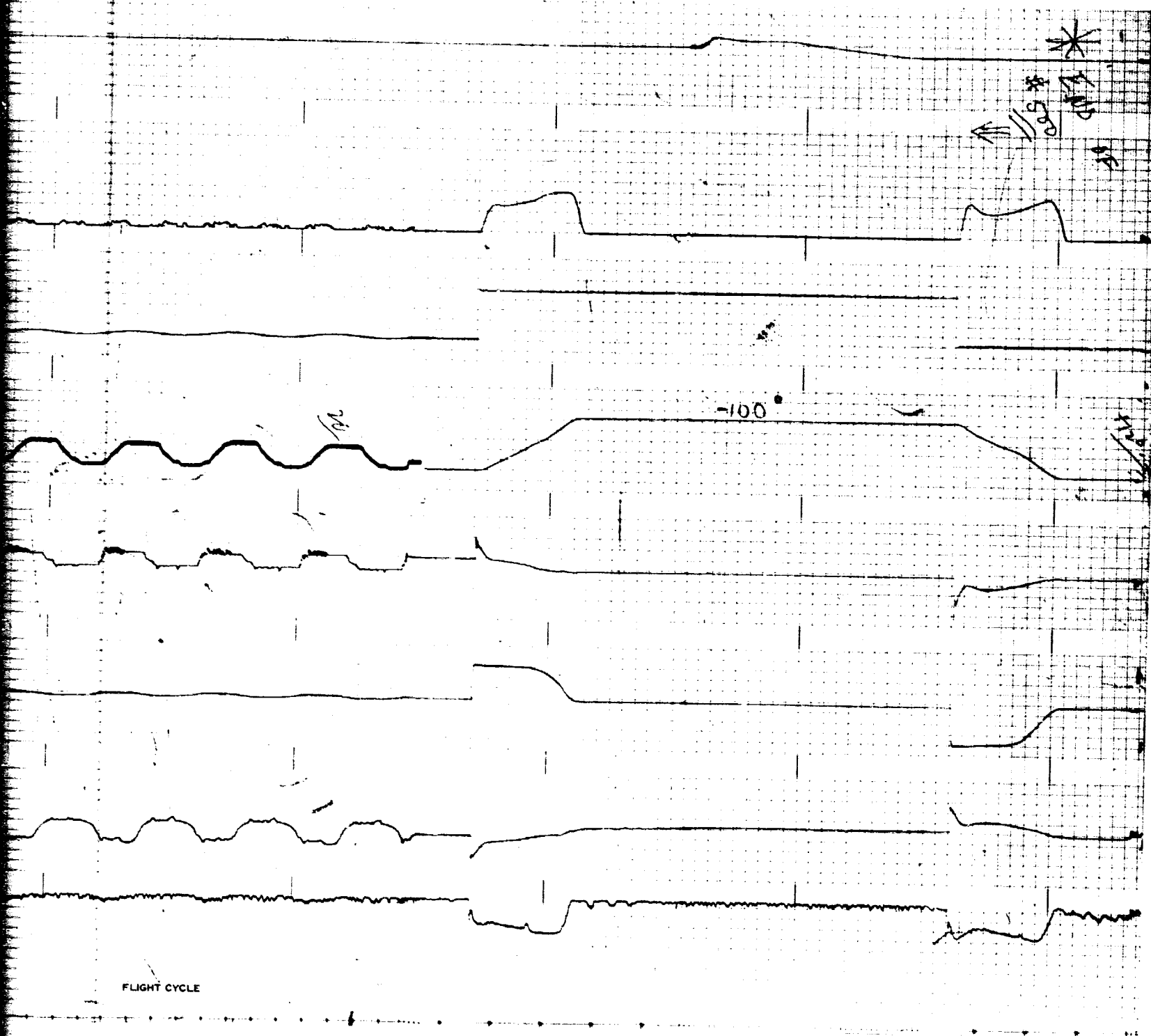




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OF POOR QUALITY

2 MM/SEC

/ FOLDOUT FRAME



FLIGHT CYCLE

20 MM/SEC

2 MM/SEC

20 MM/SEC

ORIGINAL PAGE IS
OF POOR QUALITY

119

2 FOLDOUT FRAME

PAGE 118 INTENTIONALLY BLANK

APPENDIX D

LOG SHEETS

Hamilton Standard
3509 LOCKS, CONNECTICUT • U.S.A.

U
A.

LOG OF TEST
ENGINEERING LABORATORIES

WIG NO. C-27

TYPE OF TEST

W.P.I. NO. 109-002-003A

DATE 10-30-75
ENGINEER A. S. Smith
OPERATORS F. S. Smith

PLAN OF TEST NO.
SERIAL NO.

PART NO.

UNITS →	TIME	RPM	G-Box Accel	VIBRATION VERT HORZ	REMARKS
	100		20	0 0	
	1000		20	0 0	
	1500		20	0 0	
	2000		20	0 0	
	2500		20	.1 .1	
	3000		20	.2 .1	WITH BELT ADDED
	3000		20	.1 .1	WITHOUT BELT

ORIGINAL PAGE
OF FOUR

REPORT NO.
HSER 7002

LOG OF TEST

DATE _____ ET OF _____
ENGINEER _____ OPERATORS _____

PLAN OF TEST NO. 222 PT-31 10-1-10
SERIAL NO. 1 PART NO. 222-10-1-10

FIG NO. 1.2

[illegible]

WPI NO.

[illegible]

REPORT NO.
HSER 7002

REMARKS:

PAGE NO
127

an million Standard
DSOR LOCKS, CONNECTICUT • U.S.A.

LOG OF TEST ENGINEERING LABORATORIES

295

TYPE OF TEST

w.p.t. no.

Estimated Time: 10-15 min

PLAN OF TEST
SERIAL NO.

PLAN OF TEST NO. 222 PT-31-Rev A
SERIAL NO. 1 PART NO. 76-1500-1

DATE 11/1/75

ENGINEER *McL. 30-1*

OPERATORS *H. J.*

REPORT NO.

HSER 7002

Ques. How to regulate Press with Press Relief valve in line, used Press Regulator in Pump -- Give Press. Reading on 0-200 Psi gauge.

PAGE NO

LOG OF TEST

DATE 11-20-73 BY 1 OF
ENGINEER D. L. BROWN
OPERATORS J. J. BROWN

5 NO.
TYPE OF TEST
VPI NO.

222 PT-31 Rev A
PART NO. 15200-1

PART NO. 550-1

[illegible]

ORIGINAL PAGE IS
OF POOR QUALITY

REMARKS:

111 7508 HYL oil

15.4.3

PAGE NO
129

REPORT NO.
HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

DATE 11-2-75
ENGINEER D. J. [illegible]
OPERATORS [illegible] 2 of

CM 18 18
EST NO 3441
TYPE OF TEST
(5) COG 014

2001-2002 11/11/02 4.3

PLAN OF TEST NO. 22291-31200A

PART NO. 70-100-1

SEMI NO.

[illegible]

710 1A178036, 1A

STANIS

PAGE NO
131

REPORT NO.
HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

DATE 11.2.75
ENGINEER D. J. LLOYD
OPERATORS T. D. WILKINSON

RIG NO. 6-7

TYPE OF TEST ☒ **TEST**

TYPE OF TEST G.E. WETTED DRYING
W.P.I. NO. 109-C07-402B

2.2 FUNCTIONAL TEST

PLAN OF TEST NO. 222PT-31 Rev. H
SERIAL NO. PART NO. 763529

[illegible]

REMARKS:

REPORT NO.
HSER 7002

PAGE NO
133

LOG OF TEST ENGINEERING LABORATORIES

DATE 11-26-72 SHEET 13 OF 18
ENGINEER 185001
OPERATORS

134

97-908-603-10F B
PLAN OF TEST NO. 222PT-31 Rev A
SERIAL NO. PART NO. 762570

[illegible]

REMARKS

PAGE NO

REPORT NO.
HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

SHEET 6 OF 11
DATE 11-28-75
ENGINEER D. Smith
OPERATORS 11/28/75

MG NO.

[illegible]

W.P.I. NO.

SERIAL NO.

PART NO. 10, 100

UNITS	TIME	1000	1001	1002	1003	1004	1005	1006	1007	1008	1009	1010	1011	1012	1013	1014	1015	1016	1017	1018	1019	1020	1021	1022	1023	1024	1025	1026	1027	1028	1029	1030	1031	1032	1033	1034	1035	1036	1037	1038	1039	1040	1041	1042	1043	1044	1045	1046	1047	1048	1049	1050	1051	1052	1053	1054	1055	1056	1057	1058	1059	1060	1061	1062	1063	1064	1065	1066	1067	1068	1069	1070	1071	1072	1073	1074	1075	1076	1077	1078	1079	1080	1081	1082	1083	1084	1085	1086	1087	1088	1089	1090	1091	1092	1093	1094	1095	1096	1097	1098	1099	1100	1101	1102	1103	1104	1105	1106	1107	1108	1109	1110	1111	1112	1113	1114	1115	1116	1117	1118	1119	1120	1121	1122	1123	1124	1125	1126	1127	1128	1129	1130	1131	1132	1133	1134	1135	1136	1137	1138	1139	1140	1141	1142	1143	1144	1145	1146	1147	1148	1149	1150	1151	1152	1153	1154	1155	1156	1157	1158	1159	1160	1161	1162	1163	1164	1165	1166	1167	1168	1169	1170	1171	1172	1173	1174	1175	1176	1177	1178	1179	1180	1181	1182	1183	1184	1185	1186	1187	1188	1189	1190	1191	1192	1193	1194	1195	1196	1197	1198	1199	1200	1201	1202	1203	1204	1205	1206	1207	1208	1209	1210	1211	1212	1213	1214	1215	1216	1217	1218	1219	1220	1221	1222	1223	1224	1225	1226	1227	1228	1229	1230	1231	1232	1233	1234	1235	1236	1237	1238	1239	1240	1241	1242	1243	1244	1245	1246	1247	1248	1249	1250	1251	1252	1253	1254	1255	1256	1257	1258	1259	1260	1261	1262	1263	1264	1265	1266	1267	1268	1269	1270	1271	1272	1273	1274	1275	1276	1277	1278	1279	1280	1281	1282	1283	1284	1285	1286	1287	1288	1289	1290	1291	1292	1293	1294	1295	1296	1297	1298	1299	1300	1301	1302	1303	1304	1305	1306	1307	1308	1309	1310	1311	1312	1313	1314	1315	1316	1317	1318	1319	1320	1321	1322	1323	1324	1325	1326	1327	1328	1329	1330	1331	1332	1333	1334	1335	1336	1337	1338	1339	1340	1341	1342	1343	1344	1345	1346	1347	1348	1349	1350	1351	1352	1353	1354	1355	1356	1357	1358	1359	1360	1361	1362	1363	1364	1365	1366	1367	1368	1369	1370	1371	1372	1373	1374	1375	1376	1377	1378	1379	1380	1381	1382	1383	1384	1385	1386	1387	1388	1389	1390	1391	1392	1393	1394	1395	1396	1397	1398	1399	1400	1401	1402	1403	1404	1405	1406	1407	1408	1409	1410	1411	1412	1413	1414	1415	1416	1417	1418	1419	1420	1421	1422	1423	1424	1425	1426	1427	1428	1429	1430	1431	1432	1433	1434	1435	1436	1437	1438	1439	1440	1441	1442	1443	1444	1445	1446	1447	1448	1449	1450	1451	1
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REMARKS

PAGE NO.
137

REPORT NO.

HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

DATE 11-2-68 SHEET 1 OF 1
ENGINEER D. J. [Signature]
OPERATORS [Signature]

R/G NO. 1
TYPE OF TEST 1
I.P.I. NO. 1
PLAN OF TEST NO. 1
SERIAL NO. 1

[illegible]

* Corrected 17 June On Dec. 9

REPORT NO.
HSER 7002

LOG OF TEST
ENGINEERING LABORATORIES

DATE 11-23-75 SHEET 16 OF 16
ENGINEER W. J. ...
OPERATORS ...

RIG NO. 1
TYPE OF TEST
W.P.I. NO.

PLAN OF TEST NO. 22287-313-1
SERIAL NO. PART NO.

[illegible]

REMARKS:

REPORT NO.
HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

DATE 11-1-68 SHEET 12 OF 12
ENGINEER 5
OPERATORS 1

PLAN OF TEST NO. 222PT-31 Rev A
SERIAL NO _____

FIG. NO. G-7
TYPE OF TEST G-7
W.P.I. NO. 100-102-1026
See Act for Functional Test

UNITS	TIME	Lat	Long	Alt	Wind	Temp	Humid	Cloud	Vis	Remarks
	14-07	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-08	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-09	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-10	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-11	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-12	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-13	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-14	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-15	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-16	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-17	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-18	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-19	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-20	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-21	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-22	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-23	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-24	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-25	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-26	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-27	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-28	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-29	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-30	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-31	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-32	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-33	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-34	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-35	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-36	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-37	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-38	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-39	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-40	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38
	14-41	3 05	10 18	25	10 38	25	10 45	15 20	3 25	10 38

James A. Smith, Jr.

REPORT NO.
HSER 7002

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WINDSOR LOCKS, CONNECTICUT • U.S.A.

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LOG OF TEST

ENGINEERING LABORATORIES

11/28

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151301

PLAN OF TEST NO.

ON 18/03/2017

BADLY

2224-1

EXHIBIT
CONTENTS

1

11

STEWARTS.

PAGE NO
147

REPORT NO.
HSER 7002

10

100

12-10-68

PART NO. 162570

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PAGE NO.
149

REPORT NO.
HSEK 7002

BIG NO.	TYPE OF TEST	W.P.I. NO.	Serial No.	PLAN OF TEST NO.	PART NO.	OPERATOR
1354	24 1/2	147	Com. Deleted	Flight Cycle #47	Started	11/15
1377	26 1/2	47	2700 178	78	3550 185	74° 130° 106° 95°
1400	30 1/2	47	2700 178	78	3550 185	74° 130° 106° 95°
1402	32 1/2	47	3060 200	98	3550 185	91° 135° 107° 17°
1405	33 1/2	47	Com. Deleted	Flight Cycle #47	Started	11/15
1406	34 1/2	47	3105 201	78	3550 185	91° 135° 107° 17°
1412	42 1/2	47	Com. Deleted	Flight Cycle #47	Started	11/15
1418	45 1/2	47	2700 203	98	3550 185	91° 125° 108° 97°
1420	50 1/2	47	Com. Deleted	Flight Cycle #47	Started	11/15
1422	52 1/2	47	3064 202	98	3550 185	92° 137° 108° 97°
1425	55 1/2	47	Com. Deleted	Flight Cycle #47	Started	11/15
1430	60 1/2	47	3467 204	98	3550 185	91° 129° 108° 98°
1432	102 1/2	47	Com. Deleted	Flight Cycle #47	Started	11/15
1436	106 1/2	47	3700 200	98	3550 18	93° 130° 107° 94°
1438	108 1/2	47	Com. Deleted	Flight Cycle #47	Started	11/15
1440	110 1/2	47	3065 201	98	3550 18	92° 128° 107° 93°

REMARKS.

PAGE NO

LOG OF TEST ENGINEERING LABORATORIES

DATE 12-20-20 SHEET 20 OF 20

DATE 12-1-77
ENGINEER [Signature]
OPERATORS [Signature]

PLAN OF TEST NO. 222 PF-31
SERIAL NO. _____ PART NO. _____

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STEWART

PAGE NO
151.

REPORT NO.
HSER 7002

UNITS	TIME	LAST	TOTAL	TIME	PSIG	PSIG	PSIG	PSIG	#1 CF	#2 CF	#3 CF	#4 CF	#5 CF	19.1	20.2
1858	3	12	12	100	46	3530	18		72	102	107	100	.1	.1	.30
1900	10	24	24	10720	Flight				Cycle #104	STARTED		105			
1900	44	03	03	3054	98	3530	18		91	121	108	101	.1	.15	.20
1903	12	12	12	Completed	Flight				102	92	74	03	.1	.18	.18
2002	53	17	17	START	Flight										
2005	53	17	17	3071	151	78	3530	18	76	115	31	85	.1	.1	.55
2007	5	19	19	Completed	Flight				STARTED	Cycle #107					
2011	5	23	23	47	3066	113	48	3530	44	118	90	74	.1	.1	.50
2013	4	25	25	Completed	Flight				STARTED	Cycle #108					
2018	4	20	20	47	3066	190	48	3530	44	125	102	77	.1	.1	.20
2020	4	22	22	Completed	Flight				STARTED	Cycle #109					
2021	1	26	26	47	3066	147	78	3530	44	122	105	79	.1	.1	.20
2026	4	28	28	Completed	Flight				STARTED	Cycle #110					
2027	4	28	28	47	3065	200	78	3530	44	123	107	49	.1	.1	.20
2027	4	21	21	47	3065	200	78	3530	STARTED	Cycle #111					

REMARKS:

REPORT NO.
HSER 7002

PAGE NO

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2025 RELEASE UNDER E.O. 14176

LOG OF TEST ENGINEERING LABORATORIES

2025

FIG. NO. 1

TYPE OF TEST CR CRACK ACTUATOR FUNC

TYPE OF TEST
W.P.I. NO.

PLAN OF TEST NO. _____
SERIAL NO. _____

REV. D.

ENGINEER D. H. J. S.
OPERATORS C. H. J. S.

ENGINEER D. H. / 5-1-1
OPERATIONS 5-1-1-7

[illegible]

LOG OF TEST ENGINEERING LABORATORIES

DATE 12-27-68 SHEET 27 OF 28
ENGINEER D. J. ...
OPERATORS

REG NO.	TYPE OF TEST	W.P.I. NO.
158		

Actuals Function's Test

PLAN OF TEST NO. 22207-21 SUB
SERIAL NO. 1

PART NO.

[illegible]

PAGE NO

REPORT NO.
HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

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DATE 12-0-72 SHEET 29 OF
ENGINEER D. J. L. L.
OPERATORS

DATE	ENGINEER	OPERATORS	PLAN OF TEST NO.	222 PT-31	R-V-A	PART NO	222301
TIME	ALT	PRG	PRG	PRG	PRG	PRG	PRG
1039	42	2241	4.7	3063	216	98	3550 17.5
1042	42	2241	4.7	3063	216	98	3550 17.5
1045	42	2241	4.7	3063	216	98	3550 17.5
1050	42	2241	4.7	3063	216	98	3550 17.5
1052	42	2241	4.7	3063	216	98	3550 17.5
1054	42	2241	4.7	3063	216	98	3550 17.5
1057	42	2241	4.7	3063	216	98	3550 17.5
1100	42	2241	4.7	3063	216	98	3550 17.5
1105	42	2241	4.7	3063	216	98	3550 17.5
1107	42	2241	4.7	3063	216	98	3550 17.5
1110	42	2241	4.7	3063	216	98	3550 17.5
1112	42	2241	4.7	3063	216	98	3550 17.5
1117	42	2241	4.7	3063	216	98	3550 17.5
1119	42	2241	4.7	3063	216	98	3550 17.5
1122	42	2241	4.7	3063	216	98	3550 17.5

REPORT NO.
HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

05:58

15:40 3611

2012

7.

6722 Chrysomelidae: Curculionidae: Curculioninae

PLAN OF TEST NO.

SERIAL NO.

PART IV

DATE

613NPN3

OPERATORS

12- SHEET 32 OF 32

13346

13346

13346

TIME	REMARKS	SERIAL NO.	PART NO.
1340 4.7	Completed Flight cycle #167 and started #168		
1340 3 24 25	4.7 2700 220 90 3550 17.5 34° 131° 111° 113° .1 .2 70106		
1341 3 25 25	4.7 Completed Flight cycle #170 and started #171		
1342 3 27 25	4.7 3068 220 90 3550 17.5 74° 143° 111° 116° .1 .2 03048		
1343 3 28 25	4.7 Completed Flight cycle #171 and started #172		
1344 3 29 25	4.7 Completed Flight cycle #172 and started #173		
1345 4 05 25	4.7 3433 221 90 3550 17.5 94° 136° 121° 116° .1 .2 07006		
1346 4 10 25	4.7 Completed Flight cycle #173 and started #174		
1347 4 14 25	4.7 Completed Flight cycle #174 and started #175		
1348 4 19 25	4.7 2700 224 90 3550 17.5 34° 139° 122° 117° .1 .2 70110		
1349 4 24 25	4.7 Completed Flight cycle #175 and started #176		
1350 4 29 25	4.7 Completed Flight cycle #176 and started #177		
1351 4 34 25	4.7 3068 222 90 3550 17.5 71° 143° 121° 116° .1 .2 03048		
1352 4 39 25	4.7 Completed Flight cycle #177 and started #178		
1353 4 44 25	4.7 Completed Flight cycle #178 and started #179		
1354 4 49 25	4.7 3408 222 90 3550 17.5 71° 136° 121° 116° .1 .2 06053		

REMARKS:

163

REPORT NO.
HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

DATE 12-10-75, 37 or

FIG NO 6-7

6-7% OF TEST

CI. OC. SEC. ACQUATES
100-003-AC2B

Endurance Test PLAN OF TEST NO. _____
SERIAL NO. _____

PART NO. 70-896-1C

[illegible]

UPPTS	TIME	FOR	TOTAL	TIME	RIC	LINE	Flow	PISC	15KG	PSC	G/B	#1	#3	#1	% of	Mus	Mus	Days
		Time	Time		BCAL	Flow	Cil	Flow	Flow	Flow	G/B	Flow	Flow	Flow	Flow	Flow	Flow	Flow
13.58	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.2	-3°
14.01	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.03	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.05	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.07	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.09	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.11	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.13	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.15	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.17	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.19	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.21	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.23	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.25	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.27	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.29	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.31	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.33	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.35	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.37	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.39	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.41	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.43	7	28	28	4.7	3408	85415	Start Curve "200"	79	3500	17.5	17.5	98.0	140.0	103.2	100.2	.1	.1	-3°
14.45	7	28</																

REMARKS:

PAGE NO

REPORT NO
HSER 7002

HSP 1758 4/67

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LOG OF TEST

ENGINEERING LABORATORIES

SHEET 35 OF 35

 DATE 12/1/75
 ENGINEER D. J. ...
 OPERATORS J. ...

G-7

 TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST
 PLAN OF TEST NO. 222PT-31 Rev. A
 SERIAL NO. 44
 PART NO. 163500

UNITS →	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	deg. Blade Angle
11:30	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
11:45	12	12	12	11	3100	8550	99	3500	12.5	990	1440	1007	95.7	2	1	112°
11:50	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:00	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:05	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:10	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:15	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:20	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:25	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:30	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:35	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:40	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:45	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:50	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:55	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
13:00	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
13:05	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°

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REMARKS:

 PAGE NO
 169

 REPORT NO.
 HSER 7002

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LOG OF TEST
ENGINEERING LABORATORIES

DATE 12-16-75 SHEET 16 OF 75
ENGINEER D. L. L...
OPERATORS L. L...

RIG NO. G-7TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TESTW.P.I. NO. 109-CO1-A02-RPLAN OF TEST NO. 222PT-31Rev. APART NO. 767500

SERIAL NO.

UNITS →	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
	1100	27	30	11.7	3000	8.5 GPM	99	3500	12.5	11.1	1400	1000	117.2	1	1	100°
	1105	27	30	11.7	3100	8.5 GPM	99	3500	12.5	11.2	1400	1000	117.2	1	1	100°
	1110	27	30	11.7	3100	8.5 GPM	99	3500	12.5	11.2	1400	1000	117.2	1	1	100°
	1115	27	30	11.7	3100	8.5 GPM	99	3500	12.5	11.2	1400	1000	117.2	1	1	100°
	1120	27	30	11.7	3100	8.5 GPM	99	3500	12.5	11.2	1400	1000	117.2	1	1	100°
					COMPLETED 3400 FREIGHT CYCLES											

REMARKS:

PAGE NO.

HSER 7002

DATE 11-1-72 SHEET 40 OF 40
 ENGINEER W. J. ...
 OPERATORS ...

RIG NO. G-7 PLAN OF TEST NO. 222PT-31 Rev. A PART NO. 767500
 TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST SERIAL NO. ...
 W.P.I. NO. 172

TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Dev. Blace Angle
11:00	10:00	11:00	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:05	10:05	11:05	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:10	10:10	11:10	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:15	10:15	11:15	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:20	10:20	11:20	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:25	10:25	11:25	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:30	10:30	11:30	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:35	10:35	11:35	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:40	10:40	11:40	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:45	10:45	11:45	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:50	10:50	11:50	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:55	10:55	11:55	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:00	11:00	12:00	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:05	11:05	12:05	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:10	11:10	12:10	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:15	11:15	12:15	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:20	11:20	12:20	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:25	11:25	12:25	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:30	11:30	12:30	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:35	11:35	12:35	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:40	11:40	12:40	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:45	11:45	12:45	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:50	11:50	12:50	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:55	11:55	12:55	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
13:00	12:00	13:00	1.7	3700	0.85	99	3450	18	105.2	105.2	105.2	105.2	1	1	1

REMARKS: _____

PAGE NO. _____

REPORT NO. **HSER 7002**

MS 1230 4/87

Hamilton Standard
WINDSOR LOCKS, CONNECTICUT • U.S.A.

LOG OF TEST
ENGINEERING LABORATORIES

DATE 12/15/87 SHEET 41 OF 41
ENGINEER W. J. B. B.
OPERATORS W. J. B. B.

RIG NO G-7

TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST

PLAN OF TEST NO. 222PT-31 Rev. A

SERIAL NO. 767500

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
	21:50	11:50	30:00		3408	.85	99	3450	18	104	126.5	100.5	111.3	.1	.1	700
	21:51	11:51	30:01	4.7	3400	.85	99	3450	18	115	125.5	100.9	108	.1	.1	700
	21:56	11:56	30:06	4.1	3400	.85	99	3450	18	99.4	135.5	102.2	109.7	.1	.1	700
	21:57	11:57	30:07	4.7	3400	.85	99	3450	18	100.7	136.5	108.5	110.3	.1	.1	700
	21:58	11:58	30:08	4.7	3400	.85	99	3450	18	102.4	141.6	108.1	109.3	.1	.1	700
	21:59	11:59	30:09	4.7	3408	.85	99	3450	18	102.6	143.0	109.1	109.1	.1	.1	700
	22:00	12:00	30:10	4.7	3408	.85	99	3450	18	112.0	143.0	109.8	111.1	.1	.1	700
	22:01	12:01	30:11	4.1	3406	.85	99	3450	18	100.9	135.7	110.5	111.6	.1	.1	700
	22:02	12:02	30:12	4.7	3406	.85	99	3450	18	101.6	145.4	110.4	111.1	.1	.1	700
	22:03	12:03	30:13	4.7	3406	.85	99	3450	18	101.6	144.7	110.7	111.8	.1	.1	700
	22:04	12:04	30:14	4.7	3408	.85	99	3450	18	101.6	140.7	110.3	112.2	.1	.1	700
	22:05	12:05	30:15	4.7	3400	.85	99	3450	18	99.4	132.2	113.0	113.0	.1	.1	700
	22:06	12:06	30:16	4.7	3400	.85	99	3450	18	99.4	133.6	111.6	112.5	.1	.1	700
	22:07	12:07	30:17	4.7	3400	.85	99	3450	18	98.4	132.2	113.0	113.0	.1	.1	700
	22:08	12:08	30:18	4.7	3400	.85	99	3450	18	99.4	133.6	111.6	112.5	.1	.1	700
	22:09	12:09	30:19	4.7	3400	.85	99	3450	18	98.4	132.2	113.0	113.0	.1	.1	700
	22:10	12:10	30:20	4.7	3400	.85	99	3450	18	101.6	142.8	111.1	111.5	.1	.1	700

ORIGINAL PAGE 13
OF BOOK 871110

REPORT NO. **HSER 7002**

151724-01

Hamilton Standard

WINDSOR LOCKS, CONNECTICUT • U.S.A.

LOG OF TEST

ENGINEERING LABORATORIES

174

TEST NO. **G-7** PLAN OF TEST NO. **222PT-31** REV. **A** PART NO. **767500**

DATE **12-1-58** ENGINEER **D. J. ...** OPERATORS **...**

TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
2:18	30	34	4.7	3068	.85	99	245	245	112.3	145.0	111.3	110.5	.1	.1	-3
2:22	31	35	4.7	3068	.85	99	245	245	111.6	145.0	111.6	111.5	.1	.1	-
2:26	32	36	4.7	3068	.85	99	245	245	111.9	145.0	111.5	112.3	.1	.1	-
2:30	33	39	4.7	3068	.85	99	245	245	111.7	145.6	111.9	112.2	.1	.1	7
2:36	34	40	4.7	3068	.85	99	245	245	110.6	145.0	111.2	112.5	.1	.1	100
2:40	35	41	4.7	3068	.85	99	245	245	100.1	140.5	111.2	112.0	.1	.1	120
2:44	36	42	4.7	2700	.85	99	245	245	111.6	140.5	111.5	112.5	.1	.1	100
2:50	37	43	4.7	2700	.85	99	245	245	98.6	129.5	111.6	112.3	.1	.1	7
2:55	38	44	4.7	2700	.85	99	245	245	98.2	141.2	111.7	112.2	.1	.1	12
2:59	39	45	4.7	2700	.85	99	245	245	101.2	148.2	111.2	110.5	.1	.1	3
3:02	40	46	4.7	3068	.85	99	245	245	102.0	148.2	111.6	110.0	.1	.1	3
3:06	41	47	4.7	3068	.85	99	245	245	100.2	143.2	112.1	110.7	.1	.1	0
3:10	42	48	4.7	3068	.85	99	245	245	99.7	141.6	111.7	111.3	.1	.1	0
3:15	43	49	4.7	3068	.85	99	245	245	99.1	131.2	111.3	110.7	.1	.1	7
3:20	44	50	4.7	3068	.85	99	245	245	100.5	142.8	110.7	112.0	.1	.1	100
3:22	45	51	4.7	3068	.85	99	245	245	99.9	140.8	109.8	110.7	.1	.1	100

REMARKS

PAGE NO

REPORT NO.
HSER 7002

HSER 7002

UNITS →	Test Time	Total Time	Para.	Rig. R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deq. Blade Angle
0001	13 ⁴⁶	34 ⁴²	4.7	2700	.85	99	3450	255	96.9	3300	100.5	111.5	.1	.1	-10
0008	13 ⁵⁰	34 ⁴²	4.7	2700	.85	99	3450	255	96.8	3450	112.9	111.8	.1	.1	+7
0010	13 ⁵³	34 ⁴²	4.7	2700	.85	99	3450	255	97.5	3450	109.5	110.7	.1	.1	+12
0015	13 ⁵⁷	34 ⁴²	4.7	2700	.85	99	3450	255	94.7	3450	109.5	109.5	.1	.1	-5
0058	14 ⁰²	35 ⁰⁷	4.7	3108	.85	99	3450	273	102.9	3450	107.5	102.9	.1	.1	-3
0002	14 ¹⁴	35 ¹¹	4.7	3108	.85	99	3450	273	101.7	3450	107.8	106.4	.1	.1	0
0007	14 ¹⁷	35 ¹⁶	4.7	3068	.85	99	3450	273	99.9	3450	108.3	105.4	.1	.1	0
0011	14 ²³	35 ²⁰	4.7	3068	.85	99	3450	273	98.2	3473	107.2	110.3	.1	.1	+7
0015	14 ²⁷	35 ²⁴	4.7	3068	.85	99	3450	273	99.1	3440	109.8	110.1	.1	.1	100
0020	14 ³²	35 ²⁹	4.7	3108	.85	99	3450	273	100.5	3419	109.7	109.9	.1	.1	100
0025	14 ³⁷	35 ³⁴	4.7	2700	.85	99	3450	273	95.6	3373	109.5	109.6	.1	.1	100
0029	14 ⁴¹	35 ³⁸	4.7	2700	.85	99	3450	273	96.5	3423	109.5	109.9	.1	.1	+7
0033	14 ⁴⁵	35 ⁴²	4.7	2700	.85	99	3450	273	97.7	3415	109.1	109.1	.1	.1	+12
0035	14 ⁴⁷	35 ⁴⁴	-HUT DOWN			END cycle 300									

REMARKS:

PAGE NO
175

ORIGINAL PAGE 1
OF 1 QUALITY

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REMARKS:

PAGE NO

Hamilton Standard

WINDSOR LOCKS, CONNECTICUT • U.S.A.

LOG OF TEST

ENGINEERING LABORATORIES

DATE 12-11-72 SHEET 44 OF 44
 ENGINEER J. J. J.
 OPERATORS L. J. J.

TEST NO. G-7 PLAN OF TEST NO. 222PT-31 Rev. A
 W.P.I. NO. 1 SERIAL NO. 767500

TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	Lube Oil	PSIG	PSIG	PSIG	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Blade Angle
11:11	11	11	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:12	12	12	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:13	13	13	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:14	14	14	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:15	15	15	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:16	16	16	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:17	17	17	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:18	18	18	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:19	19	19	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:20	20	20	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:21	21	21	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:22	22	22	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:23	23	23	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:24	24	24	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:25	25	25	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:26	26	26	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:27	27	27	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:28	28	28	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:29	29	29	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:30	30	30	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:31	31	31	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:32	32	32	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:33	33	33	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:34	34	34	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:35	35	35	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:36	36	36	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:37	37	37	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:38	38	38	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:39	39	39	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:40	40	40	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:41	41	41	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:42	42	42	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:43	43	43	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:44	44	44	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:45	45	45	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:46	46	46	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:47	47	47	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:48	48	48	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:49	49	49	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:50	50	50	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:51	51	51	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:52	52	52	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:53	53	53	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:54	54	54	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:55	55	55	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:56	56	56	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:57	57	57	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:58	58	58	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:59	59	59	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
12:00	60	60	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111

REPORT NO.
HSER 7002

PAGE 15
QUALITY

PAGE NO
177

Hamilton Standard

WINDSOR LOCKS, CONNECTICUT • U.S.A.

DIVISION OF UNITED AIRCRAFT CORPORATION

LOG OF TEST

ENGINEERING LABORATORIES

FIG. NO. G-7

DATE

ENGINEER

SHEET 11 OF

TYPE OF TEST

G.E. CSEEE ACTUATOR ENDURANCE TEST

PLAN OF TEST NO.

Rev. A

222PT-31

OPERATORS

W.P.I. NO.

SERIAL NO.

PART NO. 767500

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Dej. Blade Angle
	20.0	11.11	38.11	4.7	3408	177	29	2450	11.5	111°	111°	73°	74°	1	2	12°
	40.40	11.23	38.24													
	20.45	11.23	38.24	4.7	3400	174	29	2450	11.5	114°	115°	73°	75°	2	2	12°
	20.48	11.23	38.24	4.7	3408	172	29	2450	11.5	118°	115°	74°	73°	1	2	12°
	21.00	11.11	38.24	4.7	3408	177	29	2450	11.5	121°	112°	74°	74°	1	2	12°
	21.10	11.21	38.24	4.7	3408	178	29	2450	11.5	114°	114°	73°	74°	1	2	12°
	21.10	11.21	38.24	4.7	3400	176	29	2450	11.5	113°	112°	72°	72°	2	2	12°

REMARKS

PAGE NO.

REPORT NO.
HSER 7002

HSE 1258 4/67

Hamilton Standard

INDSOR LOCKS, CONNECTICUT • U.S.A.

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A.

DIVISION OF UNITED STATES DEPARTMENT OF COMMERCE

LOG OF TEST
ENGINEERING LABORATORIES

1258 P.O. G-7

TYPE OF TEST

G.E. COSEE ACTUATOR ENDURANCE TEST

W.P.I. NO.

1258 1258-11-213

PLAN OF TEST NO.

222PT-31

REV. A

ENGINEER

DATE 12 11 13

SHEET 45 OF 45

OPERATORS

PART NO. 767500

TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 LHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
11:21	11:21	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:22	11:22	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:23	11:23	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:24	11:24	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:25	11:25	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:26	11:26	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:27	11:27	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:28	11:28	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:29	11:29	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:30	11:30	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:31	11:31	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:32	11:32	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:33	11:33	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:34	11:34	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:35	11:35	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:36	11:36	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:37	11:37	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:38	11:38	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:39	11:39	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:40	11:40	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:41	11:41	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:42	11:42	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:43	11:43	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:44	11:44	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:45	11:45	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:46	11:46	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:47	11:47	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:48	11:48	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:49	11:49	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:50	11:50	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:51	11:51	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:52	11:52	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:53	11:53	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:54	11:54	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:55	11:55	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:56	11:56	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:57	11:57	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:58	11:58	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
11:59	11:59	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2
12:00	12:00	46:14	47	3000	110	3400	3400	3400	110	128	96	96	1.1	1.2	1.2

REMARKS:

PAGE NO

REPORT NO.

HSER 7032

LOG OF TEST
 ENGINEERING LABORATORIES

DATE 12-15-55
 ENGINEER J. J. J. J.
 OPERATORS J. J. J. J.

SHEET 22 OF 22

RIG NO. G-7
 TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST
 PLAN OF TEST NO. 222PT-31
 REV. A
 PART NO. 762500
 SERIAL NO.

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
	10:17	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:18	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:19	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:20	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:21	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:22	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:23	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:24	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:25	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:26	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:27	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:28	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:29	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:30	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:31	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:32	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:33	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:34	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:35	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:36	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:37	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:38	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:39	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:40	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:41	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:42	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:43	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:44	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:45	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:46	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:47	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:48	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:49	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:50	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:51	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:52	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:53	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:54	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:55	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:56	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:57	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:58	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:59	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	11:00	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5

REPORT NO. HSER 7002
 REMARKS
 PAGE NO.

DATE 1-1-68
ENGINEER
OPERATORS

222PT-31 Rev. A

PART NO. 767500

SERIAL NO.

REMARKS:

REPORT NO.
USER 7002

PAGE NO. 183

ORIGINAL PAGE
OF POOR QUALITY

G-7

184

G.E. OCSEE ACTUATOR ENDURANCE TEST

PLAN OF TEST NO.

Rev. A

222PT-37 Rev. A

WPI NO

[illegible]

SERIAL NO.

PART NO. 767500

[illegible]

SALE

PAGE 12

REPORT NO.
HSER 7002

MSF 1738 4/67

Hamilton Standard

DIVISION OF UNITED AIRCRAFT CORPORATION
MIDDLETOWN, CONNECTICUT - U.S.A.U
A.LOG OF TEST
ENGINEERING LABORATORIESDATE 12-11-77
ENGINEER J. J. J. J.
OPERATORS J. J. J. J.

FIG. NO. G-7

TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST

W.P.I. NO. 112-51-112

PLAN OF TEST NO. 222PT-31

Rev. A

SERIAL NO.

PART NO. 762500

UNITS →	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deq. Blade Angle
	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12
	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13
	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14
	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15
	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16
	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17
	11:18	11:18	11:18	11:18	11:18	11:18	11:18	11:18	11:18	11:18	11:18	11:18	11:18	11:18	11:18	11:18
	11:19	11:19	11:19	11:19	11:19	11:19	11:19	11:19	11:19	11:19	11:19	11:19	11:19	11:19	11:19	11:19
	11:20	11:20	11:20	11:20	11:20	11:20	11:20	11:20	11:20	11:20	11:20	11:20	11:20	11:20	11:20	11:20
	11:21	11:21	11:21	11:21	11:21	11:21	11:21	11:21	11:21	11:21	11:21	11:21	11:21	11:21	11:21	11:21
	11:22	11:22	11:22	11:22	11:22	11:22	11:22	11:22	11:22	11:22	11:22	11:22	11:22	11:22	11:22	11:22
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	11:24	11:24	11:24	11:24	11:24	11:24	11:24	11:24	11:24	11:24	11:24	11:24	11:24	11:24	11:24	11:24
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	11:26	11:26	11:26	11:26	11:26	11:26	11:26	11:26	11:26	11:26	11:26	11:26	11:26	11:26	11:26	11:26
	11:27	11:27	11:27	11:27	11:27	11:27	11:27	11:27	11:27	11:27	11:27	11:27	11:27	11:27	11:27	11:27
	11:28	11:28	11:28	11:28	11:28	11:28	11:28	11:28	11:28	11:28	11:28	11:28	11:28	11:28	11:28	11:28
	11:29	11:29	11:29	11:29	11:29	11:29	11:29	11:29	11:29	11:29	11:29	11:29	11:29	11:29	11:29	11:29
	11:30	11:30	11:30	11:30	11:30	11:30	11:30	11:30	11:30	11:30	11:30	11:30	11:30	11:30	11:30	11:30
	11:31	11:31	11:31	11:31	11:31	11:31	11:31	11:31	11:31	11:31	11:31	11:31	11:31	11:31	11:31	11:31
	11:32	11:32	11:32	11:32	11:32	11:32	11:32	11:32	11:32	11:32	11:32	11:32	11:32	11:32	11:32	11:32
	11:33	11:33	11:33	11:33	11:33	11:33	11:33	11:33	11:33	11:33	11:33	11:33	11:33	11:33	11:33	11:33
	11:34	11:34	11:34	11:34	11:34	11:34	11:34	11:34	11:34	11:34	11:34	11:34	11:34	11:34	11:34	11:34
	11:35	11:35	11:35	11:35	11:35	11:35	11:35	11:35	11:35	11:35	11:35	11:35	11:35	11:35	11:35	11:35
	11:36	11:36	11:36	11:36	11:36	11:36	11:36	11:36	11:36	11:36	11:36	11:36	11:36	11:36	11:36	11:36
	11:37	11:37	11:37	11:37	11:37	11:37	11:37	11:37	11:37	11:37	11:37	11:37	11:37	11:37	11:37	11:37
	11:38	11:38	11:38	11:38	11:38	11:38	11:38	11:38	11:38	11:38	11:38	11:38	11:38	11:38	11:38	11:38
	11:39	11:39	11:39	11:39	11:39	11:39	11:39	11:39	11:39	11:39	11:39	11:39	11:39	11:39	11:39	11:39
	11:40	11:40	11:40	11:40	11:40	11:40	11:40	11:40	11:40	11:40	11:40	11:40	11:40	11:40	11:40	11:40
	11:41	11:41	11:41	11:41	11:41	11:41	11:41	11:41	11:41	11:41	11:41	11:41	11:41	11:41	11:41	11:41
	11:42	11:42	11:42	11:42	11:42	11:42	11:42	11:42	11:42	11:42	11:42	11:42	11:42	11:42	11:42	11:42
	11:43	11:43	11:43	11:43	11:43	11:43	11:43	11:43	11:43	11:43	11:43	11:43	11:43	11:43	11:43	11:43
	11:44	11:44	11:44	11:44	11:44	11:44	11:44	11:44	11:44	11:44	11:44	11:44	11:44	11:44	11:44	11:44
	11:45	11:45	11:45	11:45	11:45	11:45	11:45	11:45	11:45	11:45	11:45	11:45	11:45	11:45	11:45	11:45
	11:46	11:46	11:46	11:46	11:46	11:46	11:46	11:46	11:46	11:46	11:46	11:46	11:46	11:46	11:46	11:46
	11:47	11:47	11:47	11:47	11:47	11:47	11:47	11:47	11:47	11:47	11:47	11:47	11:47	11:47	11:47	11:47
	11:48	11:48	11:48	11:48	11:48	11:48	11:48	11:48	11:48	11:48	11:48	11:48	11:48	11:48	11:48	11:48
	11:49	11:49	11:49	11:49	11:49	11:49	11:49	11:49	11:49	11:49	11:49	11:49	11:49	11:49	11:49	11:49
	11:50	11:50	11:50	11:50	11:50	11:50	11:50	11:50	11:50	11:50	11:50	11:50	11:50	11:50	11:50	11:50
	11:51	11:51	11:51	11:51	11:51	11:51	11:51	11:51	11:51	11:51	11:51	11:51	11:51	11:51	11:51	11:51
	11:52	11:52	11:52	11:52	11:52	11:52	11:52	11:52	11:52	11:52	11:52	11:52	11:52	11:52	11:52	11:52
	11:53	11:53	11:53	11:53	11:53	11:53	11:53	11:53	11:53	11:53	11:53	11:53	11:53	11:53	11:53	11:53
	11:54	11:54	11:54	11:54	11:54	11:54	11:54	11:54	11:54	11:54	11:54	11:54	11:54	11:54	11:54	11:54
	11:55	11:55	11:55	11:55	11:55	11:55	11:55	11:55	11:55	11:55	11:55	11:55	11:55	11:55	11:55	11:55
	11:56	11:56	11:56	11:56	11:56	11:56	11:56	11:56	11:56	11:56	11:56	11:56	11:56	11:56	11:56	11:56
	11:57	11:57	11:57	11:57	11:57	11:57	11:57	11:57	11:57	11:57	11:57	11:57	11:57	11:57	11:57	11:57
	11:58	11:58	11:58	11:58	11:58	11:58	11:58	11:58	11:58	11:58	11:58	11:58	11:58	11:58	11:58	11:58
	11:59	11:59	11:59	11:59	11:59	11:59	11:59	11:59	11:59	11:59	11:59	11:59	11:59	11:59	11:59	11:59
	12:00	12:00	12:00	12:00	12:00	12:00	12:00	12:00	12:00	12:00	12:00	12:00	12:00	12:00	12:00	12:00

REMARKS:

PAGE NO.

185

ORIGINAL PAGE
OF POOR QUALITY

REPORT NO.

HSER 7002

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Hamilton Standard
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1-518 G-7

36	TYPE OF TEST	W.P.I. NO.

G.E. QCSEE ACTUATOR ENDURANCE TEST

[illegible]

G-7

5

PLAN OF TEST NO.

SERIAL NO.

222PT-31

Rev. A

REV. H

LOG OF TEST ENGINEERING LABORATORIES

DATE 12-18-78

ENGINEERING

11) **January**

207-1346

[illegible]

DEW 30

PAGE NO

REPORT NO.
HSER 7002

HS 1758 4/67

REG. NO. G-7

TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST

W.P.I. NO. 777 103-403 B

PLAN OF TEST NO. 222PT-31

REV. A

DATE 12-15-75

ENGINEER D. H. HUNT

OPERATORS S. HUNT

PART NO. 767500

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deq. Blade Angle
1110	24	41	45	4.7	3068	.85	99	3500	18	122	96	55	59	.1	.1	8.5
1125	24	41	45													
1140	24	41	45													
1155	24	41	45													
1170	24	41	45													
1185	24	41	45													
1200	25	42	46	4.7	3068	.85	99	3500	18	122	96	55	73	.1	.1	12
1215	25	42	46													
1230	25	42	46													
1245	25	42	46													
1260	25	42	46													
1275	25	42	46													
1290	25	42	46	4.7	3068	.85	99	3500	18	122	96	55	76	.1	.1	100
1305	25	42	46													
1320	25	42	46													
1335	25	42	46													
1350	25	42	46													
1365	25	42	46													
1380	25	42	46													
1395	25	42	46													
1410	25	42	46													
1425	25	42	46													
1440	25	42	46													
1455	25	42	46													
1470	25	42	46													
1485	25	42	46													
1500	25	42	46													
1515	25	42	46													
1530	25	42	46													
1545	25	42	46													
1560	25	42	46													
1575	25	42	46													
1590	25	42	46													
1605	25	42	46													
1620	25	42	46													
1635	25	42	46													
1650	25	42	46													
1665	25	42	46													
1680	25	42	46													
1695	25	42	46													
1710	25	42	46													
1725	25	42	46													
1740	25	42	46													
1755	25	42	46													
1770	25	42	46													
1785	25	42	46													
1800	25	42	46													
1815	25	42	46													
1830	25	42	46													
1845	25	42	46													
1860	25	42	46													
1875	25	42	46													
1890	25	42	46													
1905	25	42	46													
1920	25	42	46													
1935	25	42	46													
1950	25	42	46													
1965	25	42	46													
1980	25	42	46													
1995	25	42	46													

REMARKS:

REPORT NO. HSER 7002

Hamilton Standard
DIVISION OF UNITED TECHNOLOGIES
WINDSOR LOCKS, CONNECTICUT • U.S.A.

U.A.

LOG OF TEST
ENGINEERING LABORATORIES

DATE 12-19-73
ENGINEER J. H. HUNT
OPERATORS J. H. HUNT

P.O. NO. 6-7

TYPE OF TEST

W.P.I. NO.

G.E. GCSEE ACTUATOR ENDURANCE TEST

PLAN OF TEST NO.

222PT-31

Rev. A

SERIAL NO.

PART NO. 767550

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Den. Blade Angle
2135	26	41	41	4.1	3060	.85	99	3500	END CYCLE #161	97	135	51	75	.1	.1	3
2145	26	41	41	4.1	3060	.85	99	3500	END CYCLE #162							
2155	26	41	41	4.1	3060	.85	99	3500	END CYCLE #163							
2205	26	41	41	4.1	3060	.85	99	3500	END CYCLE #164							
2215	26	41	41	4.1	3060	.85	99	3500	END CYCLE #165	109	104	54	51	.1	.1	12
2225	26	41	41	4.1	3060	.85	99	3500	END CYCLE #166							
2235	26	41	41	4.1	3060	.85	99	3500	END CYCLE #167	104	133	80	74	.1	.1	6
2245	26	41	41	4.1	3060	.85	99	3500	END CYCLE #168							
2255	26	41	41	4.1	3060	.85	99	3500	END CYCLE #169							
2305	26	41	41	4.1	3060	.85	99	3500	END CYCLE #170	100	132	77	75	.1	.1	3
2315	26	41	41	4.1	3060	.85	99	3500	END CYCLE #171							
2325	26	41	41	4.1	3060	.85	99	3500	END CYCLE #172							
2335	26	41	41	4.1	3060	.85	99	3500	END CYCLE #173	119	121	78	75	.1	.1	11
2345	26	41	41	4.1	3060	.85	99	3500	END CYCLE #174							
2355	26	41	41	4.1	3060	.85	99	3500	END CYCLE #175							

REMARKS

190 1758 4/17

Hamilton Standard
WINDSOR LOCKS, CONNECTICUT - U.S.A.

U.A.

LOG OF TEST
ENGINEERING LABORATORIES

DATE 12-14-75 SHEET 23 OF 23
ENGINEER D. N. L. C. C.
OPERATORS S. H. H. R. L.

S/C NO. G-7

TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST
W.P.I. NO. 117-003-ADD 13

PLAN OF TEST NO. 222PT-31 Rev. A
SERIAL NO. 767500

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deq. Blade Angle
2235	21	18	20	4.7	3408	.85	99	3500	END CYCLE #176	101	123	78	74	.1	.1	700
2205	21	18	30	4.7	3068	.85	99	3500	END CYCLE #178	99	135	78	75	.1	.1	700
2220	28	18	15	4.7	2700	.85	99	3500	END CYCLE #182	99	124	78	75	.1	.1	700
2230	28	17	05	4.7	3408	.85	99	3500	END CYCLE #185	101	137	76	74	.1	.1	700

REMARKS

PAGE NO.

REPORT NO.
HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

DATE 12-1-72 1 OF 1
ENGINEER B. L. L. L. L.
OPERATORS ...

CPI-016

TYPE OF TEST

PLAN OF TEST NO. _____
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REMARKS:

PAGE NO

REPORT NO.
HSER 7002

Hamilton Standard

DIVISION OF UNITED AIRCRAFT COMPANY, INC.
ROCKFORD, ILLINOIS • U.S.A.LOG OF TEST
ENGINEERING LABORATORIES

FIG. NO.

TYPE OF TEST

W.P.I. NO.

G-7

C-103

AC 203

PLAN OF TEST NO.

SERIAL NO.

222DT-31 REV A

PART NO.

16300

DATE

12-30-75

ENGINEER

D. E. S. HARRIS

OPERATORS

L. J. HARRIS

UNITS

TIME

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REMARKS

PAGE NO

REPORT NO.
HSER 7002

Hamilton Standard
DIVISION OF UNITED
A. A. LOCKS, CONNECTICUT • U.S.A.

U. S. A.

LOG OF TEST
ENGINEERING LABORATORIES

RIG NO. C-100

TYPE OF TEST Pressure vs Flow

W.P.I. NO. 10

PLAN OF TEST NO. 100
SERIAL NO.

DATE 1-11-68 OF
ENGINEER D. J. [illegible]
OPERATORS [illegible]

PART NO.

UNITS →	TIME	INLET PRESS	FLOW GPM	OF GPM PERMIN
	10	9	80	
	20	10.5	110	
	30	18	135	
	40	21.75	129	
	50	24.25	137	
	60	26.75	133	
	70	29	134	
	80	31	134	

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OF POOR QUALITY

REMARKS MIL-L-78086

REPORT NO.
HSER 7002

TYPE OF TEST

PLAN OF TEST NO. _____
SERIAL NO. _____

SERIAL NO.

PART NO.

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REPORT NO.

HSER 7002[illegible]

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PAGE NO

LOG OF TEST ENGINEERING LABORATORIES

ON 517

1511 KO 3d41

W.P.I. NO.

2000-2001

PLAN OF TEST NO.

SERIAL NO.

016 280 0000

DATE _____

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OPERATORS

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REMARKS:

PAGE NO
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REPORT NO.

HSER 7002

Hamilton Standard
WINDSOR LOCKS, CONNECTICUT - U.S.A.

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LOG OF TEST
ENGINEERING LABORATORIES

DATE 2-1-77
ENGINEER J. J. KIRBY
OPERATORS J. J. KIRBY, J. S.

PLAN OF TEST NO. 222PT-38 Rev. A
SERIAL NO. PART NO. 767500

TEST NO. G-7
TYPE OF TEST G.E. COSEE ACTUATOR ENDURANCE TEST
W.P.I. NO. 1735 4/67

TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4
5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5
6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7
8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9
10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11
12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12
13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13
14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
15	15	15	15	15	15	15	15	15	15	15	15	15	15	15	15
16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16
17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17
18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18
19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19
20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20

REPORT NO.
HSER 7002

PG NO. G-7

TYPE OF TEST
W.P.I. NO.

G.E. QCSEE ACTUATOR ENDURANCE TEST

PLAN OF TEST NO. _____
SERIAL NO. _____

222PT-38

SERIAL NO.

PART NO.

763500

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PAGE NO

HSER 7002

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Hamilton Standard
ANDERSON LOCKS, CONNECTICUT • U.S.A.

LOG OF TEST ENGINEERING LABORATORIES

G-7

TYPE OF TEST

G.E. QCSEE ACTUATOR ENDURANCE TEST

PLAN OF TEST NO.

222PT-38

27

ENGINEER

Neimphes

W.P.I. NO.

4406 603 1054

SERIAL NO. _____
 FILE NO. _____

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References

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REMARKS:

PAGE NO
205

HSER 7002

KLPUNKI, U.S.

Hamilton Standard

WINDSOR LOCKS, CONNECTICUT • U.S.A.

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LOG OF TEST ENGINEERING LABORATORIES

SHEET 5 OF 1308

1348 of

RIG NO. **G-7**

TYPE OF TEST

EE OCSEE ACTUATOR ENDURANCE TEST

222PT-38

PLAN OF TEST

W.P.L. NO.

PART TWO

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
14	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
15	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
16	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
17	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
18	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
19	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
20	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
21	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
22	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
23	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
24	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
25	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
26	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
27	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
28	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
29	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
30	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
31	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
32	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
33	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
34	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
35	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
36	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
37	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
38	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
39	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
40	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
41	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
42	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
43	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
44	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
45	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
46	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
47	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
48	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
49	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
50	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
51	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
52	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
53	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
54	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
55	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
56	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
57	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
58	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
59	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
60	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
61	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
62	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
63	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
64	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
65	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
66	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
67	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
68	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
69	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
70	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
71	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
72	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
73	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
74	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
75	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
76	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
77	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
78	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
79	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
80	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
81	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
82	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
83	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
84	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
85	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
86	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
87	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
88	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
89	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
90	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
91	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
92	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
93	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
94	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
95	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
96	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
97	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
98	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
99	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
100	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
101	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
102	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
103	12	12	24	3.6	3000	1500	25	3400	18	1000	1400	1.1	1000	.1	.2	10
104	12	12	24	3.6	3000	1500	25	3400	18							

DEWARS.

PAGE NO

HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

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TYPE OF TEST

100

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172-177

PLAN OF TEST NO.

SERIAL NO.

PART NO.

DATE _____

ENGINEER

OPERATORS

84

Abstract

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REPORT NO.
HSER 7002

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PAGE 207

HSER 7002

APPENDIX E

TEST CHRONOLOGY

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TEST CHRONOLOGY

11-4-75	Started installation of actuator on rig.
11-5-75 & 11-6-75	Continued installation of actuator on rig.
11-7-75	Checked torque required to change pitch at wave generator. Appears high.
11-8-75	Removed actuator from disc. Retorqued blade retaining nuts to approximately equal twisting torques for each blade. Reinstalled actuator. Torque at wave generator now \approx 150 inch pounds. Continued assembly.
11-10-75	Completed installation. Ran LVDT calibrations and lubrication flow check. Found flex shaft leaks.
11-11-75	Sealed up leaks in flex shaft. Started running travel limit switch tests. After several stops, actuator would not move. Partial disassembly revealed no back output shaft fractured.
11-12-75 thru 11-19-75	Removed actuator from rig for inspection, and reinstalled on rig with repaired (welded) no back output shaft. Torque at wave generator to change pitch 140 inch pounds and at manual input \approx 45 inch pounds.
11-20-75	Attempts to run stopped by oil leaks at rig drive flange and water leaks at rig clutch. Removed actuator and disc from rig. Reworked oil drain holes in rig drive flange, and revised drive flange seal and clutch cooling water plumbing.

TEST CHRONOLOGY (continued)

11-21-75	Reinstalled disc and actuator. Oil leaks o.k., but clutch cooling water marginal. Could not get fan speed above 2750 rpm with blade angle as circuit breakers trip.
11-22-75	Exploring rig power problem.
11-24-75 thru 11-26-75	Fabricated shroud to enclose blades. Check run shows power problem solved.
11-28-75	Ran performance tests and 15 flight cycles with reduced pitch change rate.
11-29-75	Ran 31 flight cycles (total 46) and max pitch change rate tests.
12-1-75	Started disassembly for inspection. Found no-back output shaft fractured.
12-2-75 thru 12-5-75	Continued inspection and reassembly with new output shaft. Hydraulic motor bevel gear mesh pattern high. Reshimmed closer into mesh. Trunnion roller pattern on cam is high on one side of track, low on other. Torque to change pitch at manual input <u>40</u> inch pounds.
12-6-75	Ran 14 flight cycles (total 60). Inspected no-back hardware, o.k.
12-8-75	Ran 71 flight cycles (total 131).
12-9-75	Ran 24 flight cycles (total 155). Inspected no-back hardware, o.k..
212	Ran 33 flight cycles (total 188).

TEST CHRONOLOGY (continued)

12-10-75	Ran 52 flight cycles (total 240). Torque to change pitch at manual input now 35-40 inch pounds.
12-15-75	Ran part of frequency response testing and 60 flight cycles (total 300).
12-16-75	Inspected no-back hardware, o.k. Reworked no-back output shaft to reduce stress concentrations and shot peened it in web area.
12-17-75	Reassembled and ran 70 flight cycles (total 370).
12-18-75	Ran 115 flight cycles (total 485).
12-19-75	Ran 20 flight cycles (total 505). Disassembled no-back for inspection. Output shaft fractured in one web.
12-29-75	Reassembled and ran rotating frequency response test.
12-30-75	Ran positioning accuracy and minimum blade angle change tests.
12-31-75	Re-ran travel limit switch, performance, positioning accuracy, and static frequency response tests.
1-2-76 thru 1-7-76	Complete disassembly and inspection including magnaflux and zygo. Hydraulic motor bevel gear mesh showed pitting and scoring. One hydraulic motor damaged during disassembly. No-back output shaft was fractured. All other magnaflux and zygo o.k.

TEST CHRONOLOGY (continued)

1-8-76 thru 1-12-76	Reassembled beta regulator with one new motor, new bevel gear set, and reworked feedback shaft to provide positive bevel gear mesh lubrication.
1-13-76	Reassembled differential gear train. Beta regulator at inspection for installation dimension check.
1-14-76	Ran lubrication flow versus pressure test on beta regulator.
1-15-76	Beta regulator to shipping. Reassembled no-back with new spring and new output shaft.
1-16-76	Fitting spring to drum.
1-19-76	Started actuator installation in rig. Rear housing fractured during assembly.
1-20-76 thru 1-30-76	Repair of rear housing. Ran static deflection tests on snubber.
2-2-76 thru	Reassembly on rig. Actuator has new no-back spring and output shaft, new flex shaft, and snubber. New flex shaft has slight leak.
2-5-76	Ran an LVDT calibration and maximum pitch change rate testing. Inspected no-back hardware, o.k.

TEST CHRONOLOGY) (continued)

2-6-76	Reassembled actuator and attempted to run flight cycles. Had trouble with controller and pumps which supply pitch change fluid. Ran 3 flight cycles.
2-7-76	Ran 12 flight cycles (total 15). Had trouble with pitch change fluid pumps.
2-9-76	Installed an accumulator in the pitch change fluid supply system.
2-10-76	Ran 45 flight cycles (total 60).
2-11-76	Attempted to run static frequency response test. No response at ± 4 ma input to servo valve.
2-12-76	Disassembled regulator. Found one hydraulic motor (new one) has heavy wear on housing at drive gear face. Dimensional checks show nothing. Started rework necessary to obtain new motor.
2-13-76	Reassembled regulator and ran travel limit switch tests.
2-14-76	Installed new motor in regulator. Actuator responds to ± 4 ma inputs to servo valve. Ran blade angle accuracy and performance tests.
2-16-76	Ran static frequency response test. Started disassembly.
2-17-76	Hardware inspection revealed that flex shaft had been overtorqued. All other hardware o.k.

HSER 7002

**APPENDIX F
REFERENCES**

REFERENCE LIST

HSPC 74A14	QCSEE Variable Pitch Fan System Proposal
SP 08A74	QCSEE Variable Pitch Fan Pitch Change System
NASA CR-134852	Hamilton Standard Cam/Harmonic Drive Variable Pitch Fan Actuation System Detail Design Report
NASA CR-134873	QCSEE Ball Spline Pitch Change Mechanism Design Report